

JANUARY 1951

electronics

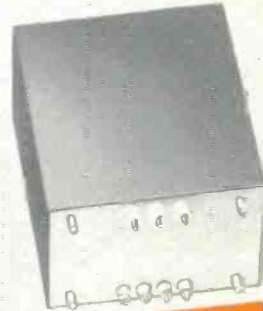
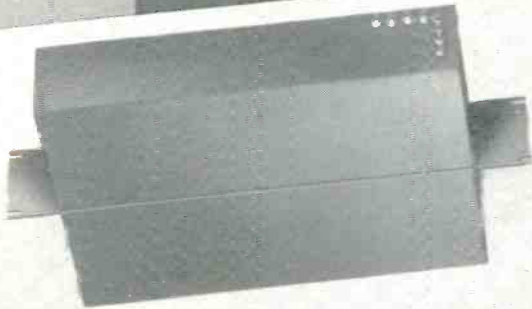
A MCGRAW-HILL PUBLICATION

PERMANENT-MAGNET
ELECTRON MICROSCOPE



for Military Components

UTC was the largest supplier of transformer components in World War II. Present UTC production is on a similar basis. Illustrated below are a few of the thousand military types in UTC 1950 production.



Carrier frequency filter.....Aircraft low frequency filter.....Plate transformer.



Typical hermetically sealed power transformers for 60 cycle service.



Hermetically sealed audio and pulse transformers.



60 cycle and 400 cycle components hermetically sealed and fosterized.



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JANUARY • 1951

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January, 1951

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Member ABC and ABP

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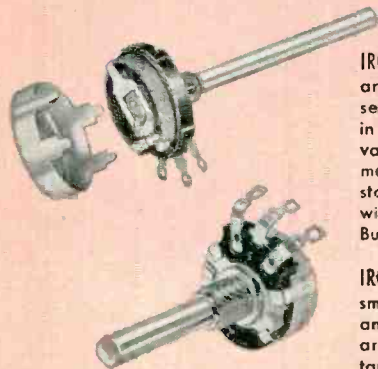
IRC Matched Pairs provide a dependable low-cost solution to close-tolerance requirements. Both Type BT and BW Resistors are available in matched pairs. Catalog Bulletin B-3.

IRC Sealed Precision Voltmeter Multipliers are suitable and dependable for use under the most severe humidity conditions. Each consists of several IRC Precisions mounted and interconnected, encased in a glazed ceramic tube. Catalog Bulletin D-2.

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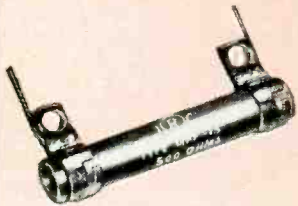
IRC Type W Wire Wound Controls are designed for long, dependable service and balanced performance in every characteristic. These 2-watt variable wire wound units provide maximum adaptability to most rheostat and potentiometer applications within their power rating. Catalog Bulletin A-2.

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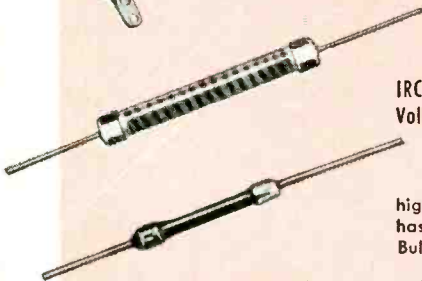
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IRC Type MP High Frequency Resistors afford stability with low inherent inductance and capacity in circuits involving steep wave fronts, high frequency measuring circuits and radar pulse equipment. Available in sizes from 1/4 to 90 watts. Catalog Bulletin F-1.




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Wherever the Circuit Says 

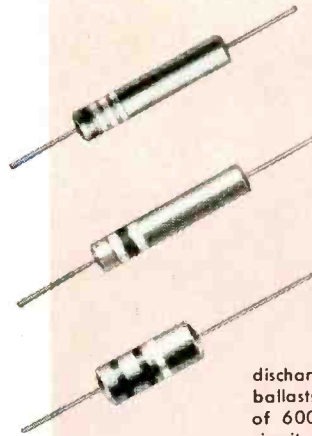
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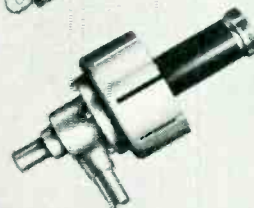
IRC Fixed and Adjustable Power Wire Wounds give balanced performance in every characteristic—are available in a full range of sizes, types and terminals for exacting, heavy-duty applications. Catalog Bulletin C-2.



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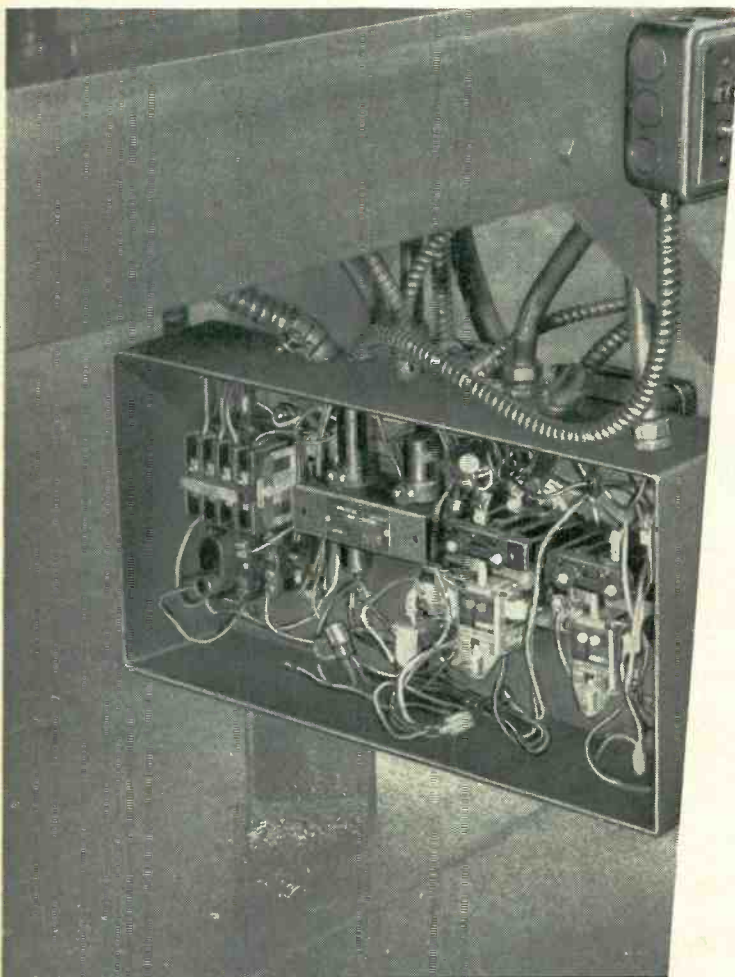
THE ADLAKE RELAY in this facing machine control box at the Northern Indiana Brass Co. was installed October 18, 1948. Prior to its installation, the machine had been subject to frequent expensive breakdowns. Yet since it was installed, *the relay has operated continuously 7¹/₂ million times with no maintenance whatever—and the machine has had no breakdowns!*

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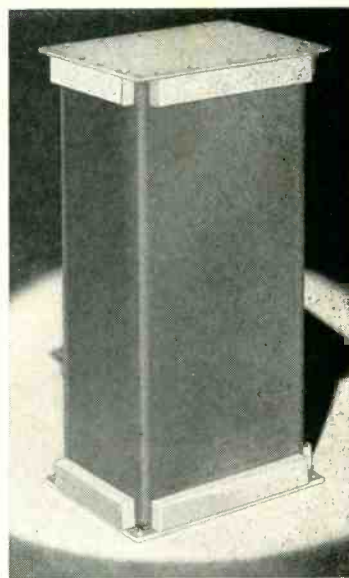
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Your inquiries will receive immediate attention.*

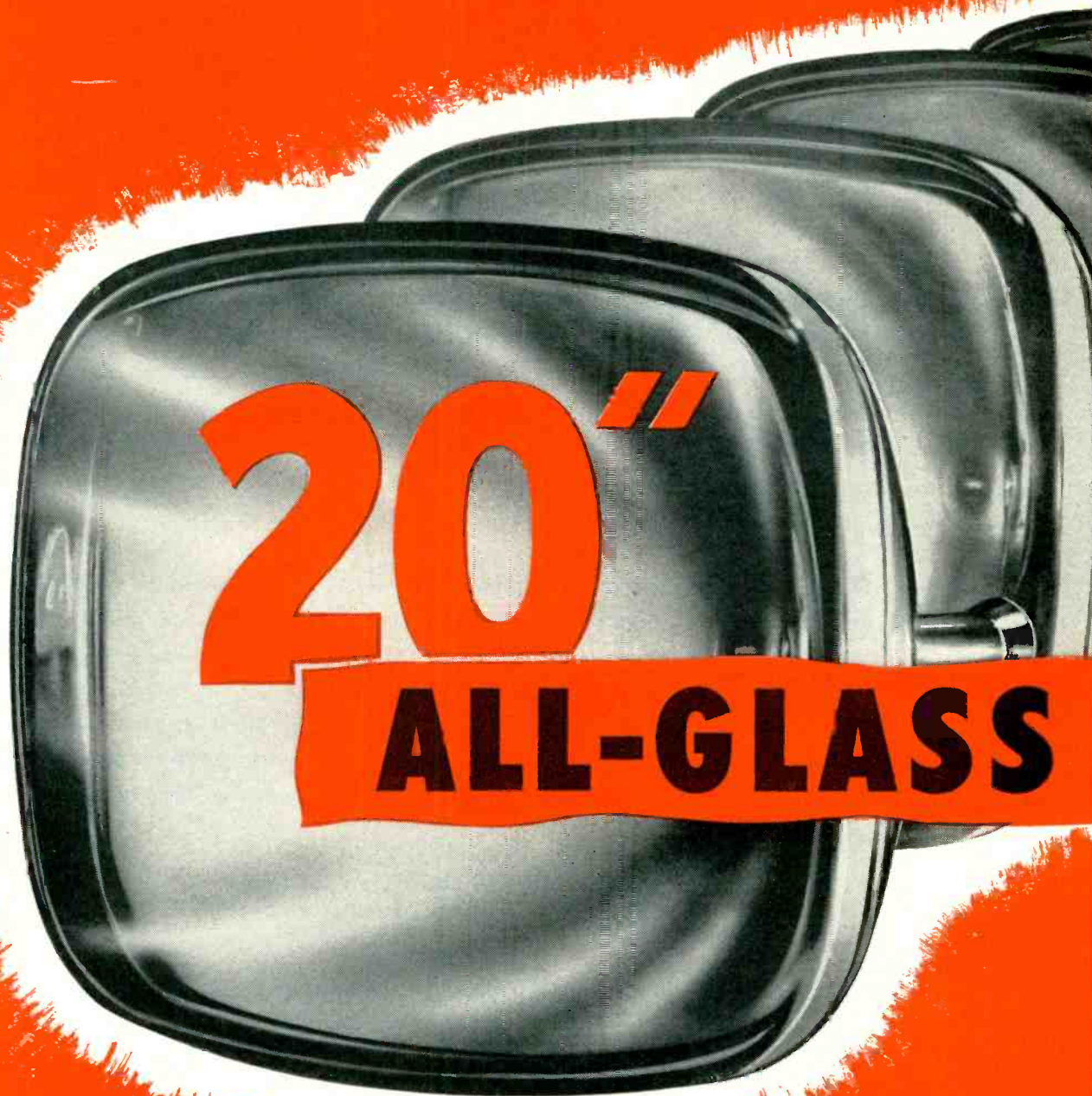
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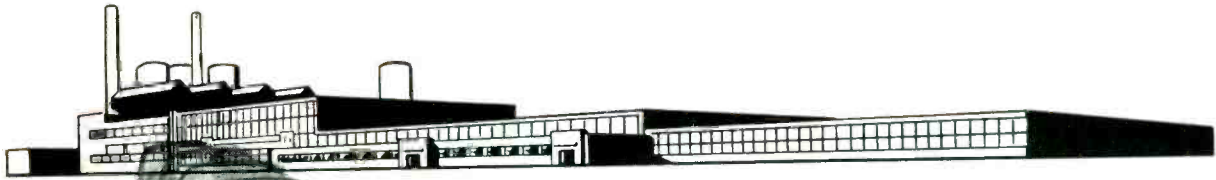
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New Corning Plant at Albion, Michigan, devoted exclusively to television bulb manufacturing is now in operation. The latest in equipment and efficient layout provides additional volume production of the finest all-glass television bulbs.

When television was still a laboratory curiosity, Corning made the *first* experimental bulbs. All during the early stages of T-V set production, Corning was the principal manufacturer of television bulbs. In keeping with this tradition, and in answer to demands from the Television Industry, Corning has introduced the *all-glass 20" rectangular bulb!*—the largest T-V bulb in volume production today.

The first of this size on the market, the new 20" bulb combines all the improvements developed through years of research at Corning. Among these are light-weight, lead-free glass ideally suited to electronic applications, stronger bulb assemblies from electric sealing, and constant quality from improved glass melting and forming techniques. The new Corning 20" all-glass bulb is the last word in quality, durability and size.

television bulbs

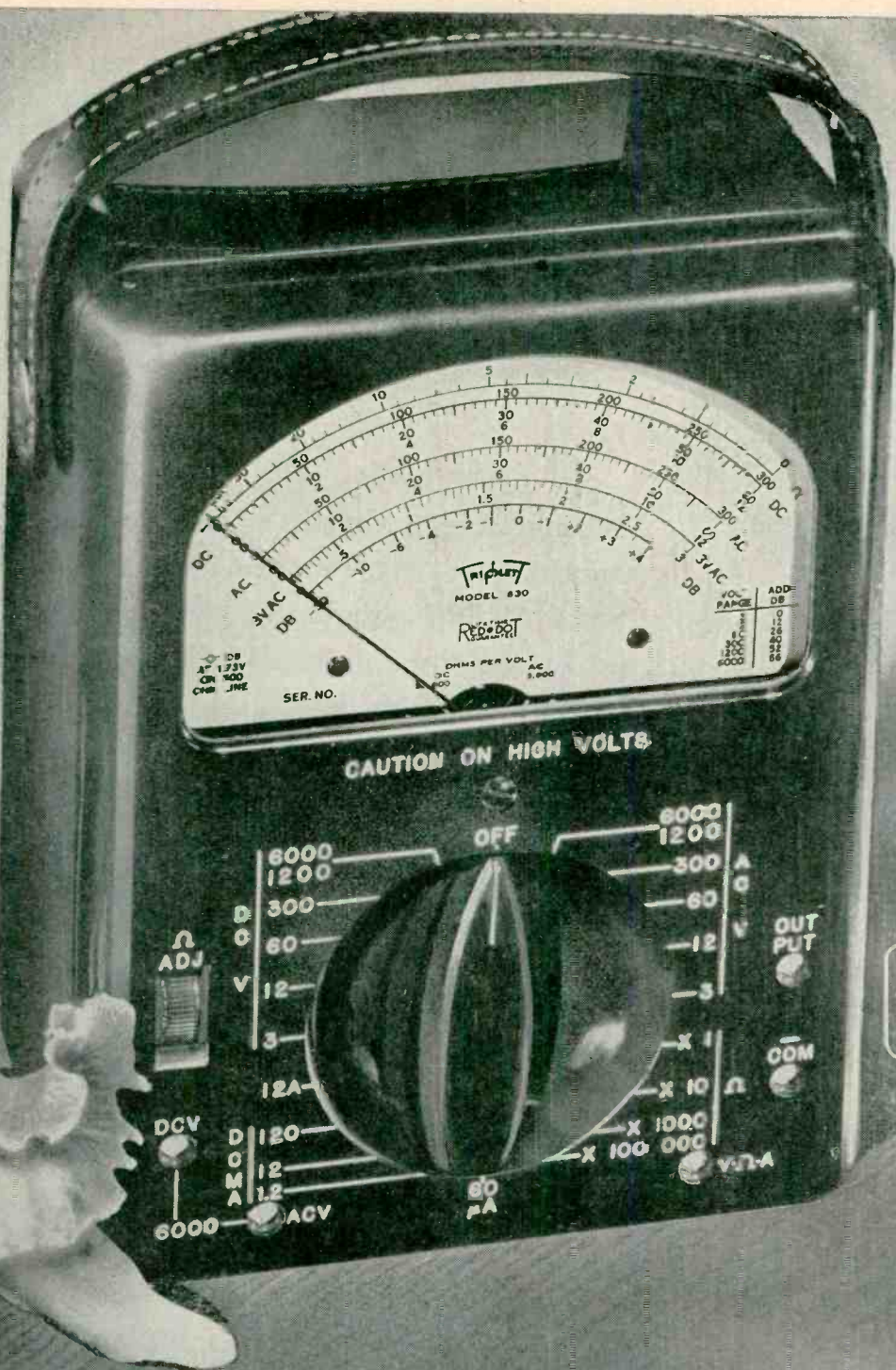


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Our company is now deeply engaged in the manufacture of fabricated metal housings and components of critically needed defense equipment.

If the world-wide crisis continues, these jobs will continue to receive high priority. This does not mean, however, that civilian orders will not be given every possible consideration, within our ability.

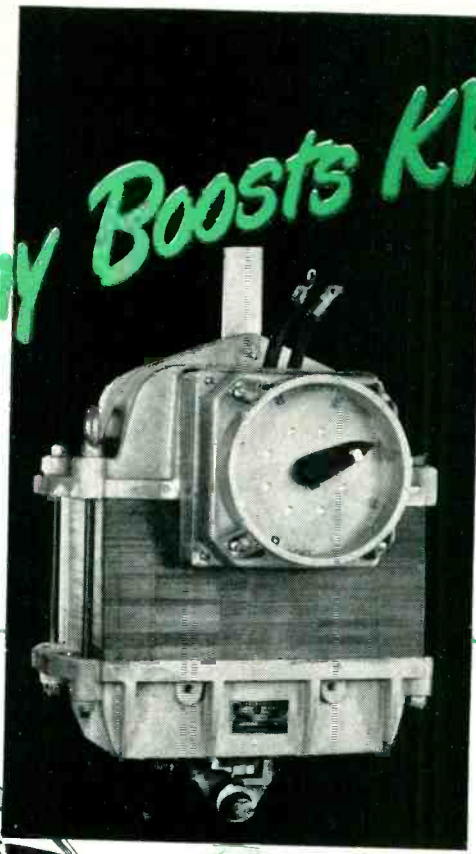
Actually, most of our customers manufacturing defense equipment are regular customers who make the same apparatus in peace and war. The only essential difference now is that we are doing their work in greater quantity. Hence, for most of our customers we are rendering an *increased* amount of service.

For those whose products do not classify as vital to defense, the door is still open, and we shall continue to serve them in any manner possible that does not retard any defense project.

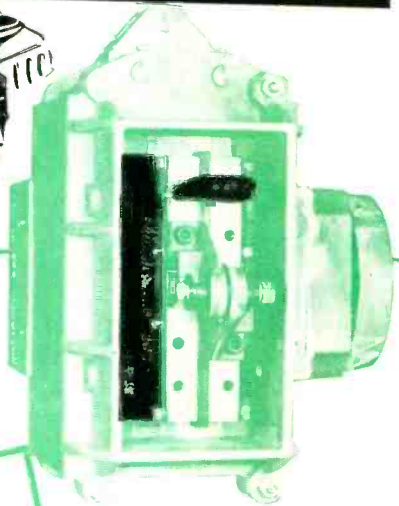
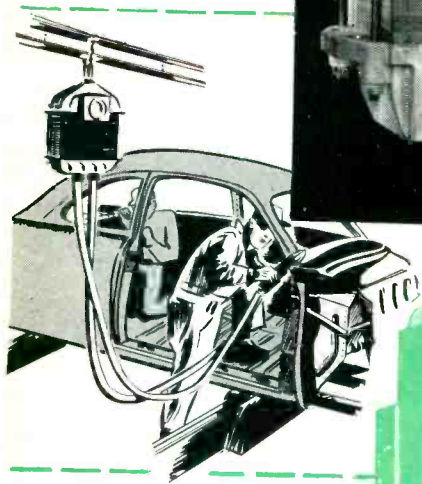
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McCarthy Boosts KVA Rating 30%



with
**NATVAR
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←
 This McCarthy Type 525-PG welding transformer is compact and weighs only 458 pounds, yet it is rated 75KVA, 220 or 440 primary volts (not interchangeable), 60 cycle, 1 phase, 108°C temperature rise, at 50% duty cycle. An extra heavy heat selector switch gives secondary voltages in eight steps from 5.00 to 9.16, parallel connection, or 10.0 to 18.32, series connection.

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 Primary coils are insulated between turns with Natvar varnished Fiberglas tape, dipped and baked. The wound coil is then insulated with mica and Natvar varnished Fiberglas tape, again dipped and baked, and finished with air drying varnish. Secondary coils are heavy wall square copper tubes through which cooling water circulates. Leads are insulated and protected with Natvar 400 heat resistant extruded vinyl tubing.

←
MCCARTHY ELECTRIC CO., Detroit, manufactures welding transformers used extensively on production lines in the automotive industry for welding bodies and various fabricated parts, and in the refrigerator industry for welding boxes. Since it is more practical to weld large assemblies with guns rather than on stationary machines, portability is important. Size and weight of the transformer must therefore be

kept at a minimum. And because many of these units are in continuous service 24 hours a day, long life is important, too.

By designing and building these transformers for higher continuous operating temperatures, McCarthy has succeeded in raising capacity 30% without increasing the size or weight. McCarthy has standardized on Natvar varnished Fiberglas and Natvar 400 Extruded Vinyl Tubing because of their uniformly high resistance to heat, and because both have exceptional aging characteristics, which means longer life.

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- Varnished papers
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- Varnished tubings and sleeveings
- Varnished identification markers
- Lacquered tubings and sleeveings
- Extruded vinyl tubing and tape
- Extruded vinyl identification markers
































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ADVENTURES IN ELECTRONIC DESIGN

Centralab's Printed Electronic Circuits May Solve a Problem for You

In a busy Washington  office during the past war  hung a sign  which said — "We do the miraculous every day — the impossible takes just a little longer." Today, that sign  could hang in the offices of  Centralab. For example, someone wanted a *small* speech amplifier  Centralab's answer —  Ampec, a full 3 stage unit, two of which can fit inside of a regular pack of cigarettes!  A radio manufacturer  wanted a *small* audio-detection unit. Centralab's answer  Audet, a unit one-third size of an ordinary soda-cracker!  How were these things done? With Centralab's  Printed Electronic Circuits — a pioneered  development of  Centralab. Yes, and here are some of the benefits that many manufacturers of radio  TV sets  and other electronic gear  have reaped from using PEC's. They've eliminated numerous individual parts  their handling, inventory  and assembly. They've gotten more consistent and better performance results.  They've reduced finished product size and weight.  They've eliminated wiring errors  and cut down on the number of  soldered connections. What's more, they've been able to stretch  their resistor supplies . . . an important factor in meeting current volume demands  for TV and radio production. Look over your own situation.  Want to cut costs?  Speed up assembly?  Then on the next two pages you may see a Centralab Printed Electronic Circuit unit  that will help you do just that! If you don't see what you want — contact us.  Tell us your problems. Maybe we can do the miraculous or take a little longer and accomplish the impossible! 

Centralab — DEVELOPMENTS THAT CAN HELP YOU 


Division of GLOBE-UNION INC., Milwaukee

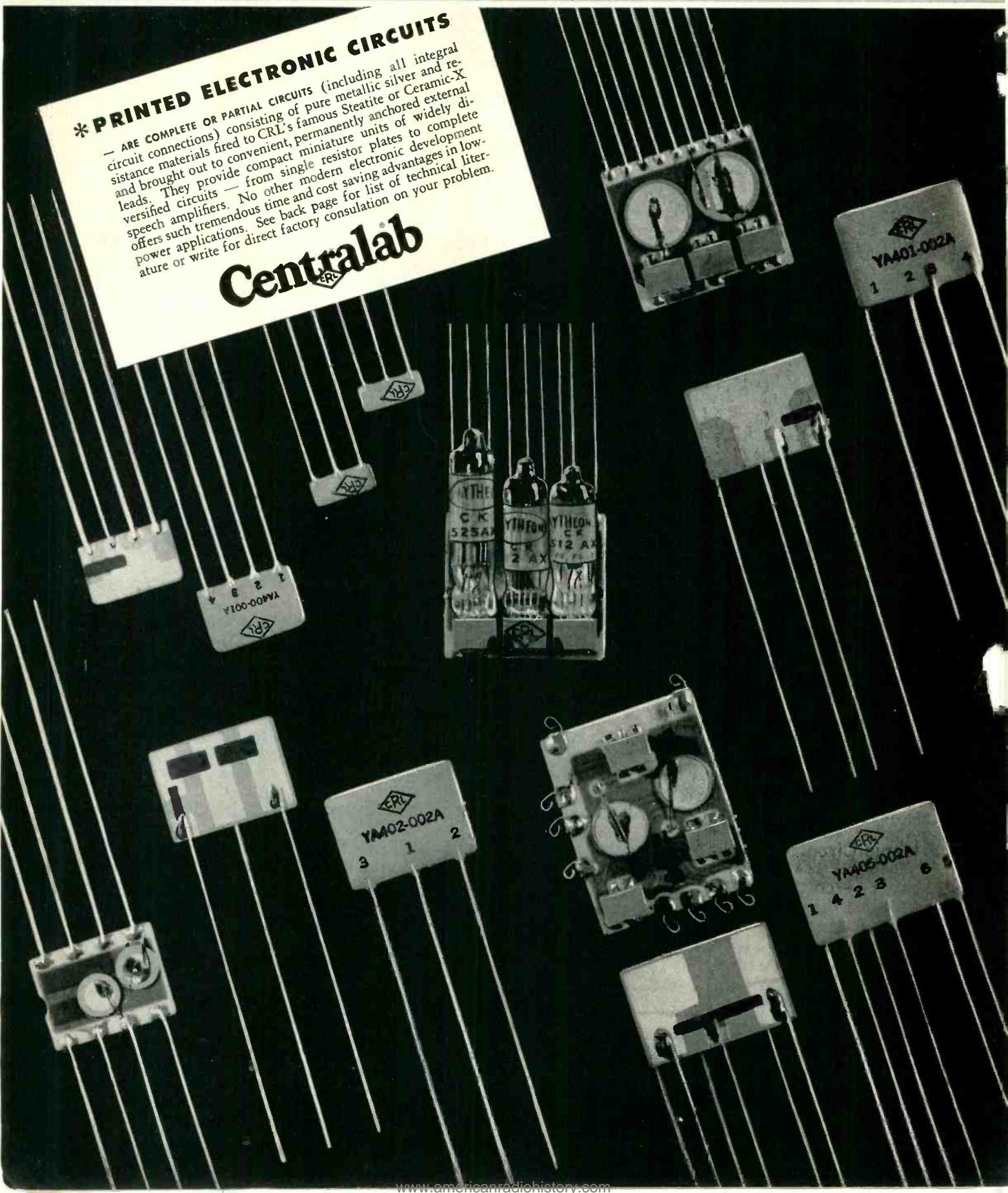
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Use P.E.C.'s * ...

* PRINTED ELECTRONIC CIRCUITS

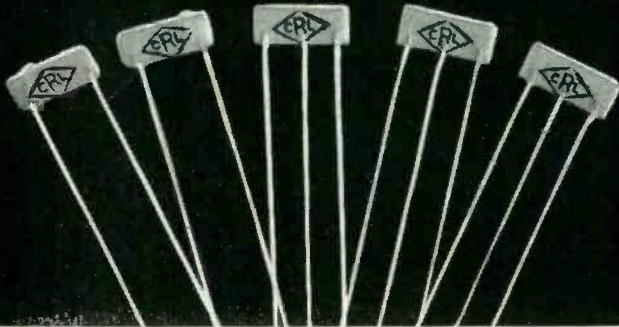
— ARE COMPLETE OR PARTIAL CIRCUITS (including all integral circuit connections) consisting of pure metallic silver and resistance materials fired to CRL's famous Steatite or Ceramic-X and brought out to convenient, permanently anchored external leads. They provide compact miniature units of widely diversified circuits — from single resistor plates to complete speech amplifiers. No other modern electronic development offers such tremendous time and cost saving advantages in low-power applications. See back page for list of technical literature or write for direct factory consultation on your problem.

Centralab

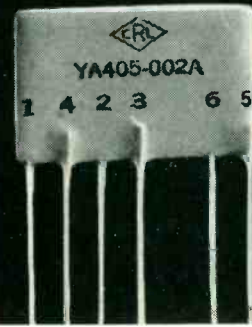


CUT ASSEMBLY COSTS

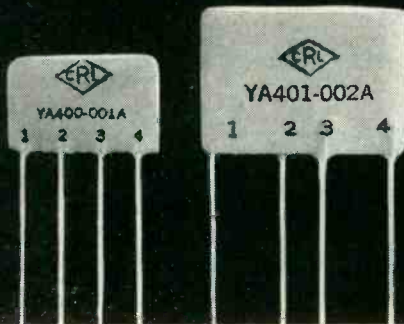
Conserve Resistors



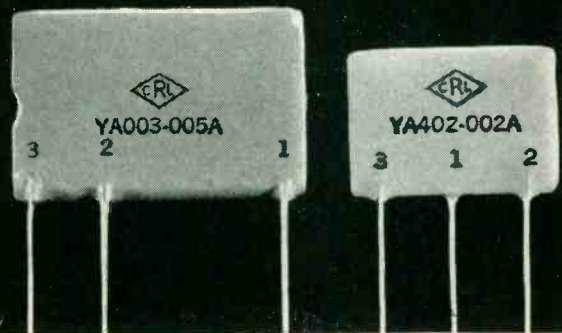
Actual size photo of plate capacitor, resistor, and resistor-capacitor units. Because of size and ease of installation, they easily fit miniature and portable electronic equipment — overcome crowded conditions in TV, AM, FM, and record-player chassis. For complete data, check coupon No. 42-24 — Ceramic Plate Components.



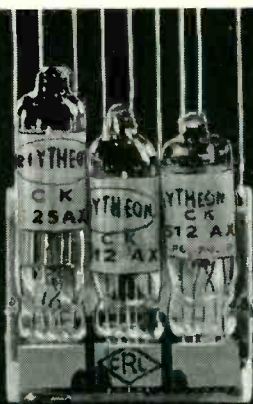
Pentode couplates are complete interstage coupling circuits consisting of 3 capacitors and 3 resistors on a small 6 lead ceramic plate. Compared with old-style audio circuits, they reduce soldered connections 50% — wiring errors accordingly. Big saving in space and weight. For complete data, check coupon No. 999 — Pentode Couplate.



Centrallab Triode Couplates save space and weight, replacing 5 components normally used in audio circuits. They consist of 3 capacitors and 2 resistors bonded to a dielectric ceramic plate. Available in variety of resistor and capacitor values. For complete data, check coupon No. 42-6 — Couplate, and No. 42-27 — Model 2 Couplate.



Centrallab Vertical Integrators give you big savings in assembly costs in TV vertical integrator networks. One type consists of 4 resistors and 4 capacitors brought out to 3 leads . . . reducing formerly required 16 soldered connections to 3! There're less parts handled, too! For complete data, check coupon No. 42-22 — Vertical Integrator.



Ampec is a full 3-stage, 3-tube speech amplifier with amazingly efficient, reliable performance. Size 1 1/4" x 1 1/8" x .340" over tube sockets! Used in hearing aids, mike preamps and similar applications where small size and outstanding performance counts. For complete data, check coupon No. 973 — Ampec.

Centralab

Division of GLOBE-UNION INC. • Milwaukee

TEAR OUT COUPON

for the Bulletins you want

CENTRALAB

Division of Globe-Union Inc.

914 East Keefe Avenue, Milwaukee, Wisconsin

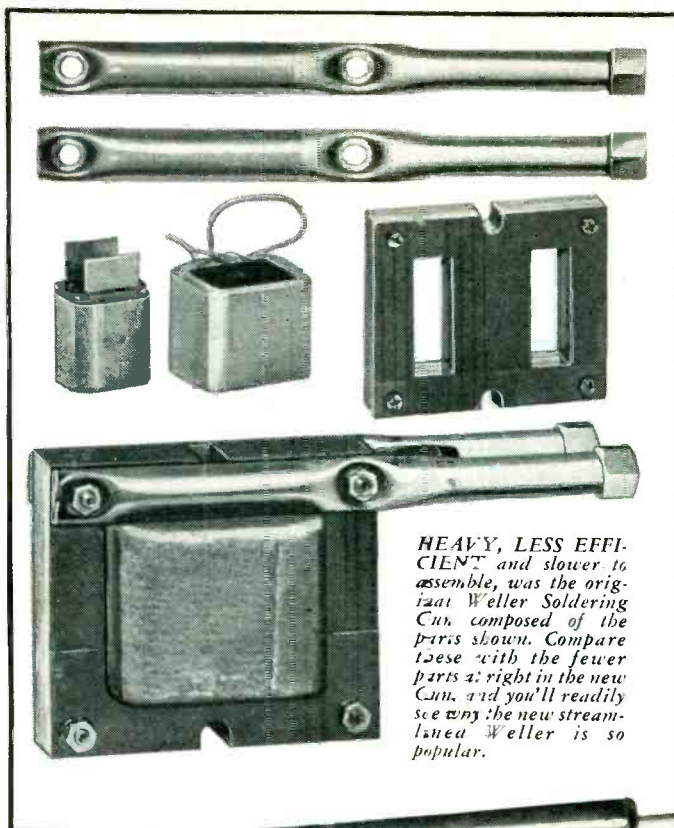
Yes—I would like to have the CRL bulletins, checked below, for my technical library!

42-24 999 42-6 42-7 42-22 973

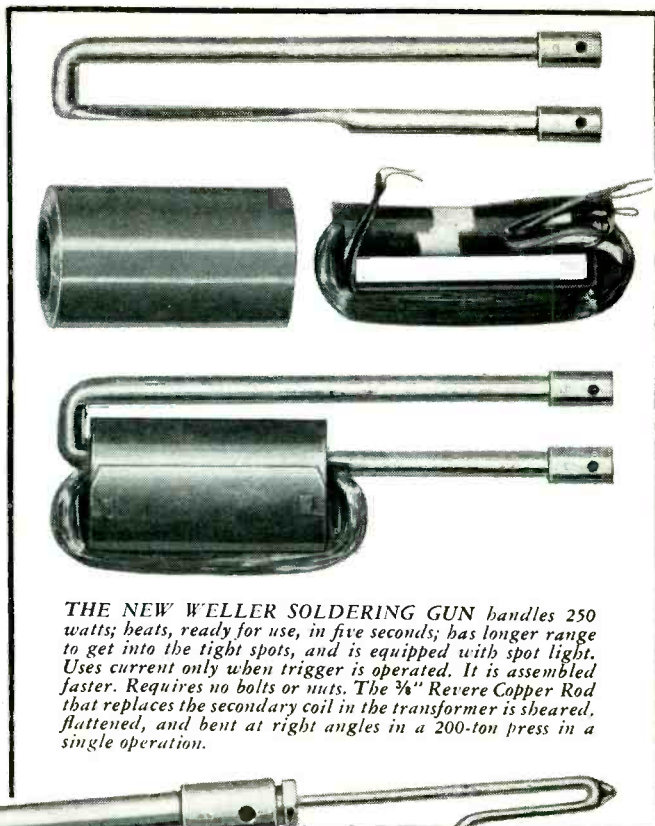
Name.....

Address.....

City..... State.....



HEAVY, LESS EFFICIENT and slower to assemble, was the original Weller Soldering Gun, composed of the parts shown. Compare these with the fewer parts at right in the new Gun, and you'll readily see why the new streamlined Weller is so popular.



THE NEW WELER SOLDERING GUN handles 250 watts; heats, ready for use, in five seconds; has longer range to get into the tight spots, and is equipped with spot light. Uses current only when trigger is operated. It is assembled faster. Requires no bolts or nuts. The 3/8" Revere Copper Rod that replaces the secondary coil in the transformer is sheared, flattened, and bent at right angles in a 200-ton press in a single operation.



COPPER TREATS YOUR PRODUCT BETTER WHEN YOU

Control Your Temper

Revere Copper Rod replaces Secondary Coil in Soldering Gun Transformer . . . reduces number of parts, makes for a speedier, more efficient assembly . . . also makes possible a lighter, more compact unit of increased capacity.

WHEN the Weller Manufacturing Company, Easton, Pa., was completing the development of its new electric soldering gun, they were confronted with this problem: The 3/8" Revere Copper Rod used to replace the secondary coil in the transformer had to maintain its rigidity yet be sufficiently soft so that during the shearing, coining, and bending operations there would be no breaking or splitting of the rod.

Revere's Technical Advisory Service recommended a certain temper copper rod. It was discovered that Weller was getting a twist in the rod when it was installed in the assembled gun. Other tempers were tried

and tested. Then a copper rod of a slightly harder temper than the first was recommended. That was it! Proper temper was the key. Proper temper was also the key to the .291 dia. copper rod used for the Soldering tip itself. For this, too, had to retain its rigidity and yet remain soft enough to be coined, punched, and formed without fracture.

"In addition to being extremely helpful in arriving at the proper tempers, Revere also recommended that we specify our rod in multiple lengths, and thus save considerably on scrap. They were also helpful in solving the problem of attaching the brass sleeve to the secondary rod in

our Soldering Gun," the Weller Manufacturing Company tells us.

So you see, Revere's interest in your problem does not stop with the recommendation of its products. Perhaps Revere can help you. Why not take your current problem to the nearest Revere Sales Office and see?

REVERE

COPPER AND BRASS INCORPORATED

Founded by Paul Revere in 1801
230 Park Avenue, New York 17, New York

Mills: Baltimore, Md.; Chicago, Ill.; Detroit, Mich.; Los Angeles and Riverside, Calif.; New Bedford, Mass.; Rome, N. Y.
Sales Offices in Principal Cities, Distributors Everywhere.



OHMITE

Has Just the Resistor You Need

Ohmite offers fixed, adjustable, tapped, non-inductive, and precision resistors in more than 60 sizes and 18 types of terminals, in a wide range of wattages and resistances.

These rugged resistors have proved their dependability under the toughest conditions. Write on company letterhead for Catalog 40.



Be Right with

OHMITE

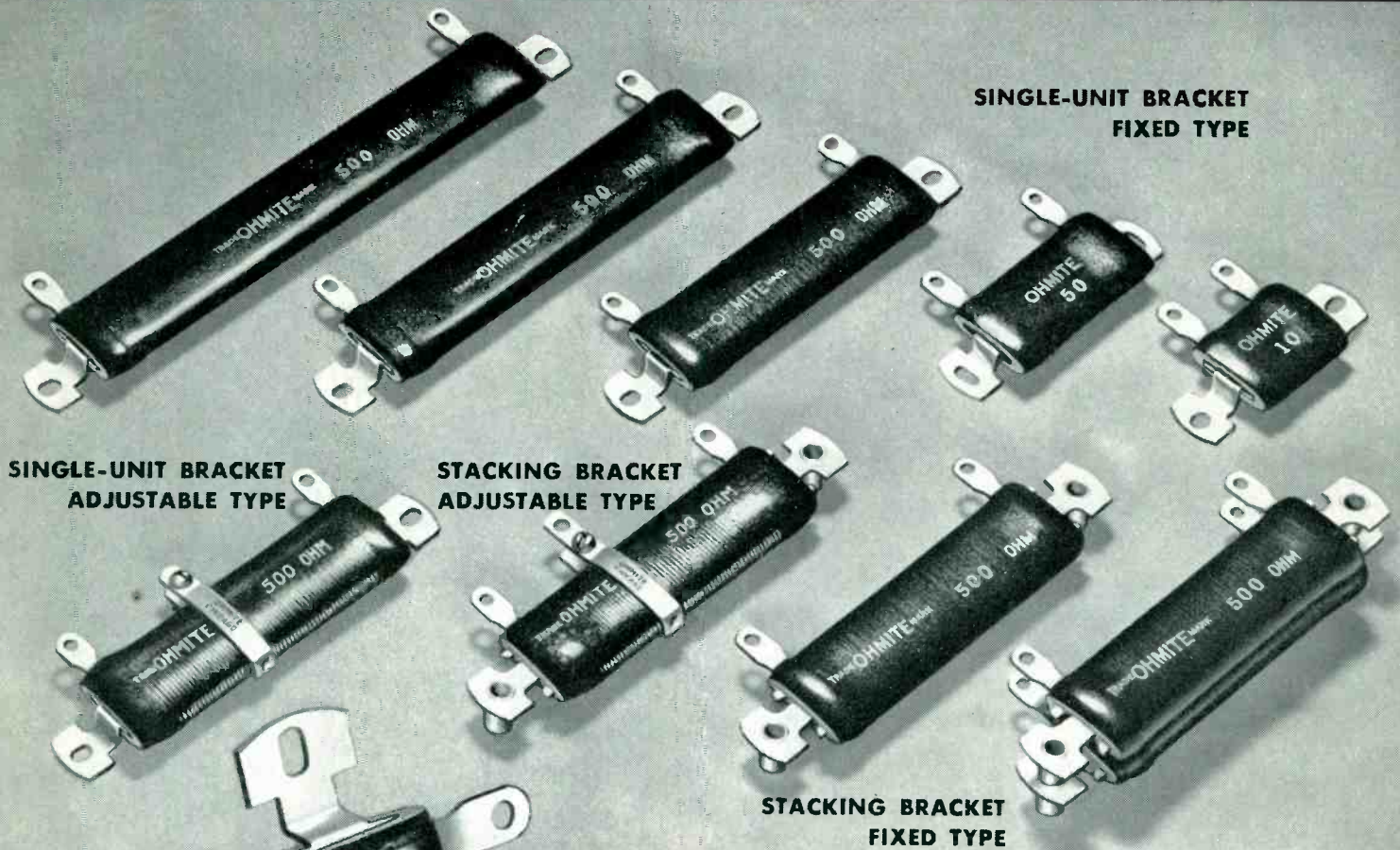
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RHEOSTATS • RESISTORS • TAP SWITCHES

OHMITE MANUFACTURING COMPANY

4816 Flournoy St., Chicago 44, Ill.

OHMITE THIN RESISTORS



SINGLE-UNIT BRACKET
FIXED TYPE

SINGLE-UNIT BRACKET
ADJUSTABLE TYPE

STACKING BRACKET
ADJUSTABLE TYPE

STACKING BRACKET
FIXED TYPE

VITREOUS-ENAMEL COVERING

Winding is rigidly held in place and protected from damage by Ohmite special vitreous enamel.

EVEN, UNIFORM WINDING

"Hot spots" and resultant failures are prevented by the resistance winding's unsurpassed uniformity.

STRONG, CERAMIC CORE

Unaffected by cold, heat, fumes, or high humidity its core provides a strong base for winding.

FIVE WATTAGE SIZES

Lengths range from 1 1/4 inch to 6 inches, corresponding to ratings of 30 to 75 watts.

INTEGRAL MOUNTING BRACKETS

Distribute heat more evenly throughout resistor and conduct heat away quickly.

...PACK HIGHER WATTAGE INTO LESS SPACE

Because of their compact design, Ohmite Thin Type Resistors have a higher wattage rating per unit of space. They provide all the time-proven superiority of conventional Ohmite vitreous-enamel resistors—giving you a compact unit you can depend upon. Available in four types—all only 1/4 inch thick by 1 inch wide—in five lengths and a wide range of resistance values.

Send for Bulletin No. 138

OHMITE MANUFACTURING CO.

4816 W. Flournoy St., Chicago 44, Ill.



Be Right with

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RHEOSTATS • RESISTORS • TAP SWITCHES

*specify
Sorensen*

RANGERS

(FULL-RANGE-VARIABLE DC SUPPLYS)

This versatile supply is a combination of the widely used Sorensen NOBATRON and a filter-variable output circuit.

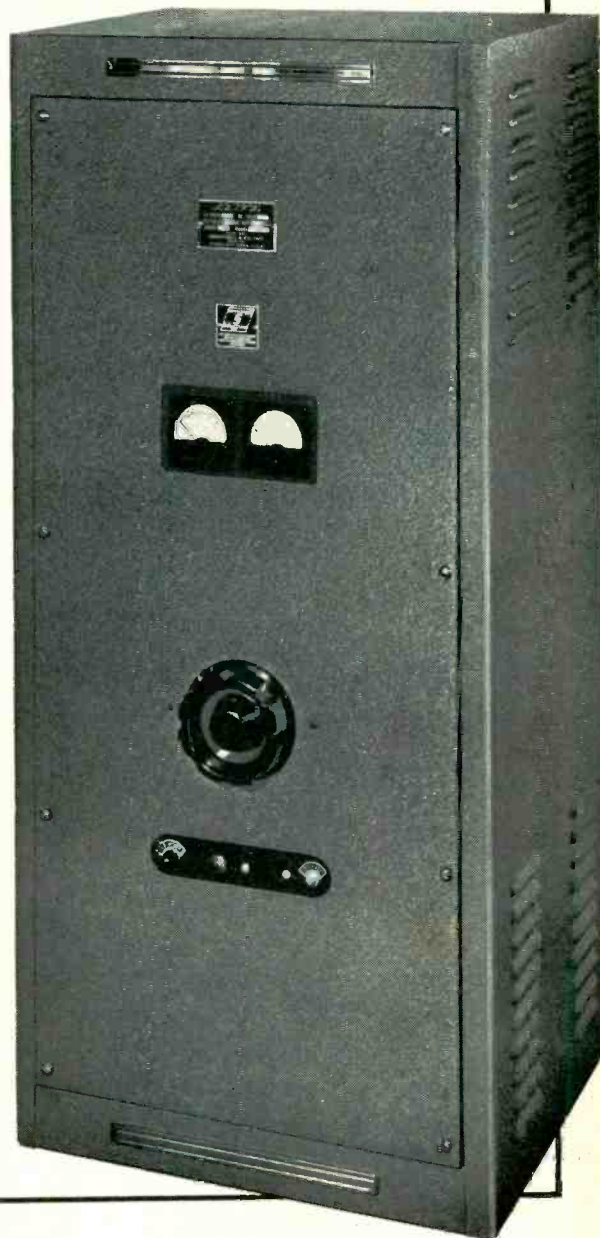
The result gives a continuously variable output voltage regulated against line and load changes through the full range of the instrument.

Look at the specifications tabulated below — check them against your requirements. Where range of output, adaptability to diverse applications is essential, the Sorensen RANGER may well be your instrument of choice.

ELECTRICAL SPECIFICATIONS

Model No.	SR-10	SR-30	SR-50
Output range	0 - 135 VDC	0 - 30 VDC	0 - 13 VDC
Current range	1 - 10 amps	3 - 30 amps	5 - 50 amps
Input voltage	95 - 130 VAC, 50 - 60 cycles, single phase		
Regulation accuracy	± 0.25 percent at any voltage setting from 3 VDC to top rating		
Ripple	RMS max. 1% of output setting		

Meters — standard. Coarse and fine adjustment available.



Write for complete information.

For other regulated DC supplies, investigate Sorensen's line of NOBATRONS (low voltage) and B-NOBATRONS (high voltage).

POWER
controlled converted
POWER

Sorensen

and company, inc.
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TEMFLEX 105

*Longer Life
at 105°C!*

Temflex 105 extruded plastic tubing affords longer retention of flexibility and original insulation characteristics. Use it for higher operating temperatures, for high voltage conductors, for oil-cooled transformers. For details, test reports, samples, write today.

Look to Irvington
for Insulation Leadership



ENDURES HEAT – Temflex 105 is Underwriters' Laboratories approved for continuous operation at 105°C!

SUPERIOR INSULATION – Temflex 105 maintains consistently high dielectric strength!

MOISTURE RESISTANT – Temflex 105 effectively seals out moisture – is Underwriters' approved for use in damp locations!

STRONG, TOUGH – Temflex 105 gives you tensile strength of 3,000 p.s.i. – with minimum elongation of 300%!

FLEXIBLE WHEN COLD – Temflex 105 stays flexible down to temperatures as low as -40°C!

RESISTS CHEMICALS – Temflex 105 shows good resistance to solvents, is unaffected by strong acid or alkali!

WITHSTANDS HOT OIL – Temflex 105 retains flexibility and dielectric properties after prolonged immersion in oil over 100°C!



IRVINGTON


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Irvington 11, New Jersey

FILTRON

RF INTERFERENCE SUPPRESSION

to New Heights
of **NOISE
ELIMINATION**



**FILTRON IS SPECIFIED ON THE
MAJORITY OF MODERN AIRCRAFT,
GUIDED MISSILES, SIGNAL CORPS,
ORDNANCE AND NAVAL EQUIPMENT**

FILTRON will design the right filter for your circuit conditions to meet size, weight and electrical characteristics — and meet RF Interference Suppression Specifications wherever RF Interference must be eliminated.

FILTRON'S advanced engineering, due to constant research and development, together with FILTRON'S production know-how, insures quality components to meet your delivery requirements.

RF INTERFERENCE SUPPRESSION FILTERS FOR:

**Motors
Generators
Inverters
Electronic
Controls**

**Dynamotors
Power Plants
Actuators
Gasoline
Engines**

And other RF Interference producing equipment



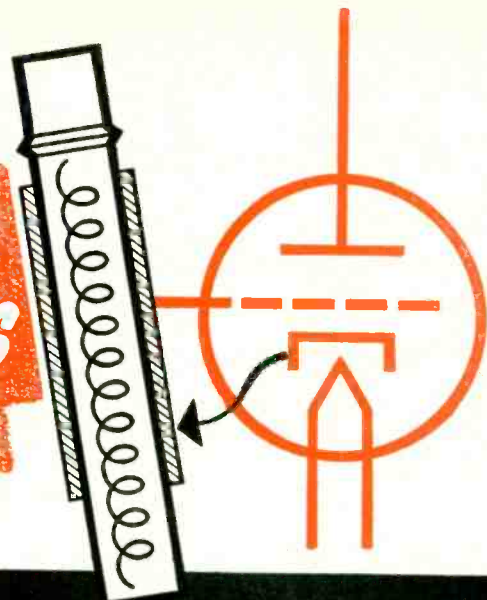
**BOEING B-47
STRATOJET**

An inquiry on your Company letterhead will receive prompt attention

THE FILTRON CO., INC.
FLUSHING, LONG ISLAND, N. Y.

LARGEST EXCLUSIVE MANUFACTURERS OF RF INTERFERENCE FILTERS

Millimeters that do a Mammoth Job with Driver-Harris Alloys

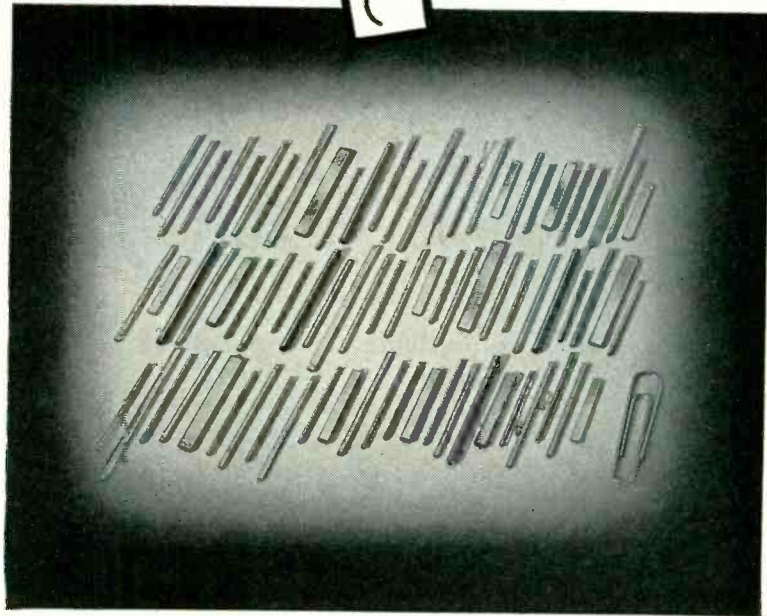


The introduction of the indirectly heated "cathode" brought about revolutionary improvement in the operation of electron tubes for radio and TV reception. It eliminated AC hum in receivers, and actually increased emission at lower filament voltage. Thus tubes became considerably more efficient, and operating life was greatly extended.

And all this as the result of employing a tiny component—customarily measured in millimeters, or very small fractions of an inch!

It stands to reason that an item of such importance as the cathode must be manufactured from materials that are carefully produced to exacting specifications. Superior Tube Company, leading manufacturers of nickel alloy cathodes, specifies Driver-Harris Alloys for both "active" and "passive" cathode base metals. "Active" materials, producing a high level of electron emission, are D-H Alloys 399, 599 and 799; "passive" materials, employed when freedom from grid back-emission is necessary, are D-H Alloys 499 and 999. All are produced free from oxides, and with extreme accuracy as to dimensions, temper and purity. The commercial grade of pure nickel does not meet specifications.

A consideration of major importance is *surface*. The surface of materials used for cathodes must possess sufficient "tooth" to enable coatings of chemical emitters (such as Barium-Strontium Oxide) to adhere successfully—without cracking or spalling. Driver-Harris furnishes the precise type of surface required.



D-H Alloy Cathodes, as produced by Superior Tube Company, Norristown, Pa., are made from thin strip stock, of thicknesses such as .002" and .0025"—handled by patented machines especially developed for the purpose of producing plain or beaded "Lockseam" type nickel cathode sleeves. Basic Dimensions: Max. OD—.100"; Min. OD—.040". Max. Length—42 mm.; Min. Length—11.5 mm. (Compare with paper clip.)

Here is but another example of the tremendous role played by D-H Alloys thruout industry—and the ability of Driver-Harris to produce *special alloys for special purposes*.

Whatever *your* particular alloy problem, let us have your specifications. We'll gladly put our specialized knowledge, and the skills acquired from fifty years of alloy manufacturing experience, at your disposal . . . make recommendations based upon your specific needs.



Manufacturers of world-famous Nichrome* and over 80 other alloys for the electronic, electrical and heat-treating industries

Driver-Harris Company

HARRISON, NEW JERSEY

BRANCHES: Chicago, Detroit, Cleveland, Los Angeles, San Francisco

*T.M. Reg. U. S. Pat. Off.

January, 1951 — ELECTRONICS

Choose JOHNSON Variable Condensers For *DEPENDABLE EFFICIENCY*

Excellent design, careful workmanship and quality materials are combined in the manufacture of JOHNSON Variable Condensers to assure highest stability of the tuned circuit.

The entire JOHNSON line features high quality steatite insulation and sturdy construction — your assurance of long, dependable service.

Type
G&D

Unusually economical for quality condensers, Types C and D have .051" thick, rounded aluminum plates, large laminated rotor brushes. Air gap from .080" to .250" (Type D) and .125" to .500" (Type C). Panel space, Type C, 5½" W x 5¾" H. Type D, 4¼" W x 4" H.

Type
E&F

Rugged, compact units for low and medium power transmitters. Aluminum plates .032" thick, rounded edges. Stainless steel shafts. Air gap from .045" to .125" (Type E) and .045" or .075" (Type F). Panel space, Type E, 2¾" square; Type F, 2-1/16" square.

Type
M

MINIATURE — SMALLEST EVER BUILT!
Ideal for VHF, miniature test equipment, etc. Soldered construction, silver plated beryllium copper contact spring, split sleeve rotor bearings — no shaft wobble. Made in single and differential models up to 19.6 mmf and butterfly up to 11 mmf. Panel space only ⅝" x ¾". Air gap .017".

Type
L

Ceramic soldered — no eyelets or rivets to loosen. All brass, soldered construction. "Bright alloy" plated. Ideal for rough service. Beryllium copper contact spring, silver plated. Made in butterfly, single and differential types. Panel space 1 ⅜" square. Air gap .030". Also furnished in .020", .060" and .080".

TYPE N
Small mounting space requirements, extremely high voltage rating and fine adjustment make these neutralizing condensers ideal.

TYPE G
Extremely popular as neutralizing condensers for medium and low power stages. Also widely used for grid and plate tuning at high frequencies.

WRITE TODAY FOR JOHNSON CONDENSER CATALOG!

TYPE BC . . . for Commercial and Broadcast use
where high voltage, high current conditions prevail.



New aluminum die cast plates have heavy beaded round outer edge for maximum voltage breakdown. Cast aluminum end plates, with rounded edges, rugged steatite insulators with long creepage path. Width 7⅞", height 7-5/16". Voltage ratings up to 18,000 volts peak breakdown.

Many other types, including pressurized units, are made for high voltage, high power applications.

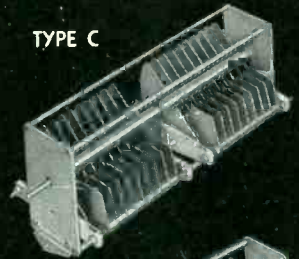


JOHNSON a famous name in Radio

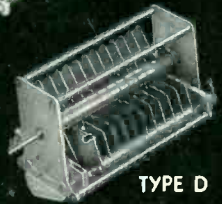
E. F. JOHNSON CO.

WASECA, MINN.

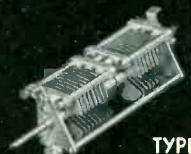
TYPE C



TYPE D



TYPE E



TYPE F

TYPE M



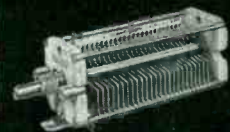
SINGLE



BUTTERFLY



DIFFERENTIAL



TYPE L SINGLE



TYPE L BUTTERFLY



TYPE N



TYPE G



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Transformers

COILS

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Conventional and *Hermetically Sealed Types*

IT'S EASY... Simply submit your
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IF you desire a sample built to your
specifications, it can be made for
you in a short time.

SEND B/P FOR COST-FREE RECOMMENDATIONS

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C O R P O R A T I O N

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NEW INDICATOR ION TRAP

*A
Rauland
"Exclusive"*



Helps you Cut Production Costs

Rauland's new Indicator Ion Trap can help you in your battle to cut pennies off production costs and thereby to price receivers competitively.

First of all, the Indicator Ion Trap completely eliminates the need for any equipment and any trained judgment in the adjustment of ion trap magnets. Adjustment can be made faster than equipment could be attached. The ion trap magnet is simply moved until the green glow signal is reduced to minimum. It can be done in seconds with absolute accuracy—without even seeing the front of the picture tube.

Second, the Rauland Tilted Offset Gun which incorporates this Indicator Ion Trap requires only one Ion Trap Magnet instead of two, nibbling a little more off production costs. Yet it gives better results—the electron beam is bent only once and is focused to maximum sharpness.

Specify Rauland tubes with these exclusive advantages, and get the benefits that only Rauland offers. For further information, write to...

RAULAND

The first to introduce commercially these popular features:

Tilted Offset Gun

Indicator Ion Trap

Luxide (Black) Screen

Reflection-Proof Screen

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Perfection Through Research

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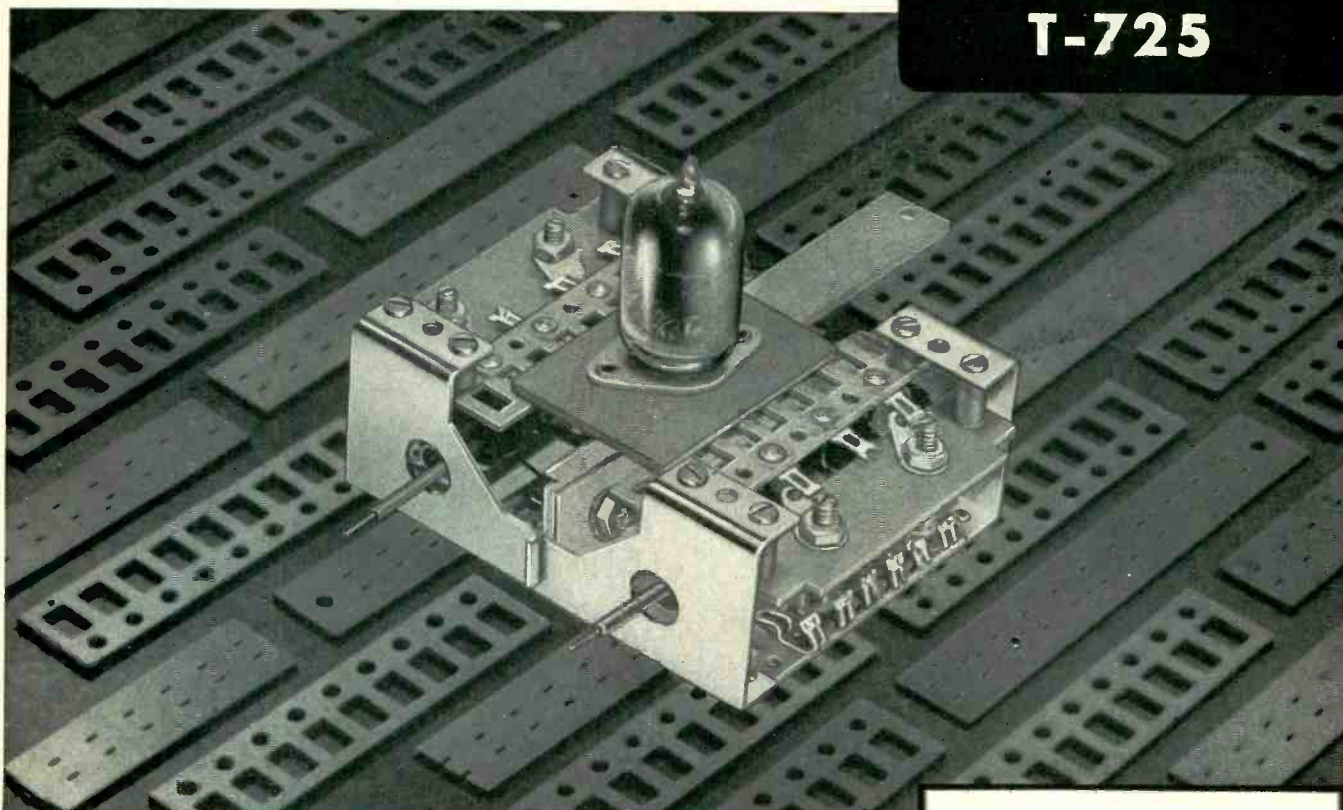


Another

"DESIGN HEADACHE"

solved by

INSUROK*
T-725



Centralab[†] required a superior combination
in the insulation for this unique slide switch
used in Anchor Radio's TV preamplifier

At the high frequencies encountered in TV equipment, insulating materials must possess a unique combination of many properties. To find such a material for its intricate slide switches, used in Anchor Radio's TV preamplifier, was the problem faced by Centralab engineers.

INSUROK T-725 laminated plastic insulation proved to be the answer. It had the necessary physical strength

and electrical properties. It was stable under elevated temperatures and high humidity. And, from piece to piece, it remained uniform.

In hundreds of similar applications, laminated and molded INSUROK are solving difficult problems for industry. Richardson's years of experience in the engineering application of plastics are available to you without obligation. Write, today.

1. Uniform quality
2. Low electrical loss
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6. Close tolerances

*Reg. U. S. Pat. Off.

†DIVISION OF GLOBE-UNION INC., MILWAUKEE

The RICHARDSON COMPANY

FOUNDED IN 1858—LOCKLAND, OHIO

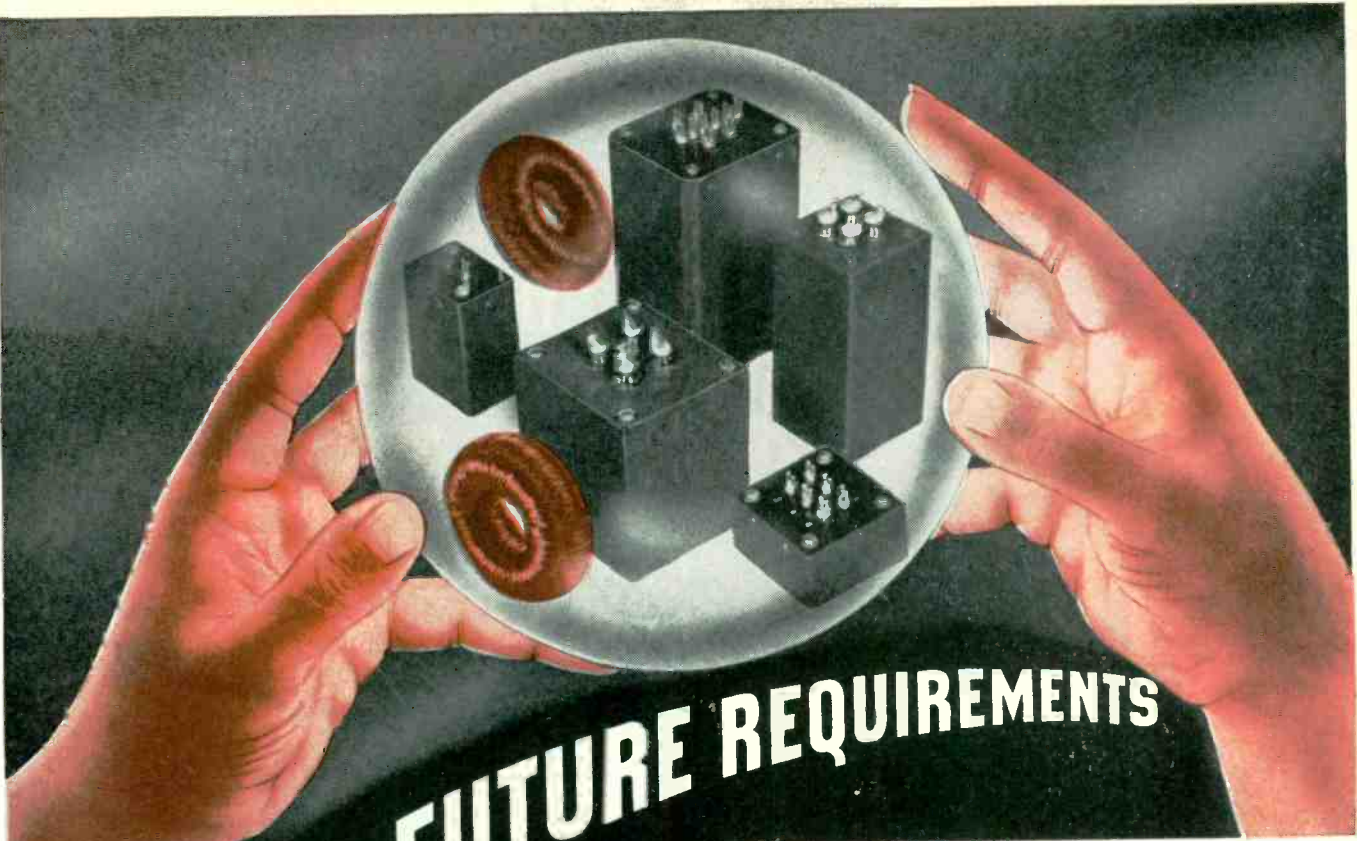
Lake St., Melrose Park, Illinois (Chicago District)

Write for

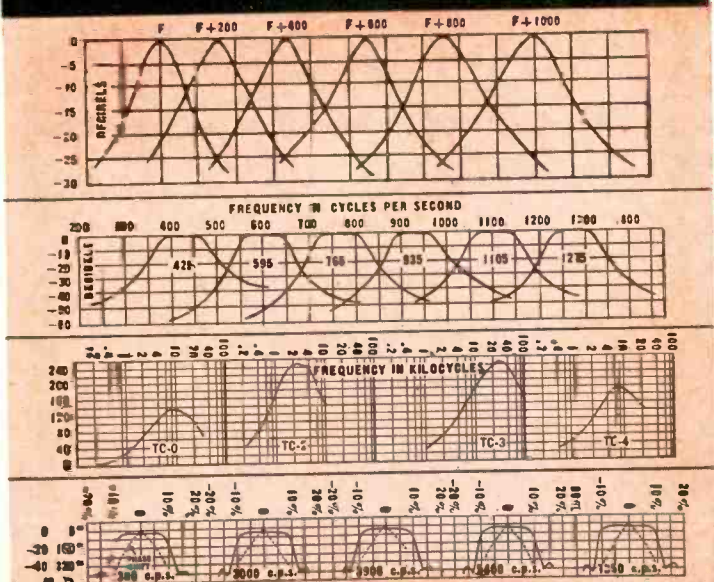
Descriptive
Data Sheet T-725



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YOUR FUTURE REQUIREMENTS IN TOROIDAL COILS and FILTERS OUR PROBLEM.. TODAY!



We do not lay claim to any special powers of prognostication, but we can compare ourselves to the seasoned hunter or veteran sailor in their ability to sense the way the wind is blowing. By maintaining constant vigil of the Horizon in our Industry, we strive to be well prepared to meet the ever changing requirements for high quality filters. In following this policy we have been able to give you 'Yes' or 'No' answers on the spot to your queries of 'is this practical' or 'can this be done?' If it can be done, we have probably tried it. If it cannot be done we are still trying to do it. This has obviated unnecessary expenditure of our customers' time and money, and has helped expedite the development of new equipment by eliminating the several blind alleys that can be so costly. In these times, especially, the continued application of foresight, ingenuity and new ideas, as well as the constant expansion of production facilities, will be the key note of our 'Burnell Customer Service.'

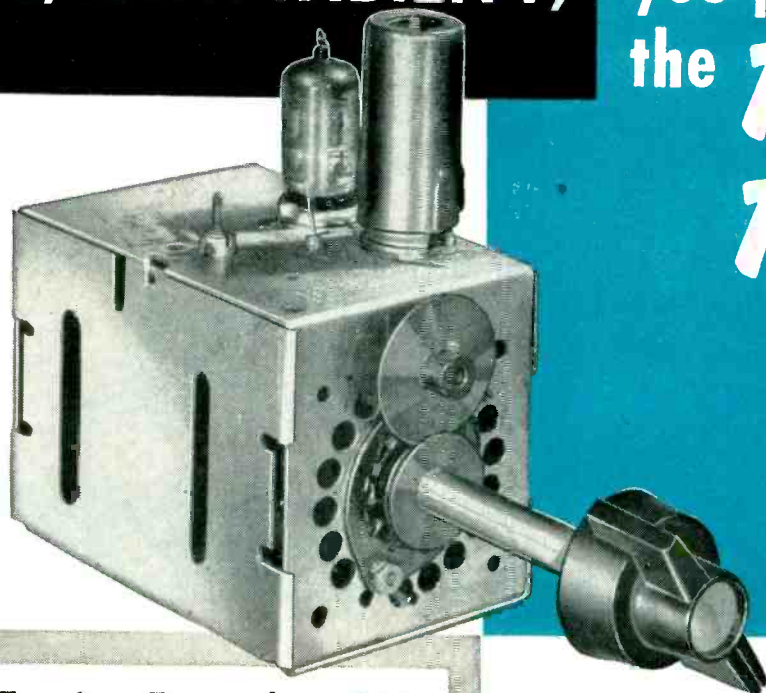
Exclusive Manufacturers of
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YONKERS 2, NEW YORK
CABLE ADDRESS "BURNELL"

**For PERFORMANCE,
PRICE, ADAPTABILITY,**

**you just can't beat
the *Tarzian
Tuner!***



A compact, precision-built "package," offering maximum performance per dollar cost. And, backed by TARZIAN engineering "know-how."

**Only Tarzian Tuner has ALL
of these desirable Features**

- Low oscillator radiation
- High gain and low noise
- Designed for 21 or 41 megacycle I.F. systems
- Insulated shaft design available at low cost
- Anti back lash, air dielectric fine tuning, giving uniform coverage on low and high channels
- Three tube performance with two tubes
- Each channel individually aligned for maximum performance
- Good input balance—no tracking difficulties
- Completely shielded
- Oscillator tube shield provides rigid horizontal and vertical positioning of the tube
- Extra terminals provided for tie-points

Write for complete information,
specifications and technical data.

- Since the time it was first introduced, the TARZIAN front-end tuner has won the acclaim of the industry. It is small, skillfully designed, well-built and low-priced. That's why 17 of the nation's set manufacturers today are specifying the TARZIAN tuner as a component for their products.

Engineering service available
upon request

Sarkes Tarzian, inc.

TUNER DIVISION, DEPT. E-1

537 South Walnut Street • Bloomington, Indiana

**The SARKES TARZIAN
stations in Bloomington**

WTTS - WTTV

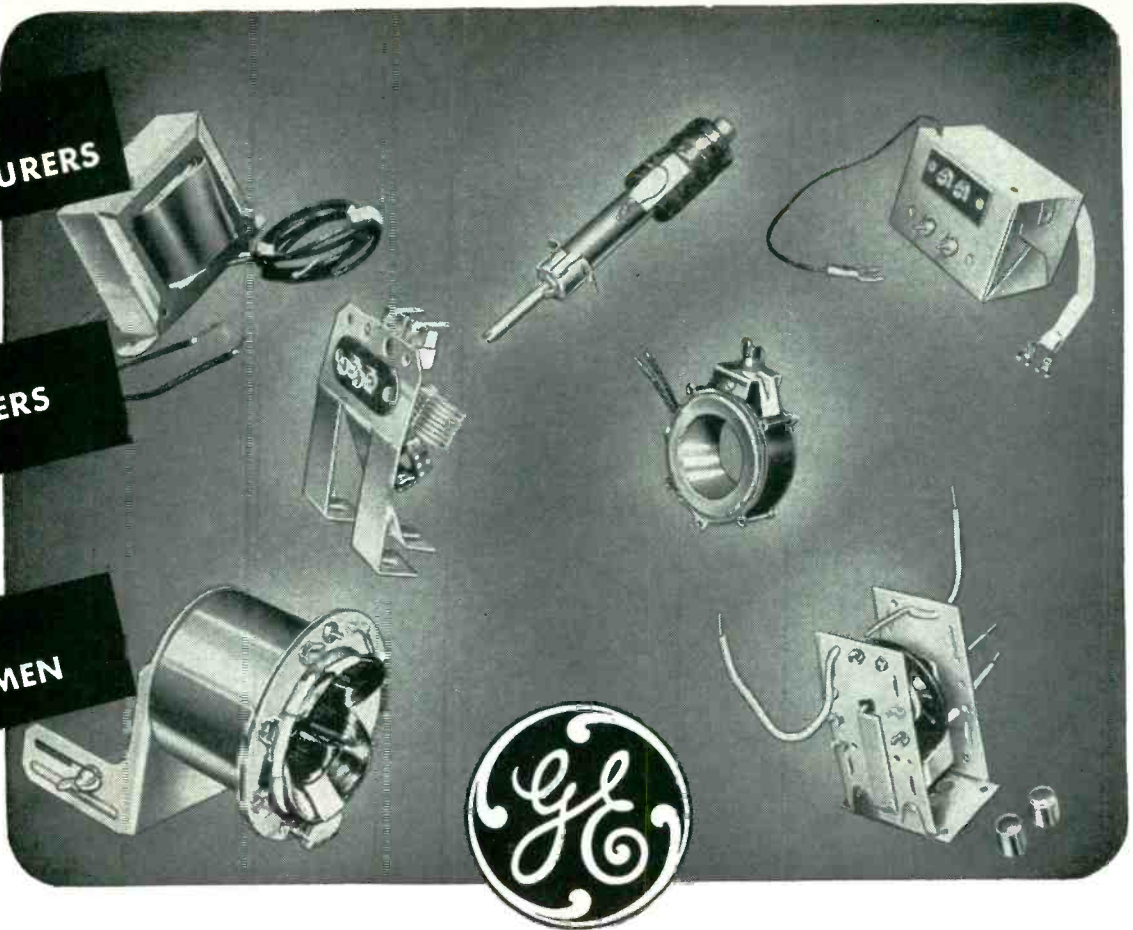
5000 Watts

Channel 10

TV
MANUFACTURERS

TV DEALERS

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Available Now! CRITICAL TV COMPONENTS

DEALERS AND SERVICEMEN—Your share of today's multi-million dollar TV replacement market is limited only by your ability to handle it. Now you can get *ferrite transformers, ferrite core yokes, linearity controls, focus coils*—the vital TV components you need—from one dependable source—General Electric! Don't wait to cash in on the biggest *new* business in television history—call your distributor today and stock the General Electric line!

RECEIVER MANUFACTURERS—Here's a way to cut production headaches and manufacturing costs! You simplify ordering and delivery when you design G-E components into your sets. Remember, too, that your sets will be serviced *in the field* because G-E distributors and dealers everywhere stock these parts. Let us review your requirements for next year's production right now. General Electric application engineers are at your service.

GENERAL  **ELECTRIC**



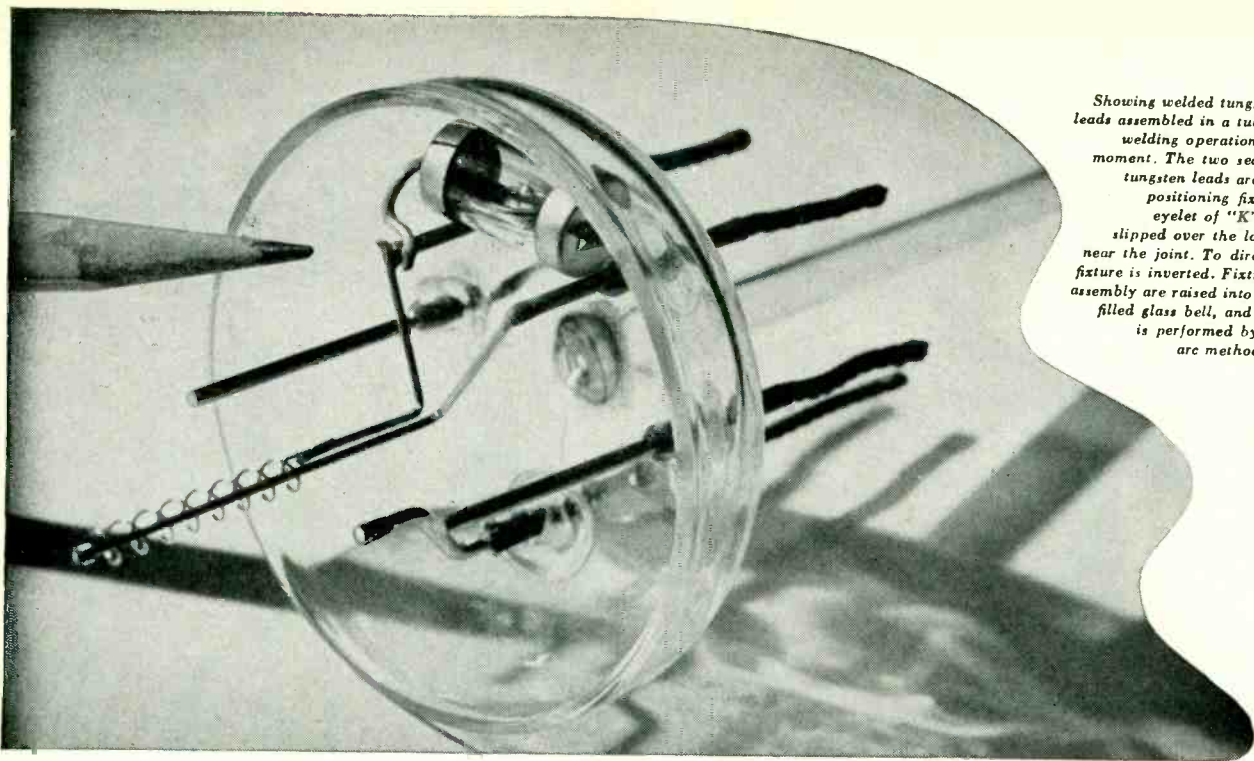
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FOR NEW
FREE
CATALOG

General Electric Company, Section 411
Electronics Park, Syracuse, New York
Rush me the new G-E Catalog of TV Components.

NAME.....

ADDRESS.....

CITY.....STATE.....



Showing welded tungsten filament leads assembled in a tube base. The welding operation takes but a moment. The two sections of the tungsten leads are placed in a positioning fixture. A tiny eyelet of "K" MONEL is slipped over the lower section, near the joint. To direct flow, the fixture is inverted. Fixture and lead assembly are raised into a hydrogen-filled glass bell, and the welding is performed by the carbon arc method.

How a problem in welding tungsten was solved

While improving the design of their VHF beam tetrodes, the United Electronics Company ran into a difficult technical problem.

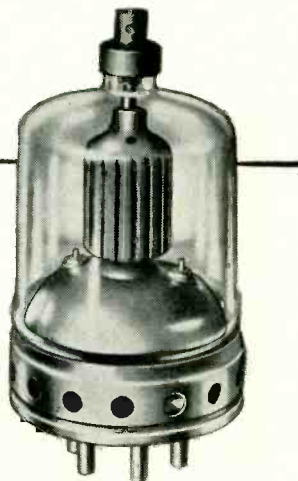
In their tube types 5D22 and 4D21, tungsten filament leads are brought out to conventional base prongs. However, to locate the filament at the center of the structure, the two internal filament leads had to be sharply offset. It was necessary, also, that the leads be accurately aligned with the base outlet holes, to eliminate stresses which might crack the glass envelope when the tube was put in service.

Bending the tungsten leads to shape proved too inaccurate a method. So it was decided to make the leads in two sections — one straight, and one bent — welding them together in precision positioning fixtures.

This method of assembly proved satisfactory, but difficulty was immediately encountered in finding a suitable joining metal.

Several metals were tried without success. Either they failed to "wet" the tungsten, or caused it to embrittle.

VHF beam tetrode tube, manufactured by the United Electronics Co., Newark, N. J.



Finally, United Electronics Company engineers tried "K"® MONEL—and it proved to be the answer to their problem.

"K" MONEL "wet" the tungsten satisfactorily; flowed well; made strong, smooth joints; was resistant to oxidation and corrosion. In addition, "K" MONEL's melting point was safely above both exhausting and tube operating temperatures.

* * *

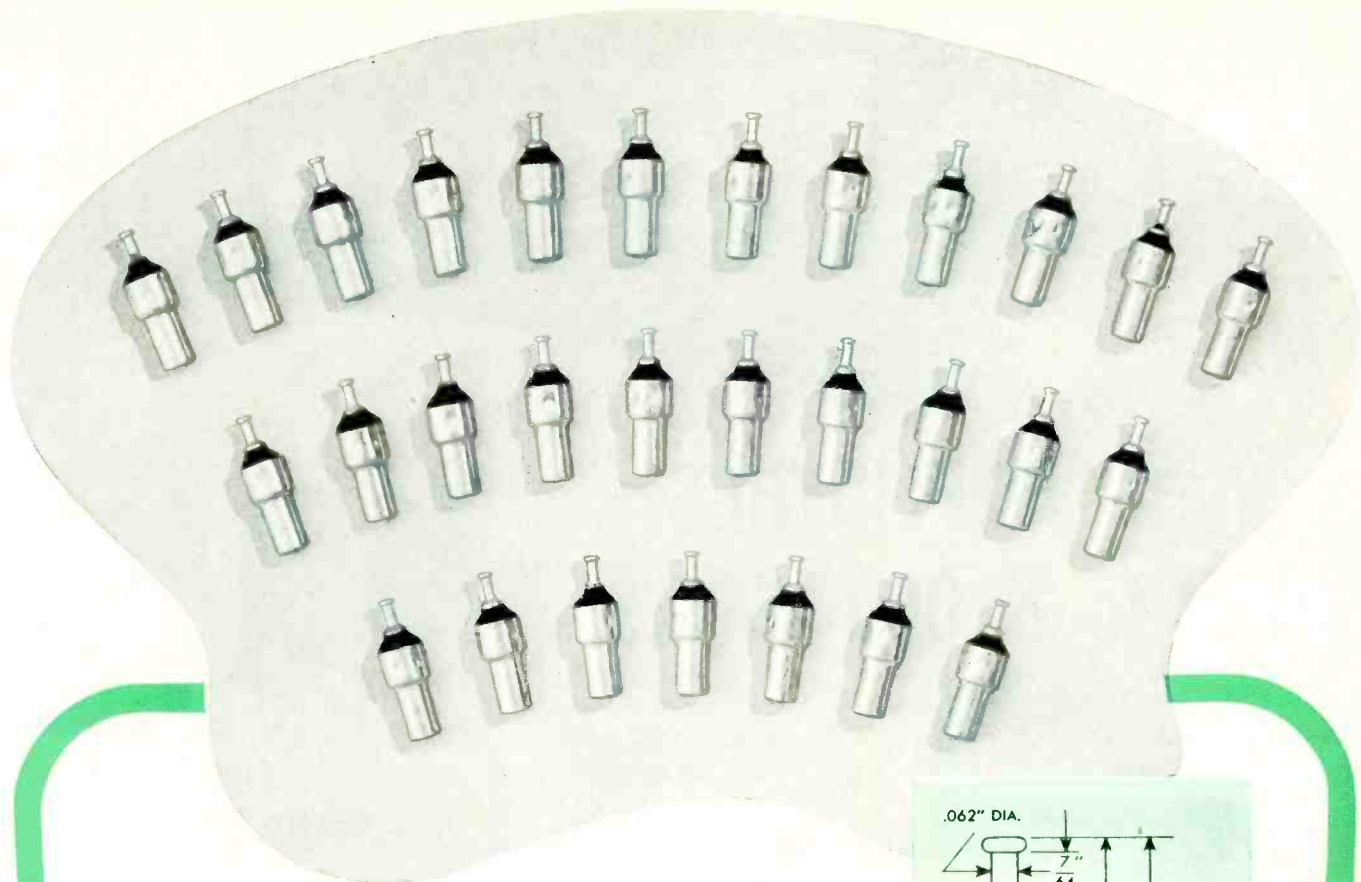
If you have a problem in metal selection, get to know the family of INCO Nickel Alloys with their unique combination of properties. Our technical department is always ready to assist you. Write for "66 Practical Ideas for Metal Problems in Electrical Products."

The International Nickel Company, Inc.

67 Wall Street • New York 5, N.Y.

EMBLEM OF SERVICE
NICKEL  **ALLOYS**

MONEL • "K" MONEL • "S" MONEL • "R" MONEL • "KR" MONEL • NICKEL • LOW CARBON NICKEL • DURANICKEL • INCONEL • INCONEL "X"

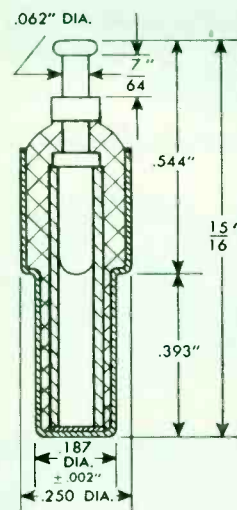


ERIE STYLE 325 . . . A Rugged Stand-Off . . . Quickly Installed . . . Makes a Neater Chassis . . . Provides Uniform, Efficient By-passing

Manufacturers of TV and other high frequency receivers have welcomed the Erie Type 325 Ceramicon because its distinctive features give the answer to many production problems. Consider these advantages:

- 1 For the first time in a hermetically sealed case, a by-pass to ground is provided through the shortest possible path, by taking advantage of the concentric cylindrical electrode configuration and making connection to the outer shell at the plane of the chassis.
- 2 The design provides extremely low and uniform series inductance and effective v.h.f. by-pass.
- 3 In assembly operations terminals and lead lengths are fixed, resulting in better mechanical uniformity.
- 4 High speed assembly is facilitated through use of a standard push-on clip. For more critical applications shell may be soldered directly into a hole in the chassis.
- 5 Post terminal matches tube socket terminal height to maintain uniform short leads, and provides a sturdy tie point for several connections.
- 6 Unusual mechanical ruggedness minimizes danger of breakage in installation and in use.

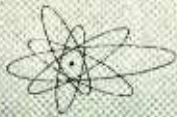
Available in 10, 33, 47, 68, 82, 100, 680, 1,000 and 1,500 MMF capacity. 500 Volts D. C. working.



Electronics Division

ERIE RESISTOR CORP., ERIE, PA.
LONDON, ENGLAND • • TORONTO, CANADA





Designers



AMPLIDYNES— 500 to 25,000 WATTS

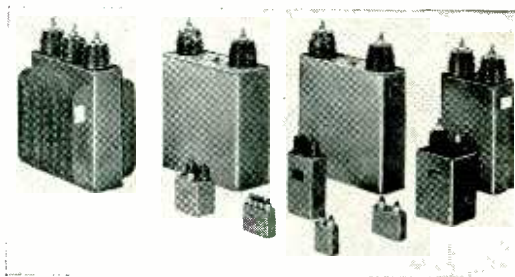


▼ 5-kw Amplidyne generator

▲ 1-kw Amplidyne motor-generator set.



◀ 3-kw Amplidyne motor-generator set



PULSES —MADE TO ORDER

Specially designed General Electric Type-E networks will generate pulses within ± 5 per cent of any length you require from 0.1 to 40 microseconds. These networks consist of capacitor and coil sections adjusted to close tolerances and hermetically sealed in single metal containers. In the last war G-E Type-E networks were produced on a large scale to meet radar demands. Now they are available for commercial or military use in a wide variety of designs, impedances, ratings, and sizes. See Bulletin GEA-4996.

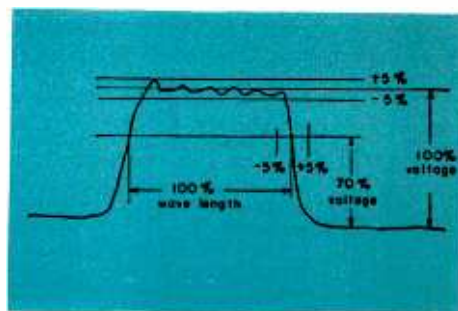
**PRECISE CONTROL OF position • torque • speed
tension • power factor • voltage • current**

The General Electric amplidyne is a simple d-c generator which, through the arrangement of field and armature circuits, possesses extremely high speed of response and amplification.

First used in radar and fire-control apparatus, it now has many new jobs. That's why G-E amplidyne generators and motor-generator sets are made in a wide variety of sizes and frames with output ratings from 500 watts to 25 kilowatts.

What are your requirements? For further data, write, giving complete details, to *Electrical Industries Sec., Resale Industries Div., Apparatus Dept., General Electric Co., Schenectady 5, N. Y.*

A G-E 25-KW AMPLIDYNE AMPLIFIES A 9/10 WATT INPUT 22,200 TIMES

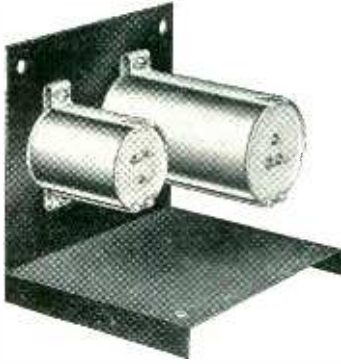


Typical design and operational limits of G E Type-E pulse-forming network: Ripple at top of pulse $\pm 5\%$; Wave length $\pm 5\%$ measured at 70% amplitude; Capacitance tolerance $\pm 10\%$

GENERAL ELECTRIC

Digest

TIMELY HIGHLIGHTS
ON G-E COMPONENTS



OIL-IMMERSED SELENIUM RECTIFIERS —use them "ANYWHERE"!

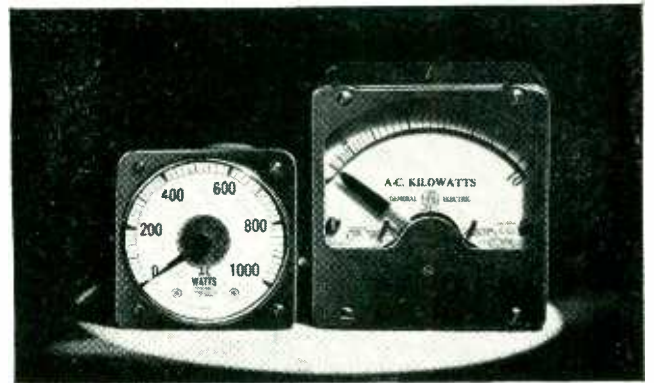
G-E hermetically sealed, oil-immersed selenium rectifier stacks make it possible for you to design metallic rectifiers into equipment that will be subjected to corrosive fumes, salt air, dust, fungus, or other atmospheric conditions. Because they're immersed in oil, these stacks will stand higher current drains than equivalent-size "open" units. Available in single- or full-wave circuits. Ratings: from 12 to 180 d-c volts output, 15.5 to 270 a-c volts input, .25 to 27.0 d-c amps. Write for complete data on ratings and dimensions to *Electrical Industries Section, Resale Industries Division, Apparatus Dept., General Electric Co., Schenectady 5, N. Y.*



PUSH-BUTTON STATIONS—make your selection from the COMPLETE G-E LINE

There's a General Electric push-button station or unit for virtually any electronic application. The complete line includes dozens of types. All stations have sturdy nonbreakable steel frames and covers with ample clearance between terminals. G-E units for built-in applications have terminals anchored to a molded base for firm support. Contact maintenance on all stations and units is virtually unnecessary because large fine-silver double-break contacts are used. For full data, check Bulletin GEA-3469.

NEW! SHADOW-PROOF DIALS MAKE SWITCHBOARD INSTRUMENTS EASIER-TO-READ



Here is a new switchboard instrument that can be read easily—anytime. Its dial can be clearly illuminated from almost any angle because it is set forward flush with the front of the case. A protruding anti-glare convex-type glass front prevents reflections. The new meter is available in 4¼- or 8¾-inch models, both with long 250-degree scales. D-c ammeters, volt-ammeters; a-c ammeters, volt-meters, wattmeters, frequency and power-factor meters, temperature indicators, and synchroscopes. Send for Bulletin GEC-218.

General Electric Company, Section 667-10
Apparatus Department, Schenectady 5, N. Y.

Please send me the following bulletins:

- (V) Indicate for reference only GEA-3469 Push-button stations
(X) for planning an immediate project GEA-4996 Pulse-forming networks
 GEC-218 Switchboard instruments

Name _____

Company _____

Address _____

City _____ State _____

flexite

APPROVED
by the
UNDERWRITERS
LABORATORIES
under their reexamination service

ABOVE 105° C

**the flexible,
extruded plastic tubing
that resists high temperatures**

YES, FLEXITE is the electrical insulation tubing that sets new standards for resistance to extreme high temperatures. Compounded of a plasticized copolymer of vinyl chloride and vinyl acetate and manufactured with a true wall thickness, smooth inside and outside, FLEXITE PLASTIC TUBINGS offer the greatest resistance to high and low temperatures, are extremely flexible and have great tensile strength. FLEXITE compares more than favorably with tubings of similar nature. Check the specifications of FLEXITE, compare them with the requirements for your products and against other insulations for identical use . . .

YES, you will find that FLEXITE sets a new high standard for protection against high temperatures, high dielectric, stretching, tearing, abrasion, exposure to acids, oils and alkalis, flammability, etc. — samples and additional information will be sent upon request. **And for a Plastic Tubing to Withstand Normal High Temperatures Mitchell-Rand Offers Flexite-Norm . . . write for specifications.**

flexite		physical & electrical properties	
a. tensile strength, minimum average	2500 PSI	Colors	Black, white, red, green, yellow and blue are standard colors.
b. ultimate elongation, min. average	300%	Dimensions and Tolerances	Standard sizes to fit B & S wires #20 to #0 inclusive, as specified by ASTM Spec. D922-47T.
c. dielectric strength, minimum	800 v/mil	Wall Thickness	In accordance with ASTM Spec. D922-47T, as follows: #20 — #10 incl. — .016" ± .003" #9 — #0 incl. — .020" ± .003"
d. flammability	non-inflammable	Standard Lengths	Standard 36" lengths, or continuous lengths in coils. Sizes #20 — #10 incl. will be supplied on paperboard spools when so ordered.
e. heat resistance	After 100 hrs. at 300° F. the tubing is not brittle and when flexed does not crack.	Quality	Uniform in quality and condition, smooth on both inside and outside, free of defects such as pin-holes, blisters, foreign inclusions and other imperfections.
f. heat endurance	Recommended for continuous operating temperatures up to 105° C., and when baked at 125° C. for 2,000 hours does not become brittle.	Test Methods	Properties enumerated in above specifications shall be determined according to Tentative Methods of Testing Non-rigid Polyvinyl Tubing, American Society for Testing Materials, Designation D876-46T.
g. low temperature flexibility	-30° C.		
h. heat shrinkage	ASTM Standards #20 — #17 incl. — less than 8% #16 — #6 incl. — less than 5% #5 and larger — less than 3%		
i. oil resistance	Highly resistant to effects of transformer and lubricating oils, does not stiffen when continuously exposed to them.		

WHATEVER YOUR ELECTRICAL INSULATION PROBLEM MITCHELL-RAND HAS THE ANSWER
And for a Plastic Tubing to Withstand Normal High Temperatures Mitchell-Rand Offers • Flexite-Norm • write for specifications.

M-R THE
ELECTRICAL
INSULATION
HEADQUARTERS
FOR 61 YEARS.



MITCHELL-RAND INSULATION CO. Inc.

51 MURRAY STREET • CORLANDT 7-9264 • NEW YORK 7, N. Y.

A PARTIAL LIST OF M-R PRODUCTS: FIBERGLAS VARNISHED TUBING, TAPE AND CLOTH • INSULATING PAPERS AND TWINES • CABLE FILLING AND POEHEAD COMPOUNDS • FRICTION TAPE AND SPLICE • TRANSFORMER COMPOUNDS • FIBERGLAS SATURATED SLEEVING • ASBESTOS SLEEVING AND TAPE • VARNISHED CAMBRIC CLOTH AND TAPE • MICA PLATE, TAPE, PAPER, CLOTH, TUBING • FIBERGLAS BRAIDED SLEEVING • COTTON TAPES, WEBBINGS AND SLEEVINGS • IMPREGNATED VARNISH TUBING • INSULATED VARNISHES OF ALL TYPES • EXTRUDED PLASTIC TUBING

America's Road to Victory

... Let's Increase Production

This is the time to speak out—now—at the beginning. Our industrial program for re-armament is getting off on the wrong foot.

The talking and writing about it emphasize the wrong things.

Its headline words are “cuts” and “controls.”

Those words make bad propaganda for the cold war.

“Cuts” and “controls” are no words to challenge the imagination and energy of our own people. They won't impress the masters of the Kremlin. And they can only make it appear to the rest of the world that America thinks it can defend the free way of life by abandoning it.

America stands as the world's champion against aggression because America has become the most powerful free nation in the world.

How did we get that way?

Not by putting ceilings on wages; not by rationing or clamping iron-clad government controls all over business and industry.

To be sure, some temporary controls are necessary to channel very scarce materials speedily to use for defense. So, too, are special taxes and credit restrictions needed to combat inflation. But they will be fatal if they blind us to this fact:

We became the strongest nation in the world by out-producing every other nation.

Production—The Final Answer

Next year our government is planning at least a \$40 billion military program. Instead of planning only on controls to divert \$40 billion of production from the making of civilian goods to the making of military supplies, we should be figuring out also ways to push up total production.

Of course, our industrial plant is running at close to “capacity” now. And our labor force has reached almost full employment. There isn't much slack to be taken up.

Can even the United States add a \$40 billion miracle of production on top of what it is already doing?

Our answer is “Yes”—and within two years. It can be done by adding about \$6 billion each year to our program of capital investment which now runs about \$22 billion a year.

Part of this added production will come from expanding our industries. The steel companies, for example, already have plans to increase their capacity almost ten per cent in the next two years.

But by far the largest part of that \$40 billion of added production must come from higher productivity—raising industry's efficiency.

continued on next page

To meet our goals we need to raise our productivity five per cent a year.

Can it be done?

The answer is an emphatic "Yes."

Raise Industry's Productivity

McGraw-Hill's studies of industry's equipment show that there are countless opportunities for improving efficiency. Our manufacturing industries alone need at least \$35 billion of new equipment to raise their facilities to first class technical standards.

Here are some of the broad possibilities reported by the trained editors of McGraw-Hill's business magazines:

In many manufacturing plants as much as 40 per cent of workers' time goes into moving materials and parts—shifting things about within the plant between processes and to and from shipping platforms.

FACTORY estimates that improved materials handling equipment and methods might well cut handling costs twenty-five per cent and save annually over 650,000 man-years of unnecessary labor.

Modern machine tools designed since World War II are 40 per cent more productive, on the average, than is old equipment. But AMERICAN MACHINIST surveys show that 95 per cent of industry's machine tools are of designs at least ten years old. Replacing them could raise productivity of the metalworking industries at least ten per cent—enough to absorb a major share of the metalworking industries' part of the defense program as now planned.

In coal mining, latest equipment and methods can raise productivity sharply. The editors of COAL AGE estimate that production of bituminous coal could be raised from seven tons per man-shift to ten within three to five years.

Many new textile production techniques are 50 per cent to 75 per cent more efficient than those in use now. If plants could be fully modernized, and full use made of latest management methods, TEXTILE WORLD estimates that output-per-manhour would rise 20 per cent. A FOOD INDUSTRIES study indicates that modern equipment plus the best management techniques could raise productivity in food processing at least 20 per cent.

These are just some of the opportunities that industry can seize and by which the nation can profit.

A Nation-Wide Effort

Of course, industry itself can't do the whole job. Labor, government and all the rest of us must cooperate.

Government's part is to see that its emergency controls are so applied that they will increase productivity and thus make possible an early lifting of such controls.

Labor's part is to help in the development of labor-saving methods and machinery and to welcome their adoption as the only sure way of continuing to advance the American standard of living while maintaining the American free way of life.

For all of us the job is to work constantly for an expanding, ever-stronger America with constantly growing productivity; not a pinched and shackled America cooped up under wage and price ceilings and tied to a ration card.

Challenge to Industry

Here is a sharp challenge to industry to study the best work-methods that are being reported—to use every minute and every dollar it can to replace obsolete equipment.

Here is a sharp challenge to government to do everything within its power to make its control policies and its fiscal policies strengthen the incentives to industrial modernization—to demand sacrifice for a purpose and not for effect.

The job to which such opportunities point will take time—though nothing holds back adoption of some of the simpler improvements in work-methods reported in business magazines all the time.

But increasing production is our one best hope that we may be spared the full array of price, wage and production controls now and be freed eventually from all controls.

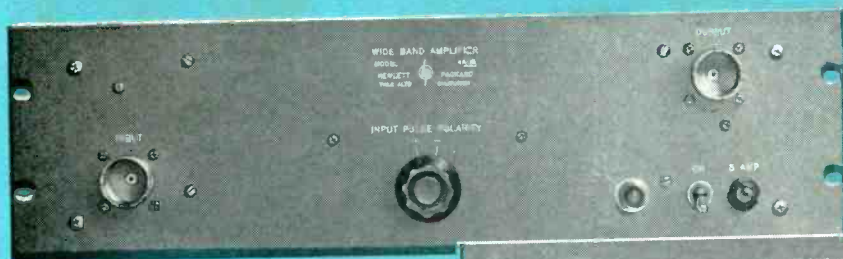
General Omar Bradley has said that the protection of our national independence calls for "long-range commitments that we are willing to carry out."

A long-range commitment to fight this battle for peace with America's most powerful weapon—industrial productivity—is the surest guarantee of victory for the free world.

Let's make that commitment—now—at the beginning.

McGraw-Hill Publishing Co., Inc.

COMPLETE, WIDE-BAND INSTRUMENTATION FOR DISTORTION-FREE, FAST-PULSE MEASUREMENT!



New -hp- 460B Fast-Pulse Amplifier



-hp- 46A Connectors and Accessories



-hp- 460A Wide-Band Amplifier



SPECIFICATIONS

-hp- 460B PAST PULSE AMPLIFIER

FREQUENCY RESPONSE: Closely matches Gaussian curve. Hf 3 db point is approx. 140 mc. Lf 3 db point is approx. 50 kc into 200-ohm load.

MAXIMUM OUTPUT VOLTAGE: High bias, approx. 125 v. negative open circuit. Normal bias (linear amplification) approx. 8 v. peak into 200-ohm load or 16 v. peak open circuit, pos. or neg. pulses.

GAIN: Approx. 15 db into 200-ohm load.

INPUT IMPEDANCE: Approx. 200 ohms.

RISE TIME: Approx. 0.0026 μ sec.

DELAY: Approx. 0.016 μ sec.

DUTY CYCLE: 0.10 max. for 125 v. output pulse.

LINEARITY PULSE OPERATION: See Figure 1.

MOUNTING: Relay rack. 5 1/4" x 19" x 6" deep.

POWER SUPPLY: 115 v. 50/60 cps. 35 watts.

PRICE: \$225.00 f.o.b. factory.

-hp- 460A WIDE-BAND AMPLIFIER

(Specifications same as Model 460B except:)

MAXIMUM OUTPUT VOLTAGE: Approx. 8 v. peak open circuit; 4.75 v. peak into 200-ohm load.

GAIN: Approx. 20 db with 200-ohm load.

DELAY: Approx. 0.012 μ sec.

PRICE: \$185.00 f.o.b. factory.

-hp- 46A ACCESSORIES

- hp- 46A-16A PATCH CORD - 200-ohms, 2' long. \$18.50.
 - hp- 46A-16B PATCH CORD - 200-ohms, 6' long. \$25.50.
 - hp- 46A-95A PANEL JACK - For 200-ohm cables, low capacitance. 1 1/8" dia. \$7.50.
 - hp- 46A-95B CABLE PLUG - For 200-ohm cables, low capacitance. \$7.50.
 - hp- 812-52 CABLE - 200-ohm cable in lengths to specification. Per foot \$1.75.
 - hp- 46A-95C 50-OHM ADAPTOR - Type N connector for coupling 50-ohm line into -hp- amplifiers. \$15.00.
 - hp- 46A-95D ADAPTOR - Bayonet sleeve for connecting -hp- 410A VTVM to output of 460A/B amplifiers. \$15.00.
 - hp- 46A-95E CONNECTOR SLEEVE - Joins two 46A-95B CABLE PLUGS. \$7.50.
 - hp- 46A-95F ADAPTOR - For connecting to 5XP CRT. \$10.00.
 - hp- 46A-95G ADAPTOR - For connecting to Tektronix type 511 oscilloscope. \$12.50.
- Data subject to change without notice.

UP TO 90 DB GAIN IN CASCADE! AMPLIFIES MILLI-MICROSECOND PULSES! RISE TIME .0026 μ SEC! 125-VOLT OPEN-CIRCUIT OUTPUT! GIVES OVER 100 MC BANDWIDTH TO YOUR STANDARD OSCILLOSCOPE!

Here at last is complete instrumentation for true amplification of fast pulses at high power levels sufficient to operate scalars or counting meters, cathode ray tubes, or to give more than 100 mc band-width to your present oscilloscope. New -hp- 460B Fast-Pulse Amplifiers, in cascade with -hp- 460A Wide-Band Amplifiers, amplify up to 125 volts, open circuit (limited duty cycle). This permits full deflection of 5XP cathode ray tubes, or 2-inch deflection of 0.0026 μ sec, combined with zero overshoot, insures distortion-free amplification of pulses faster than 0.01 μ sec.

New -hp- 460B Amplifier, cascaded with -hp- 460A provides linear amplification of 16 volts peak output and pulse amplification of 125 volts output (slight non-linearity). This combination provides maximum usefulness in fast-pulse study for nuclear radiation work, television or VHF research; for increasing frequency range of your oscilloscope, or general wide-band laboratory amplification. In addition to the above instrumentation, -hp- also offers series 46A accessories—a complete set of 200 ohm cables, adapters and fittings for inter-connecting amplifiers or patching to oscilloscopes.

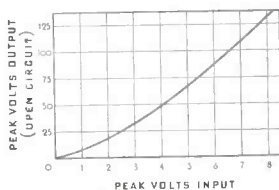


Fig. 1: Linearity of -hp- 460B Fast-Pulse Amplifier

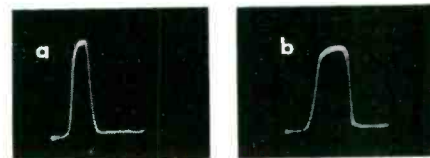


Fig. 2: (a) 0.01 μ sec pulse through -hp- 460B Amplifier (b) 0.02 μ sec pulse through 3 amplifiers in cascade

Get complete details. Write direct or see your -hp- sales representative.

HEWLETT-PACKARD COMPANY

2177A Page Mill Road • Palo Alto, California, U.S.A.

Sales Representatives in all principal cities.

Export: Frazar & Hansen, Ltd., San Francisco, New York, Los Angeles

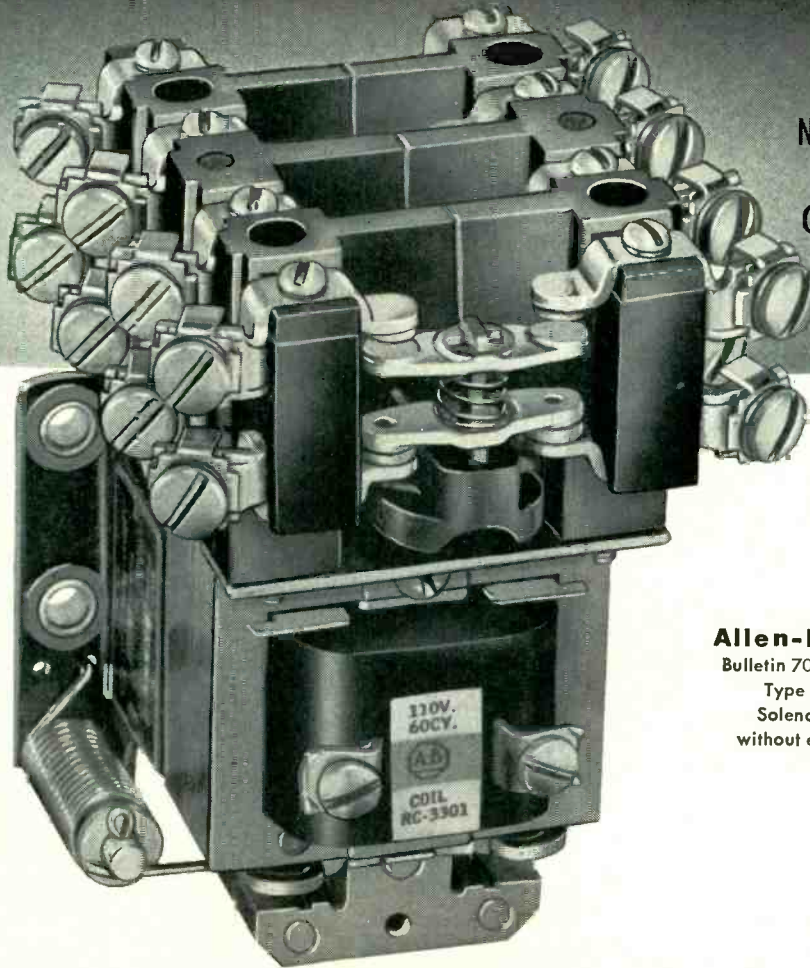
HEWLETT-PACKARD  INSTRUMENTS

4

Normally
Open
Contacts

4

Normally
Closed
Contacts



Dimensions
of Universal Relay
High—3-15/16 in.
Wide—2-15/16 in.
Deep—3-5/16 in.

Allen-Bradley
Bulletin 700 Universal
Type BX 440
Solenoid Relay
without enclosure.

These **SMALL UNIVERSAL RELAYS**

are instantly adaptable for switching
a wide variety of power supply circuits

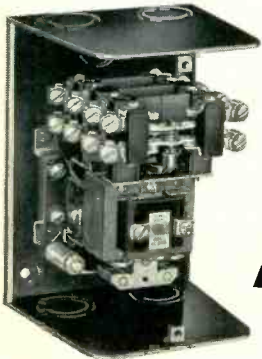
There are literally thousands of places for these small, dependable solenoid relays in electronic power circuits. These Bulletin 700 relays are built in an amazing variety of contact arrangements . . . normally open and normally closed . . . from one to eight poles. Enclosures are available for almost any service requirement.

^ The Type BX 440 Universal Solenoid Relay has

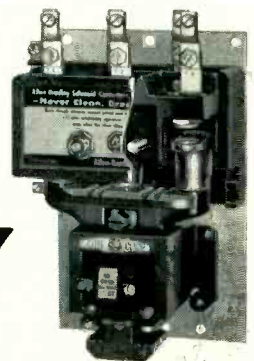
four normally open and four normally closed contacts which may be used interchangeably for handling a wide variety of circuit arrangements.

It will pay you to get a full listing of Allen-Bradley Bulletin 700 A-C Relays. And for heavier currents, Allen-Bradley solenoid contactors are available up to 900 amperes . . . with or without enclosures. Investigate the Allen-Bradley line.

Allen-Bradley Co., 110 W. Greenfield Ave., Milwaukee 4, Wis.



Allen-Bradley Relay in
general purpose enclosure.

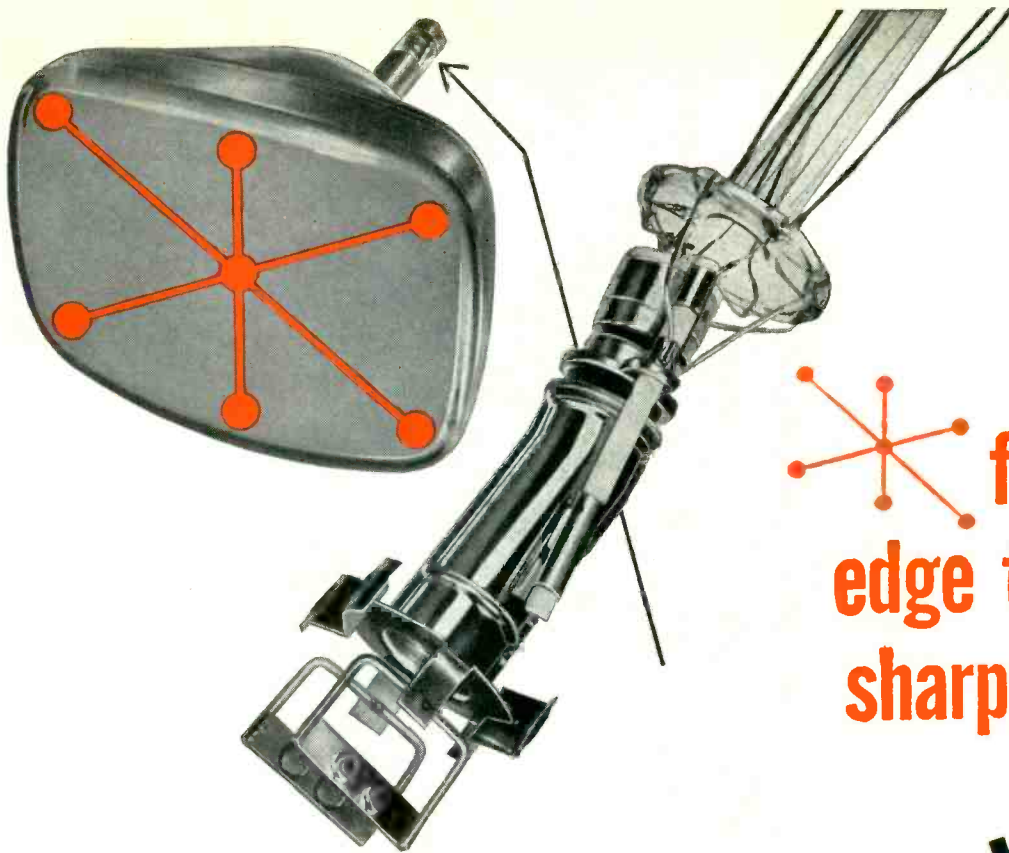


Bulletin 702 Solenoid Con-
tactor—50 ampere rating.

ALLEN-BRADLEY

RELAYS • RESISTORS

QUALITY




**for
edge to edge
sharpness...**

the **New** Du Mont Bent-Gun

the latest refinement in the most copied gun structure

Uniform sharpness of trace to the very edges of the screen distinguishes the new Du Mont Bent-Gun.

A higher degree of pre-focusing passes a smaller-diameter beam through the deflection field. Spot distortion is reduced and a uniform overall focus results. Other design changes are: Improved bulb spacer insures proper anode contact and electron gun centering; rounded corners on pertinent gun parts eliminates stray emission at higher anode voltages; new grid-cathode assembly allows a longer G-2 (second grid) without increasing overall length.

This new Du Mont Bent-Gun is now being incorporated in ALL Du Mont Teletrons. Therefore, whether planning a new TV receiver or modifying an old one, be sure to include the Du Mont Teletron for the best in TV pictures. Simply specify DU MONT.

FIRST WITH THE FINEST IN **T-V** TUBES

DU MONT

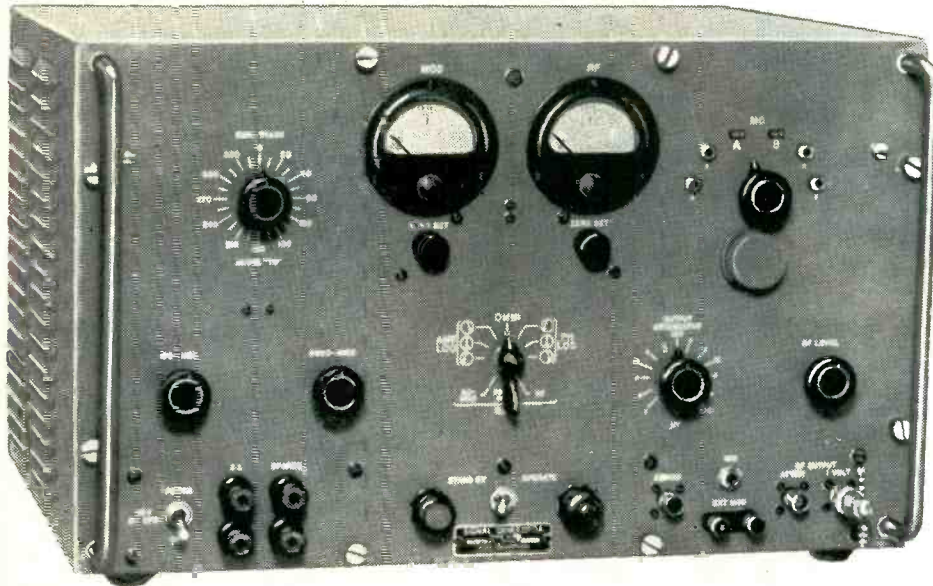
Teletrons^{*}

ALLEN B. DU MONT LABORATORIES, INC.,
Tube Division, Clifton, N. J.

*Trade-mark.

SIGNAL GENERATORS by

AIRCRAFT RADIO CORPORATION



TYPE H-14

108-118 MEGACYCLES

Tests OMNI Receiving Units
in Aircraft or on the Bench

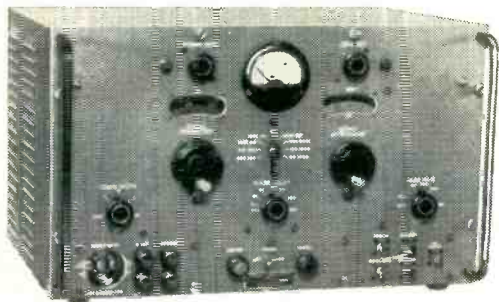
Checks on:

- 24 Omni courses
- Left-center-right on Phase-localizer
- Left-center-right on Amplitude-localizer
- Omni course sensitivity
- To-From and Flag-alarm operation
- All necessary quantitative bench tests

quickly and accurately just before take-off. RF output for ramp checks, 1 volt into 52 ohm line and for bench checks, 0-10,000 microvolts. Provision for external voice or other modulation. AF output available for bench maintenance and trouble shooting.

The Type H-14 Signal Generator, 108-118 megacycles, provides a standard signal source for the complete testing of VHF airborne omnirange and localizer receivers in aircraft or on the bench. It provides for testing 24 omni courses, plus left-center-right checks on both amplitude and phase localizers. Aircraft may be checked out

Price: \$885.00 net, f.o.b. Boonton, N. J.



ARC Communication and Navigation Equipment



Aircraft Radio Corporation also manufactures LF and VHF airborne communication and navigation equipments—all CAA-Type-Certificated for scheduled air-carrier use or for those whose type of flying requires a high degree of reliability and performance. Equipment consists of light, small units which can be combined to provide the required operation, whether it be the 1 Receiver/1 Transmitter (15 pound) installation in a 2-place helicopter, or a 3 Receiver/2 Transmitter/ VHF Omni installation (70 pounds) in larger 2-engine aircraft.

TYPE H-10—Microwave Test Set; 23,500-24,500 Megacycles

Provides source of cw or pulse frequency—modulated RF, power level -37 to -90 dbm. RF power meter measures levels from +7 to +30 dbm. Frequency meter for measuring output or input RF accurate to better than 20 mc. Primary purpose of the H-10 is to

measure receiver sensitivity, bandwidth, frequency, recovery time, and overload characteristics, plus transmitter power and frequency. Recommended as a standard source of RF for research or production testing. Equal to military TS-223/AP.

Price: \$1692.00 net, f.o.b. Boonton, N. J.

TYPE H-12—VHF Signal Generator; 900-2100 Megacycles

Provides source of cw or pulse amplitude-modulated RF, power level 0 to -120 dbm. Internal pulse circuits with controls for width, delay, and rate, and provision for external pulsing. Single

dial tuning, frequency calibration accurate to better than 1%. Built to Navy specifications for research and production testing. Equal to military TS-419/U.

Price: \$1950.00 net, f.o.b. Boonton, N. J.



WRITE TODAY for descriptive literature on A.R.C. Signal Generators or airborne LF and VHF communication and navigation equipments, CAA Type Certificated for transport or private use.

Aircraft Radio Corporation

Boonton, N. J.

Dependable Electronic Equipment Since 1928

It's a fact that

✓ The American Lava Corporation has one of the best equipped Research Divisions in the industry. The American Lava Staff has graduate engineers from all leading engineering schools. Ceramic, electrical and mechanical engineers are preponderant but every engineering degree currently being awarded by U. S. Engineering Schools is held by one or more men on this staff.

✓ Almost every month, the Research Division successfully completes the development of a new ALSiMag composition to comply with special requirements. These developments are in close cooperation with the customer. When requested, all details are kept confidential.

✓ Continuous operation of kilns at 12 different temperatures, at temperatures ranging from 1400° F. to above 3000° F., permits the firing of each ALSiMag composition at its optimum temperature.



ALSiMAG

TRADE MARK REGISTERED U.S. PATENT OFFICE

At American Lava Corporation, you are most apt to find the answer to any question involving technical ceramics. American Lava Corporation is composed of MEN who give intelligent, sympathetic consideration to customer problems—backed by specialized experience gained in 49 years of concentrating entirely on custom made technical ceramics. The knowledge of these men is available to you on request. If requested, all customers' information is kept strictly confidential.

AMERICAN LAVA CORPORATION

49TH YEAR OF CERAMIC LEADERSHIP

CHATTANOOGA 5, TENNESSEE

OFFICES: METROPOLITAN AREA, 671 Broad St., Newark, N. J., Mitchell 2-8159 • CHICAGO, 228 North LaSalle St., Central 6-1721
PHILADELPHIA, 1649 North Broad St., Stevenson 4-2823 • LOS ANGELES, 232 South Hill St., Mutual 9076
NEW ENGLAND, 38-B Brattle St., Cambridge, Mass., Kirkland 7-4498 • ST. LOUIS, 1123 Washington Ave., Garfield 4959



Brand-new

12.5-AMP THYRATRON



General Electric's GL-5855 is designed for control work that requires high current capacity . . . toughness and stamina . . . utmost dependability.

HERE'S a new motor-control tube that handles big currents, and can take the punishment of full-time, heavy-duty operation . . . on through a long life span which squeezes value out of every dollar.

Study the clean, sturdy design. Under the heavy glass envelope is a structure so simple, so inherently braced, that vibration and shocks have little effect. Bolts fasten the tube to the panel, assuring firm support and providing tight, solid electrical contacts.

Cleanness and simplicity go further . . . right through to application needs. No snubber circuit is required. The high commutation factor (200) means that the anode gas absorption from inductive loads is negligible. This makes for long tube life with a straightforward, economical circuit.

To a husky 12.5-amp rating are added high anode voltage, high peak-to-average current ratio, stable control characteristics, and short heating time. This pattern has made the earlier, smaller GL-5544 and GL-5545 popular; assures enthusiastic acceptance for the new thyatron. Also, the GL-5855 has a wide temperature range, making the tube virtually climate-proof.

Wire or write for complete ratings and performance data. Or better, ask for an across-your-desk talk with an experienced G-E tube engineer! *Electronics Department, General Electric Company, Schenectady 5, N. Y.*

GL-5855
12.5-amp control thyatron

Filament voltage	2.5 v
Filament current	34 amp
Peak anode voltage, forward and inverse	1,500 v
Peak cathode current	150 amp
Avg cathode current	12.5 amp
Current averaging time	15 sec
Ambient temp range	-55 to +70 c
Commutation factor	200

NOTE—Commutation factor is the product of the rate of current decay in amperes-per-microsecond just prior to commutation and the rate of inverse voltage rise in volts-per-microsecond just after commutation.

GENERAL  **ELECTRIC**

190-K1

Looking for trouble before it starts...

with an **MB VIBRATION EXCITER**



One of the many instruments produced by the Sperry Gyroscope Company is here undergoing a "shake test" on the MB model S-3 Vibration Exciter. Such vibration testing contributes to the dependability in service for which Sperry instruments are noted. The instrument is fastened to the shake table of the exciter, which is controlled from panel. Amplitude, velocity and acceleration are being read directly on an MB Vibration Meter.

WHEN PRODUCTS GIVE unexpected trouble in service, you'll find too often that it's due to vibration.

Foresighted concerns take no chances with this enemy of equipment life. At Sperry Gyroscope Company, possible troubles due to vibration are ferreted out in the laboratory. By means of an MB Vibration Exciter, which has quick, easy adjustments for force and frequency, instruments are checked for vibratory response — for ability to resist fatigue. Result: Trouble is eliminated in the design stage, *before* it starts.

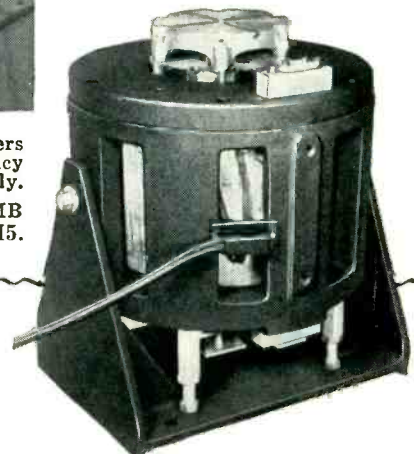
This shaker is adaptable to countless situations. You can test miniature electrical assemblies to mammoth wing structures; filaments to heavy axle shafts. In one of its jobs — fatigue testing — the shaker reproduces vibratory effect of years within hours. One company, for example, reduced the time of spot-checking bellows to 10 minutes — a job which formerly took 12 hours per unit!

Location of noise sources . . . actual observation of the motions of vibrations . . . study of damping characteristics of materials . . . these are but a few other important jobs where an MB Exciter pays off.

Models which deliver forces of 5, 25, 50, 100, 200, 300 pounds and higher are now available — all electromagnetic. We'd like to explain the technique of their use in detail, show you how to use one on your own problems. Write us without obligation.

The Model S3 Vibration Exciter illustrated delivers peak force of 200 pounds. Operates in frequency range of 3 to 500 C.P.S. Has rotating power supply.

Write us for more detailed information on MB Vibration Exciters, and ask for bulletin 410 M5.



THE **MB** MANUFACTURING COMPANY, Inc.
1060 State Street, New Haven 11, Conn.

PRODUCTS AND EQUIPMENT TO CONTROL VIBRATION . . . TO MEASURE IT . . . TO REPRODUCE IT



*Most Trusted Name
in Picture Tubes ...*



THE SAFEST PICTURE
TUBE IN THE WORLD



Only Zetka utilizes the power-tube method of producing picture tubes. This means custom-processing, long pumping, set-testing. Zetka tubes are superior, more sharply focused, safe. Rectangulars and rounds in 16", 17", 19" and 20"



Zetka

zetka

TELEVISION TUBES, INC. 131-137 GETTY AVE. • CLIFTON, N. J.

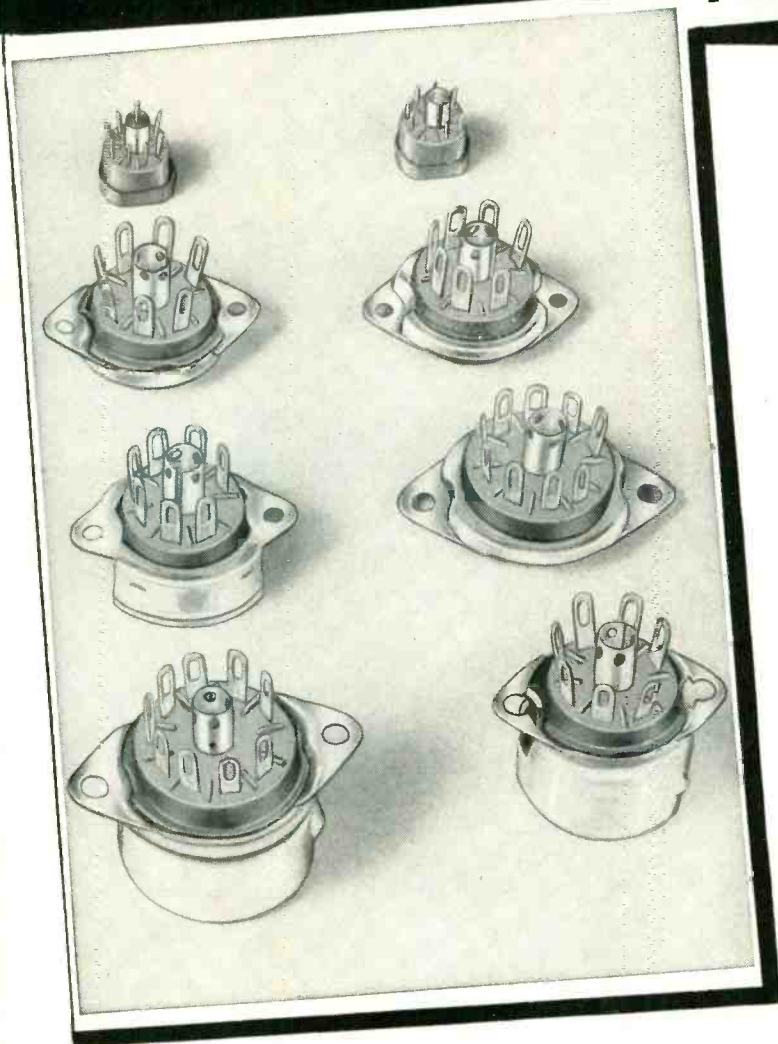
For 37 years, Zetka has been a respected name in the radio and television industry.

MYCALEX

MINIATURE TUBE SOCKETS

7-PIN and 9-PIN... and SUBMINIATURES

**PREMIUM INSULATION
PRICED COMPETITIVELY**



Now MYCALEX offers both 7-pin and 9-pin miniature tube sockets . . . with superior low loss insulating properties, at new low prices that offer ceramic quality for the cost of phenolics.

MYCALEX miniature tube sockets are injection molded with precision that affords uniformity and extremely close tolerances. MYCALEX insulation has high dielectric strength, very low dielectric loss, high arc resistance and great dimensional stability.

Produced in two grades: MYCALEX 410 conforms to Grade L4 specifications, having a loss factor of only .015 at 1 MC. It is priced comparably with mica filled phenolics.

MYCALEX 410X is for applications where low cost of parts is vital. It has a loss factor only one-fourth that of "everyday" quality insulating materials, and a cost no greater.

Prices gladly quoted on your specific requirements. Samples and data sheets by return mail. Our engineers will cooperate in solving your problems of design and cost.

Mycalex Tube Socket Corporation

*"Under Exclusive License of Mycalex Corporation
of America"*

30 Rockefeller Plaza, New York 20, N.Y.



MYCALEX CORP. OF AMERICA

"Owners of 'MYCALEX' Patents"

Executive Offices: 30 Rockefeller Plaza, New York 20, N. Y.

Plant and General Offices: Clifton, N. J.



BRADLEY

RECTIFIERS

perform as rated!

YOU CAN COUNT on performance exactly as rated with Bradley rectifiers — whether your requirements involve one unit or a hundred thousand units. Our exclusive vacuum process—as applied to selenium and copper oxide rectifiers — provides the highest type of quality control. You get the rectifier you need, predictably accurate, true to rating and long-lived even under extreme operating conditions.



SEBL SERIES
Selenium for high voltage uses.



CX14 SERIES
Copper oxide for instruments.

SPECIAL POWER CONVERSION PROBLEMS — the kind that get you shrugs elsewhere — are challenges that we accept and handle with speed and competence. Bradley has helped many leading manufacturers use rectifiers in new ways that have led to improved product performance. We can help you, too, on either standard or special requirements. If your product involves a rectifier — see Bradley to get the performance desired.



SE11X SERIES
Selenium for high current uses.

PHOTOELECTRIC CELLS

Bradley Luxtron® photoelectric cells convert light directly into electrical energy without external power source. Wide range of models, sizes and shapes available.

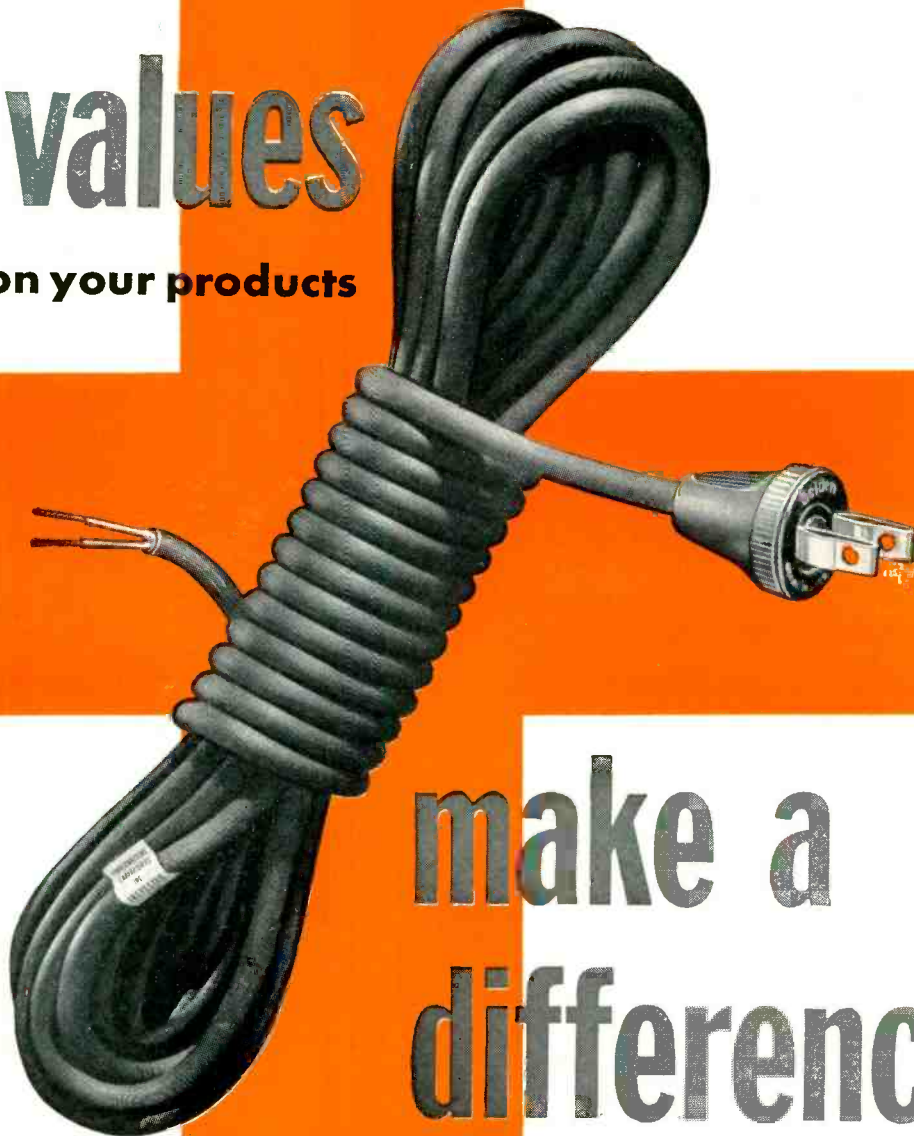
*T.M. Reg. U.S. Pat. Off.

BRADLEY LABORATORIES, INC.

82 MEADOW STREET NEW HAVEN 10, CONNECTICUT

plus values

in the cords on your products



make a difference

a Belden Cord Means

- + SAFETY and APPEARANCE
- + QUICK ASSEMBLY
- + FEWER REJECTIONS
- + LONG LIFE IN SERVICE



Belden Engineered Cords give you real Plus Values because they are engineered to your product, complete with molded plugs or connectors. They are built far above minimum standards, to give your product a chance to operate without cord failure and to maintain your customer's good will.

All Belden Cords are factory tested to eliminate cord grief—extra assembly operations—rejections—extra cost. Investigate Belden Cords, today. Write

Belden Manufacturing Company
4625 W. Van Buren Street
Chicago 44, Illinois

CORDITIS-FREE CORDS BY

Belden

WIREMAKER FOR INDUSTRY



HOW DID SUNSET BLVD GET ON BROADWAY?

Everyone knows that it's hard to be in two places at the same time.

But recently, Paramount Pictures had to be in 387 places at once.

The release of their smash hit, "Sunset Boulevard," called for *simultaneous* openings in theatres on Broadways all over America. And although Gloria Swanson

is being mentioned for an Oscar, Paramount feels there ought to be a special award for a star not even mentioned in the cast.

That's Air Express!

Thanks to Air Express, Paramount could work on the cutting, editing and printing of this film up to the last minute — and still get there on time!

But, you don't have to be in the motion picture industry to profit from regular use of Air Express. Here are its unique advantages which any business can enjoy:

IT'S FASTEST — Air Express gives the fastest, most complete door-to-door pick up and delivery service in all cities and principal towns, *at no extra cost.*

IT'S MORE CONVENIENT — One call to Air Express Division, Railway Express Agency, does it all.

IT'S DEPENDABLE — Air Express provides one-carrier responsibility all the way and gets a *receipt upon delivery.*

IT'S PROFITABLE — Air Express expands profit-making opportunities in distribution and merchandising.

Like to know more? Call your local Air Express division of Railway Express Agency.



AIR EXPRESS
GETS THERE FIRST

THE CERAMIC CORES THAT
PAVED THE WAY TO BETTER

TV



- ✓ Lower losses with higher efficiency and lower operating temperatures
- ✓ Lighter weight, smaller sizes for more compact construction, lower costs of finished equipment
- ✓ Much higher permeability
- ✓ Less corona effect
- ✓ Lower cost

Technically, Stackpole Ceramag Cores are molded from a metallic oxide powder mixture which, when properly handled during processing, promotes cubic crystal growth. This results in a non-metallic material having low eddy current loss and exceptionally high permeability.

Practically, Stackpole's skill in the highly critical fabrication of these cores in production quantities has resulted in lower costs and higher standards of performance and dependability for the nation's leading television receivers.

Besides the more popular standard Ceramag core types illustrated above, many specials are regularly supplied.

Electronic Components Division

STACKPOLE CARBON COMPANY, St. Marys, Pa.

NEED A MIXER FOR YOUR UHF TV CONVERTER DESIGN?

SPECIFY GENERAL ELECTRIC 1N72* UHF GERMANIUM DIODES

Designed specifically for the TV market and performance tested for a full year, this low noise, high stability diode is now available in production quantities at new low prices.

CHARACTERISTICS: Low noise factor . . . improved burn-out resistance . . . operation not affected by overloads . . . snap-in design for use with miniature clips to avoid inductive leads . . . input and output impedances approximately 100-500 ohms . . . no contact potential . . . welded whisker construction.

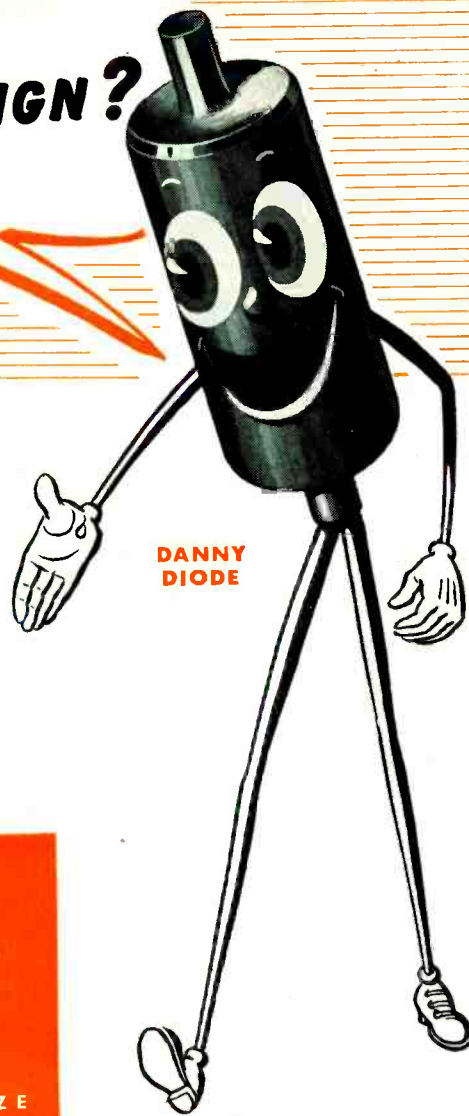
New Plant Facilities To Meet Total Industry Requirements—A complete new G-E plant devoted exclusively to the man-

ufacture of diodes is now in operation near Syracuse, New York. These facilities enable us to handle the total industry requirements for UHF television mixer crystals. General Electric application engineers are at your service to help your designers interpret the characteristics of this crystal to your circuit's advantage. For full information, call the G-E electronics office nearest you or write for Bulletin X57-015A: *General Electric Company, Section 411, Electronics Park, Syracuse, New York.*



ACTUAL SIZE

*formerly designated G-7



DANNY DIODE

SPECIFICATIONS

UHF TYPE 1N72 (Formerly Designated G-7) Specifications at 25° C:

Design frequency 500 mc
Useful frequency range DC to over 1,000 mc
Noise figure 14 to 19 db*

*Measurements made with Measurements Corp. Model 84 Signal Generator, R.C.A. Model A Converter with 0.7 ma rectified local oscillator current and G-E Model 814 television receiver with television channel 3 used as IF frequency with noise band width of 3.5 mc. Noise figure is measured by noting signal required to double zero signal noise power output of converter. Similar measurements made on average 1N21B diodes indicated noise figure of 16 db.

Maximum Ratings:

Average rectified current 25 ma max.
Peak rectified current 75 ma max.
Temperature range -50 to +75°C

... Other Applications, Too

For example, as harmonic generators to provide local oscillator injection from the low frequency local oscillator . . . As detectors in high frequency RF voltage measurements . . . and in low frequency circuits where a low impedance crystal is needed.

COMPLETE LINE OF GENERAL ELECTRIC WELDED GERMANIUM DIODES

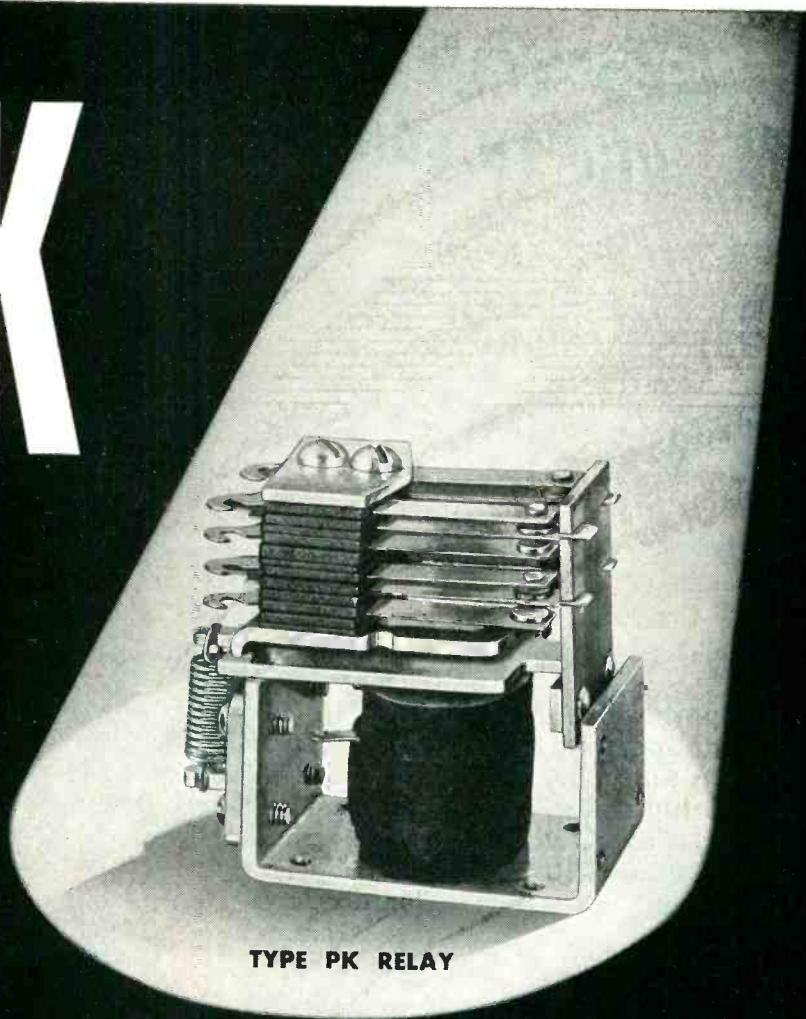
General Purpose	Television	JAN	UHF	Quads	Transistors
1N48 1N63	1N64	1N69	1N72	1N73	SX-4A
1N51 1N75	1N65	1N70		1N74	Z-2
1N52					

You can put your confidence in—

GENERAL ELECTRIC

PEAK

IN
POWER
VERSATILITY
QUALITY
PERFORMANCE



TYPE PK RELAY

HERE ARE THE FACTS AND FIGURES:

CONTACTS: 10 amp. standard. 24 volts D.C., 115 volts A.C.
15 amp. contacts available.

SENSITIVITY: D.C.: 4 pole 1.5 watts
2 pole .7 watts
A.C.: 4 pole 5 volt amperes
2 pole 2.5 volt amperes
Can also be furnished in 6 pole AC and DC up to 4000 Ohms.

COIL: To 115 volts D.C., 230 volts A.C.

NOMINAL HEAT USE: D.C. 30°C above room ambient
A.C. 45°C above room ambient

MAX. INPUT FOR 85° RISE: D.C. 5 watts
A.C. 11 volt amperes

MOUNTING: Base or end mounting

WEIGHT: 4.5 oz. 4 P.D.T.

WEIGHT HERMETICALLY SEALED: 7.7 oz.

DIMENSIONS: Open Relay— $2\frac{1}{16}$ " \times $1\frac{1}{8}$ " \times $2\frac{1}{16}$ "
Sealed Relay— $3\frac{1}{8}$ " \times $1\frac{1}{2}$ " \times $2\frac{5}{16}$ "
Overall Mounting Flange— $3\frac{1}{8}$ "
Center to Center Mounting Holes— $2\frac{1}{16}$ "

A Quality Relay

The new Allied PK Relay is designed to offer versatility in a power relay where quality and low cost are factors. Besides stability in operation its reliability allows a range in applications from high quality instruments to vending machines. The PKU relay will comply with Underwriters' Laboratories requirements and can also be supplied hermetically sealed.

Bulletin PK gives complete details. Send for your copy today.

Be sure to send for your copy of Allied's Relay Guide. It gives the engineering data for 27 Allied relays in a concise tabular form for easy reference.



AL-144

ALLIED CONTROL COMPANY, INC. 2 EAST END AVENUE, NEW YORK 21, N.Y.

Improve Your Controls
with

VICKERS MAGNETIC AMPLIFIERS

SELF-SATURATING



HIGH POWER

For 60 cps power sources—27 styles—maximum output powers from 62 watts to 4200 watts.

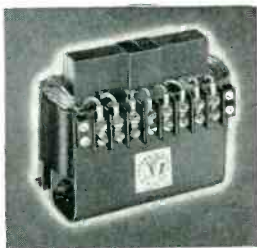
HIGH PERFORMANCE

For 60 cps power sources—28 styles — maximum output powers from milli-watts to 108 watts. For 400 cps power sources—20 styles—maximum output powers from 30 watts to 385 watts.



HIGH GAIN

For 60 cps power sources—22 styles — maximum output powers from 1/2 watt to 1200 watts.



All amplifiers furnished complete with Vickers special Selenium Rectifiers.



Now More Than 90 STANDARD Styles Offer These Advantages

- HIGH PERFORMANCE
- NO MAINTENANCE
- RUGGED CONSTRUCTION
NO MOVING PARTS
- NO WARM-UP TIME
- A-C OR D-C CONTROL
A-C OR D-C OUTPUT
- RESPONDS TO SUM OR DIFFERENCE
OF SEVERAL SIGNALS
- ALLOWS ELECTRICAL ISOLATION
BETWEEN CIRCUITS

TYPICAL APPLICATIONS

Servomechanisms — Line-To-Line Voltage Regulators — Hydraulic Transmission Controls—A-C and D-C Generator Voltage Regulators—Speed and Frequency Regulators — Lamp and Furnace Controls—Temperature Regulators—Time Delay Devices.

WRITE FOR BULLETIN 20-A

for information on the *complete* line of Vickers Standard Magnetic Amplifiers. Please make request on your letterhead.



VICKERS ELECTRIC DIVISION

VICKERS Inc.
1801 LOCUST STREET • ST. LOUIS 3, MISSOURI

85° BELOW ZERO

would freeze an eskimo



... WON'T FREEZE **VARGLAS SILICONE**

500° ABOVE

would roast the devil



... WON'T ROAST **VARGLAS SILICONE**

Electrical Insulating
Tubing and Sleeving
lead wire and tying cord

Efficient at 500° F. or more in some applications—yet completely flexible at -85° F. Resistant to moisture and lubricating oil—flame resistant and self-extinguishing—this pioneer silicone tubing and sleeving developed by Varflex is available in various NEMA colors where required.

Varglas Silicone is a combination of *Varglas*—continuous filament Fiberglas; moisture and fungus proof; will not burn; strong and flexible at high and low temperatures; chemically inert . . . and *Silicone High Temperature Resin*—which has a natural affinity for Fiberglas; renders it abrasion-resistant, flexible and non-fraying. Normalizing process removes binder and organic inclusions from the Fiberglas; improves electrical qualities and allows uniform impregnation.

Investigate the NEW, low cost VARFLO Sleeving and Tubing if you do not have to allow for an unusually high operating temperature. Samples and prices on request. It's flexible. It takes rough handling without loss of dielectric. It won't fray out. Made with a Fiberglas braid, it won't support combustion—YET COSTS NO MORE THAN COTTON.

Clip and mail this coupon TODAY!

VARFLEX CORPORATION

308 N. Jay St. Rome, N. Y.

Please send me folder containing free samples of Varglas SILICONE products.

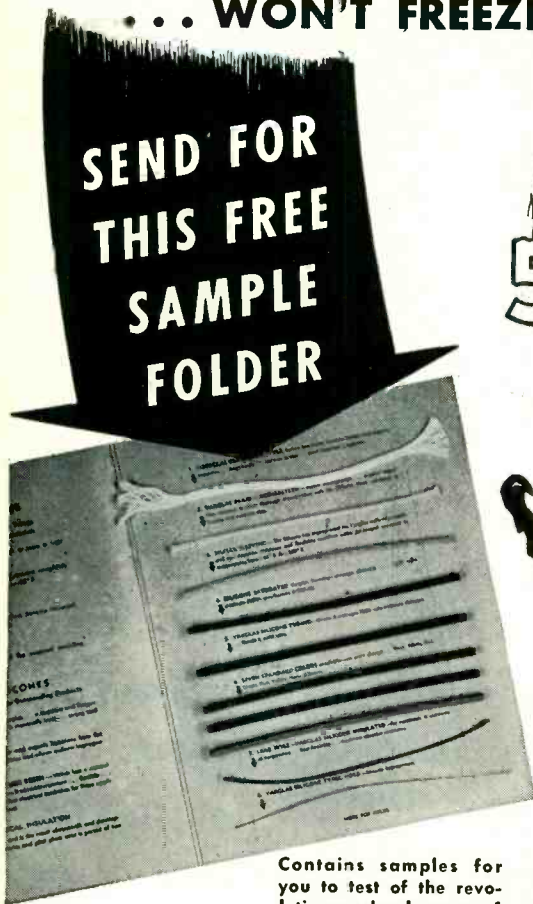
Name _____

Company _____

Address _____

City _____ Zone _____ State _____

Contains samples for you to test of the revolutionary development of Varflex laboratories . . .



bringing

Your Product

to market



is a full time job for... electronics

When you consider that there are more than 2,000 widely-diversified products sold to manufacturers and users of electronic equipment, the problem of bringing your product to that market — and selling it, might, at first, seem complicated. But it isn't.

Consider first how products are bought and by whom. Components and materials used in the design, testing or production of electronic equipment of all sorts are bought for engineering reasons by engineers. That this is true is obvious when one considers the extremely technical nature of the industry's products. The buying for this industry is done by men like the one shown . . . back-in-the-plant, design, development and test engineers, generally inaccessible to salesmen.

And it is their counterparts throughout industry and, of course, in communications and broadcasting who, by use of electronic equipment to solve their own design, test, production and control problems, create the markets for packaged electronic equipment.

It is for these men that **ELECTRONICS** is edited. Bringing them the up-to-the-minute electronic design, use and product information is **ELECTRONICS'** full time job. (A job it has held for over twenty years.) Because of this, they work with **ELECTRONICS** at their sides and refer to it more than to any other single source for the information they need in their work. It is for this reason that bringing your product to this market isn't as complicated as it might seem at first. **ELECTRONICS** provides a market place, the only one, in which you can reach these men who do the specifying and buying of electronics throughout industry...be it electronic manufacturing or general industry.



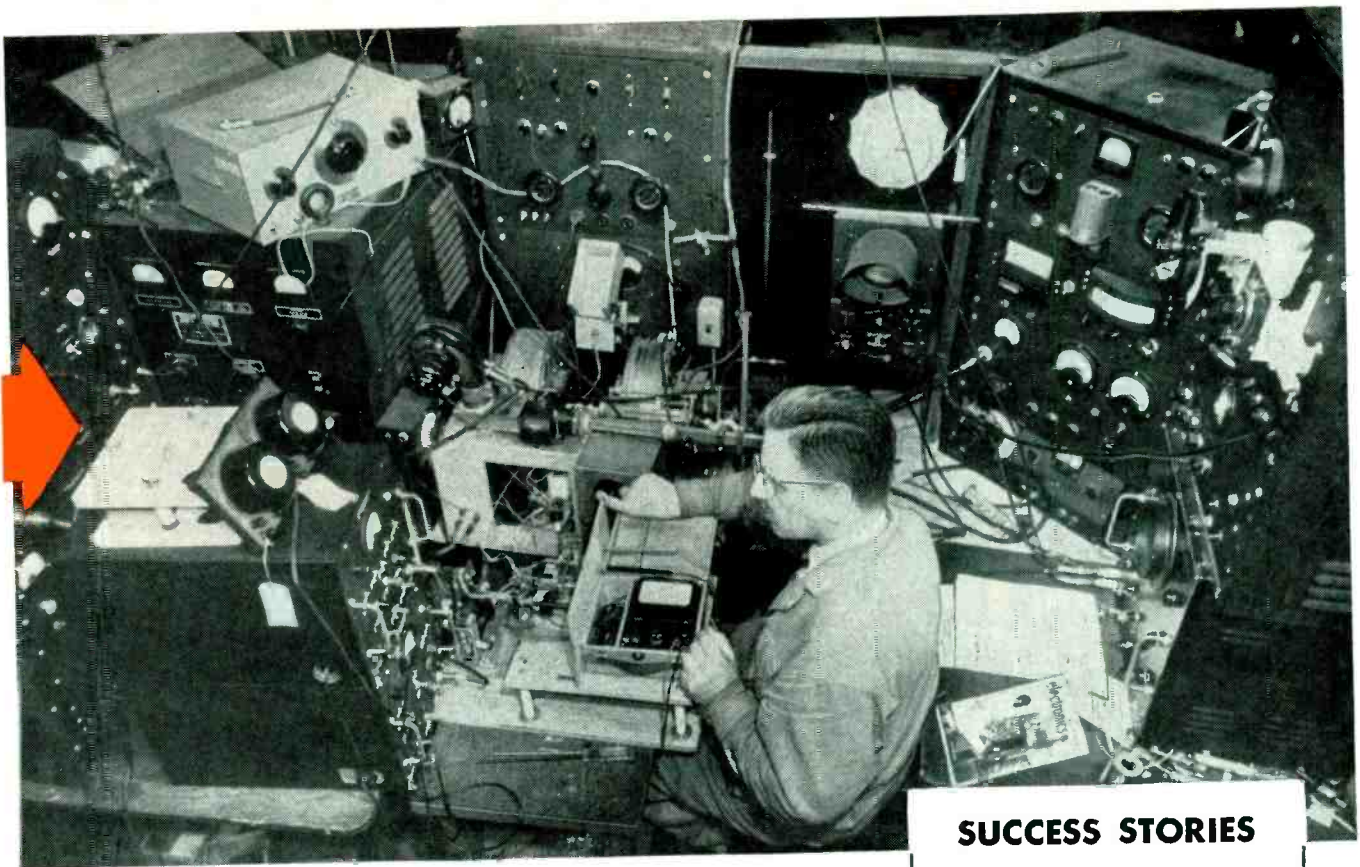
electronics

THE DIRECT ROUTE TO---

12 REGULAR ISSUES

supplying latest technical information, design and product news

A McGraw-Hill Publication • 330 West 42nd St., New York 18, N. Y.



What is YOUR PRODUCT?

With **ELECTRONICS'** blanket coverage of all industry, it doesn't matter whether your product is a material, component or a piece of electronic gear — a getter or a gear train, a capacitor or a cabinet, a servo or a spring, a motor or a motor control.

Both designers and users of electronic equipment find **ELECTRONICS** their best source of information. Manufacturers find it their best source of sales to both.

Take instrumentation for example. **ELECTRONICS** research department recently completed a survey of reader purchasing in that one, only partially electronic field. Returns were from every segment of industry and revealed that 116,395 instruments of 53 specified types are used by the four hundred and fifty-nine respondents. A copy of the complete results is yours for the asking.

Similar documented evidence that **ELECTRONICS** is not only the market place for all things electronic but also for all manner of other products used in conjunction (allied) with electronic products is available in another survey study we would like to show you, "The **ELECTRONICS** Audience—What is its buying scope?" Ask your **ELECTRONICS** representative for details.

*Further evidence is the list at the right showing some of the allied products currently being advertised successfully in **ELECTRONICS**. Positive evidence of the market offered by **ELECTRONICS** for your particular product can be obtained profitably by advertising in **ELECTRONICS**.*



--- A \$2,000,000,000 MARKET PLACE

ANNUAL BUYERS' GUIDE
supplying all basic product source and technical specifying data

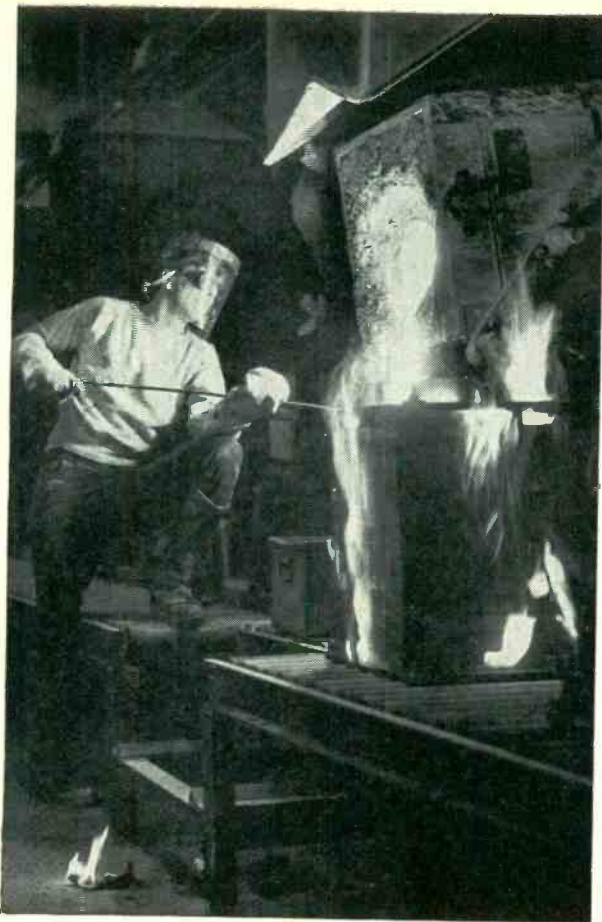
SUCCESS STORIES

Following is a partial list of allied products currently being advertised successfully in **ELECTRONICS** . . .

- BEARINGS
- BLOWERS
- BOBBINS
- BUSHINGS
- CARBON
- CERAMICS
- COUPLINGS
- DRAFTING EQUIPMENT
- FASTENERS
- GASES
- GEAR TRAINS
- GRAPHITE
- HAND TOOLS
- HEATING TANKS
- INSULATION
- IONIZATION CHAMBERS
- LIGHTING EQUIPMENT
- METAL STAMPINGS
- METALS & ALLOYS
- MOLDINGS
- MOTORS
- MOUNTINGS
- PAPER
- PHOTOGRAPHIC EQUIPMENT
- PLASTICS
- RINGS
- SEALS
- SOLDER
- SOLDERING GUNS
- SPRINGS
- TAPES
- TUBING
- WASHERS
- WIRE & CABLE

CARBOLOY

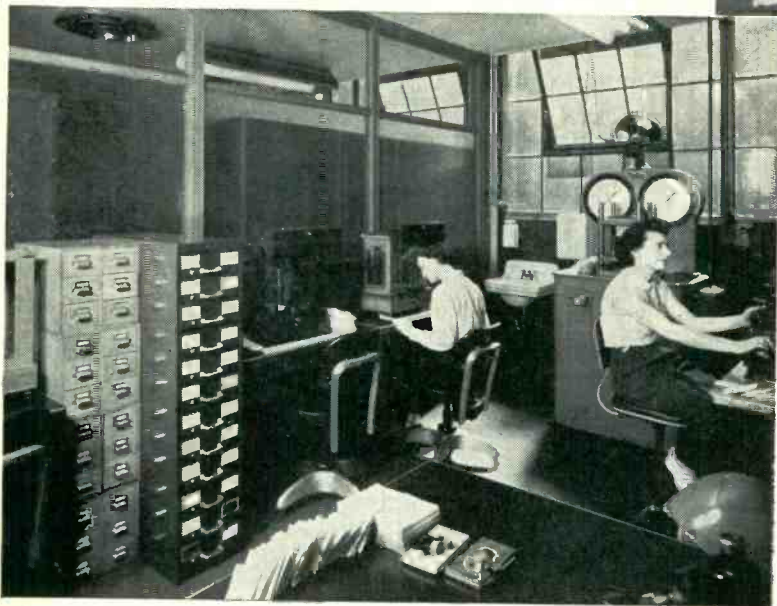
assures uniform



1 Pouring molten CarboLOY Permanent Magnets from electric furnace at 1800°C. Samples of every melt are checked for physical, chemical, and metallurgical qualities before release for fabrication.



3 Every CarboLOY Alnico Permanent Magnet is subjected to countless quality checks like this flux test to assure you of outstanding uniformity and performance.



2 As permanent magnets move from one production step to the next, every batch is quality checked and recorded.

LOOK TO
CARBOLOY CO., INC.

*for the finest
in versatile metals*

continuous quality control Alnico permanent magnets

4 Carboly's rigid quality tests pay off in uniform high quality Carboly Permanent Magnets for peace-time uses like this television tube. You are assured of the same high quality for radar and other defense applications.



FOR OVER 22 years the name "Carboly" has been a synonym for uniformity and outstanding quality with users of cemented carbide. Today, the same exacting standards of quality control that have earned this reputation for Carboly Company, Inc., are being applied to the production of permanent magnets, (among them Alnico) and other versatile metals, mass-produced for industry.

Your inquiries or orders for Carboly Permanent Magnets for use in essential goods will receive immediate attention.

The trade-mark "Carboly" identifies manufacture by Carboly Company, Inc.

CARBOLOY
THE QUALITY BRAND

PERMANENT MAGNETS

(Alnico and other types)

GREATER VALUE

WITH

BENDIX ELECTRICAL CONNECTORS

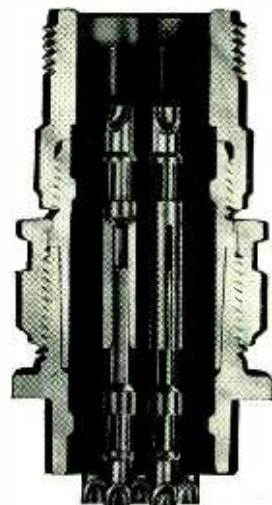
PRESSURE TIGHT SOCKET CONTACTS

PLUS

- **Moisture-proof**
- **Radio Quiet**
- **Single-piece Inserts**
- **Vibration-proof**
- **Light Weight**
- **High Insulation Resistance**
- **Easy Assembly and Disassembly**
- **Fewer Parts than any other Connector**
- **No additional solder required**

Outstanding design and precision workmanship assure completely pressurized electrical connectors for all sizes of contacts. A truly important feature, but only one of the many exclusive advantages that contribute toward making Bendix outstanding in the electrical connector field. Increased resistance to flash over and seepage is made possible by the use of Scinflex dielectric material—an exclusive development of Bendix. In temperature extremes, from -67°F. to +300°F. performance is remarkable. Dielectric strength is never less than 300 volts per mil. Remember, for the greatest value in electrical connectors, it pays to specify Bendix. Our sales department will gladly furnish complete information on request.

PLUS



SHELL

High strength aluminum alloy . . . High resistance to corrosion . . . with surface finish.

CONTACTS

High current capacity . . . Low voltage drop.

SCINFLEX ONE-PIECE INSERT

High dielectric strength . . . High insulation resistance.

Pin and socket arrangements available for all sizes of contacts.



Bendix

SCINTILLA MAGNETO DIVISION of
SIDNEY, NEW YORK

Export Sales: Bendix International Division, 72 Fifth Avenue, New York 11, N. Y.

FACTORY BRANCH OFFICES:

117 E. Providence Ave., Burbank, California • 23235 Woodward Ave., Ferndale, Michigan • 7829 W. Greenfield Ave., West Allis 14, Wisconsin.
582 Market Street, San Francisco 4, California



AVIATION CORPORATION

Mr. BROADCASTER



HERE'S MONEY IN YOUR POCKETBOOK

**Greater Operating Economy
Lower Initial Cost
Longer Life**

You save from every angle when you buy and use transmitters employing Eimac tubes. Saving starts with the initial tube cost . . . you save again every hour you're on the air because of higher tube operating efficiency . . . and you save still further by staying on the air more hours without service shutdown.

Take as an example of Eimac tube economy the rugged 3X2500F3 triode pictured above. Initial cost is \$198.00 each, yet as power amplifiers they will provide 5 kw output per tube . . . that's lots of watts per dollar cost. The dependability of this tube and its high frequency version (type 3X2500A3) has been proven over many years by thousands of hours of life in AM, FM, and TV service.

These tubes are the nuclei around which modern transmitter circuits have been developed and built.

Let us send your engineering staff complete data on the 3X2500F3 and other Eimac tubes for broadcast service. A letter to us will bring the material by return mail.

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TUBES
The Power for R-F

249

BROWN
INSTRUMENTS
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	27 RPM MOTOR	54 RPM MOTOR	162 RPM MOTOR
MAXIMUM TORQUE	Approx. 85 inch-ounces	Approx. 43 inch-ounces	Approx. 19 inch-ounces
MAXIMUM POWER	Approx. 6300 inch-ozs. per minute at approx. 17-18 rpm.	Approx. 6700 inch-ozs. per minute at approx. 30-32 rpm.	Approx. 8150 inch-ozs. per minute at approx. 100 rpm.
POWER REQUIREMENTS	Line field—approx. 9.5 Watts. Amplifier field—approx. 4.0 Watts. Total power—approx. 13.5 Watts.		

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Available in the 3 speeds indicated in the table, this totally enclosed and self-lubricated motor is ideal for service where positive positioning is required. Its low inertia eliminates coasting, promotes maximum effectiveness from any dynamic braking. The motor is designed to have a tapered curve of speed versus voltage and, at the same time, to maintain high

torque at low speeds. Your local Honeywell engineer is qualified to discuss your application. Call him in, today . . . and write for a copy of Data Sheet #10.20-2. MINNEAPOLIS-HONEYWELL REGULATOR CO., Industrial Division, 4428 Wayne Ave., Philadelphia 44, Pa. Offices in more than 80 principal cities of the United States, Canada and throughout the world.

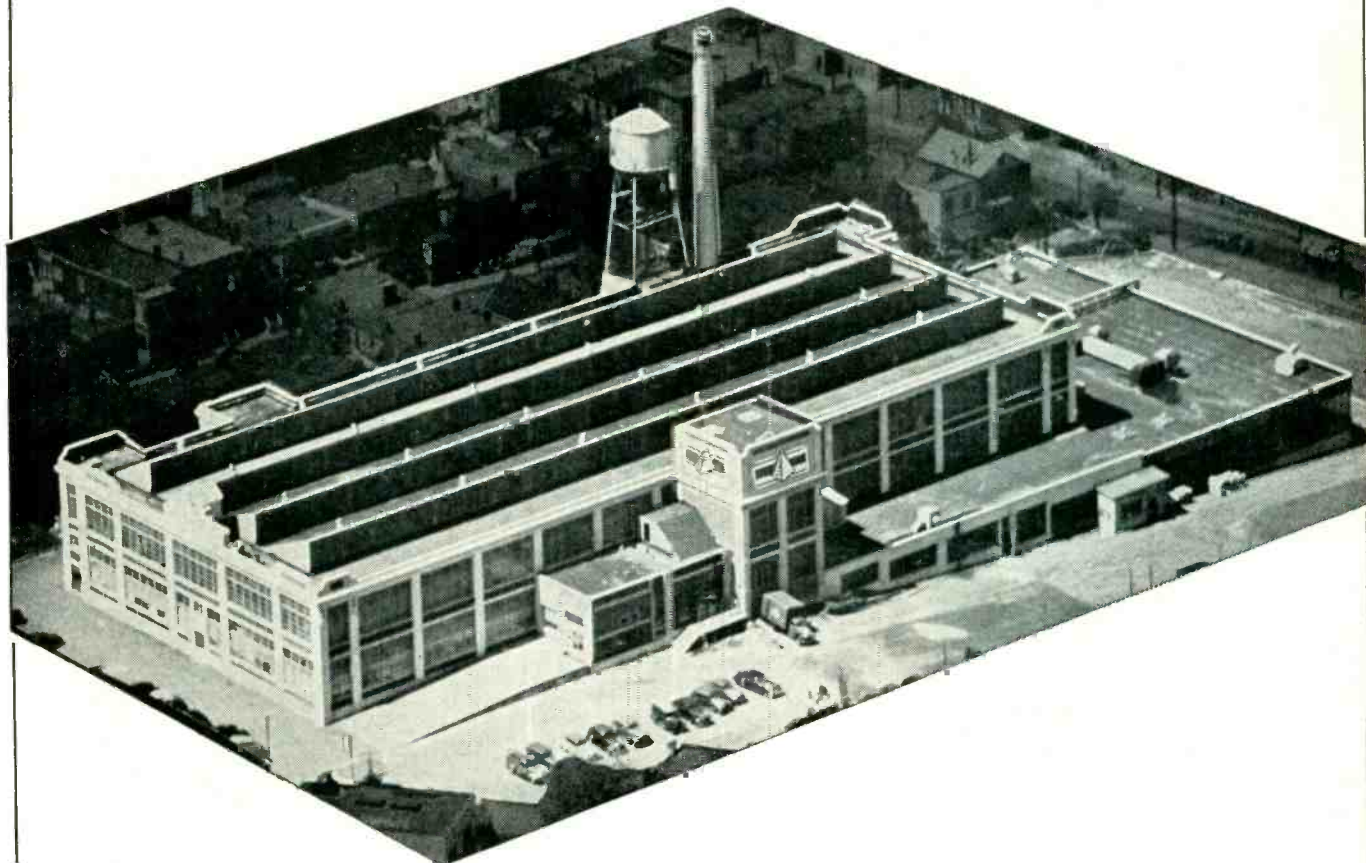
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Audio Fair has made a place for itself among important annual meetings, national in one sense and local in another. Second shindig conducted under the auspices of the relatively young Audio Engineering Society at the Hotel New Yorker pulled more engineers from greater distances to hear technical papers, had 50 percent more exhibits and a larger overall attendance than in 1949. But local dealer-distributors rented many of the rooms and metropolitan-area hobbyists swelled the gate.

Men and women attending moved in a world consisting largely of corner speakers and magnetic amplifiers, amid weird sounds such as those generated by a showpiece recording aptly entitled "Ionisation" that rattled the rafters. There appeared to be a growing trend toward the use of separate remote-control boxes for high-fidelity amplifiers. Incidentally, the desirability of standardized input and output connectors for such amplifiers is becoming evident.

Difficulty of deciding how high high-fidelity should be in new sound system designs is illustrated by the story about a recent listener test in which two units, one cutting off at 5,000 cycles and the other going on up, were compared. A white light indicated when one unit was playing and a yellow light showed when the other was in use. Study of ballots indicated only one thing . . . that people prefer white lights.

Engineers make poor test audiences. Two identical amplifiers were played but when using one of them needle scratch was deliberately introduced into the recording. The technicians assumed that because they heard scratch one amplifier was doing a better job on highs, and voted for it.

United Nations has until recently rented American cameras to handle televising of meetings at Lake Success and Flushing. Now,

according to H. B. Rantzen, who is Director of the Telecommunications Services Division, British units are being tried out too. Most attractive appears to be a type employing an image orthicon, first because equipment must perform at low light levels and, second, because replacement tubes are more readily available.

Specifications for new electronic equipment for UN Headquarters have been written and requests for bids are not internationally. We understand that there are severe financial restrictions so that it is a question of fitting new gear in with equipment already on hand rather than provision of entirely new systems.

650 Radio Patents were the subject of 1,500 suits between 1910 and 1942. Some 35 percent were dismissed or settled out of court, and 30 percent involved consent decrees, validity not being determined. Information regarding the remainder of the suits is obscured in the records.

Of the patents involved, 16 percent were declared valid and infringed, 3 percent valid but not infringed, and 2 percent invalid.

Public Relations are very important to a large lab operating in the midst of a nice residential neighborhood near New York. So before shutting down last Christmas eve the timer on a high-power electronic carillon was set to spread carols over the countryside at 2 o'clock the following afternoon.

The thing went off at 2 a.m.

Wayne Coy of the FCC says there are now 1,200 American ship-borne radar installations.

A Subscriber who works for a southern broadcast station has worked out some of the details of an idea that might be useful to chiropractors. He thinks that if low-voltage a-c is applied each side of a patient's backbone amplified bridge output potential might

The **A-B-C's** of SYLVANIA SILICON DIODES



Applications
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Characteristics

● Here's a fund of up-to-the-minute information about Sylvania Silicon Diodes that belongs in the file of every electronics engineer. This new 16-page booklet describes crystal rectifiers covering the frequency range from 1000 to 25,000 mc per second. It explains the various types of Silicon Diodes with their

ratings and common applications.

The booklet discusses mixer crystals, including the new matched pairs, microwave video detectors and Silicon Diode use in UHF and SHF instrument applications. For your free copy of this new booklet, simply clip the coupon and mail today.

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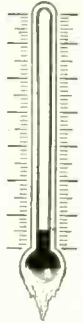
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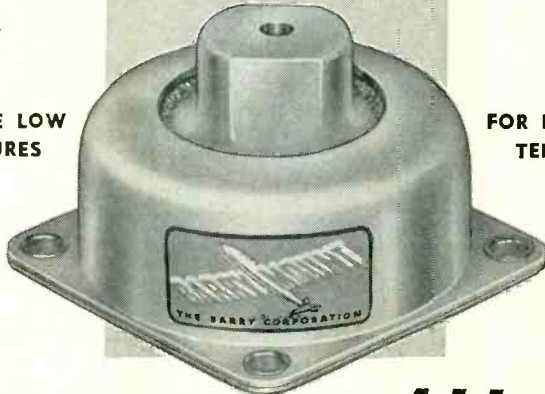
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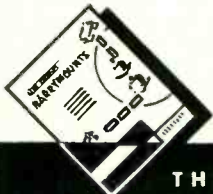


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Design Features of ALL-METL BARRYMOUNTS

- ① . . . Outstanding vibration isolation under severe temperature and environmental conditions.
- ② . . . High shock protection in accelerated take-offs and arrested landings.
- ③ . . . Unit mountings are interchangeable with mountings now in use.
- ④ . . . Complete line of ALL-METL mounting bases to JAN-C-172-A dimensions.
- ⑤ . . . Special ALL-METL bases made to customers' requirements.

FREE CATALOGS give dimensions and load ratings of stock BARRYMOUNTS. Write today for Catalog 509 describing ALL-METL unit mountings and mounting bases. Catalog 502, covering general aircraft applications, and Catalog 504, covering industrial mountings, are also free on request.



THE **BARRY** CORP.

Main Office 707 Pleasant St. • Watertown 72, Massachusetts

New York Rochester Philadelphia Washington Cleveland Dayton Detroit
Chicago Minneapolis St. Louis Seattle Los Angeles Dallas Toronto

indicate differences in tissue resistance associated with nerve impingement and that this might help when diagnosing spine defects.

Component Parts made by electronic equipment manufacturers find their way into an extremely wide variety of end products. Vic Mucher says Clarostat's are used in the following:

- Air cleaners
- Aircraft de-icer controls
- Aircraft wing flap controls
- Alarm systems
- Analyzers
- Antenna dummy loads
- Antenna rotor controls
- Atomic program
- Attenuators
- Audio-frequency amplifiers
- Audio-input amplifiers
- Battery-charging equipment
- Battery-testing equipment
- Boosters
- Cathode-ray oscillographs
- Colorimeters
- Communication systems
- Compasses
- Computers
- Cyclotrons
- Diathermy equipment
- Direction finders
- Electric dryers
- Electrical bridges
- Electrocardiographs
- Electronic dictation machines
- Electronic heating equipment
- Electronic sorters and counters
- Fire-control apparatus
- Fire detectors
- Fuel gages
- Gas detectors
- Graphic recording instruments
- Guided missiles
- Heat-controlling equipment
- Intercommunication systems
- Loran navigational devices
- Meteorological studies
- Microwave amplifiers
- Microwave landing systems
- Mine-detection apparatus
- Monitors
- Optical equipment
- Power amplifiers
- Precision measuring instruments
- Radar microwave amplifiers
- Radar recording cameras
- Radar systems and equipment
- Radiation counters
- Receivers
- Recorders
- Rockets
- Servo amplifiers
- Servomechanisms
- Signal generators
- Sonar
- Sonobuoy
- Spectrophotometers
- Speech scramblers
- Synchrosopes
- Transceivers
- Transmitters
- Transmitter input controls
- X-ray cameras

Advertising of radio and television sets increased sharply in the last half of 1950. An informal poll of RTMA Advertising Committee members indicates that at least 9 percent more will be spent by the average manufacturer in 1951 than in 1950.

Reader who liked our September wheeze about the new AN-system of definitions points out that CU/SBW-8 would indicate the

eighth model of a coupling unit for a remote-controlled shipboard carrier pigeon.

Industrial Television is already at work, according to Bill Norvell of Remington Rand, in the following applications:

- Remote handling of explosives
- Adjustment of bombs
- Rocket-motor testing
- Telemetering
- Atomic research
- Structural testing of aircraft
- Helicopter rotor testing
- Teaching of surgery
- Navy training programs

Other possible industrial applications of television equipment include:

- Observation under water
- Microscopic and telescopic observations
- Night-watchman operations
- Time studies
- Manufacturing production control
- Department-store merchandising
- Sales promotion
- Factory training
- Transmission of business records
- Monitoring of motion-picture sets
- Teaching of dentistry
- Observation of sports fouls
- Transmission of race results
- Transmission of weather charts
- Traffic control
- Civilian defense
- Police-record transmissions
- Railroad-yard inspection
- Reservation information

First widescale use of industrial color television, Norvell thinks, may be in the medical field.

Rectangular Picture Tubes represented 47 percent of all cathode-ray tubes sold to television set makers in July, the first month in which detailed statistics were compiled by RTMA. Eighty-four percent of all c-r tubes sold to manufacturers were 16 inches or more in size.

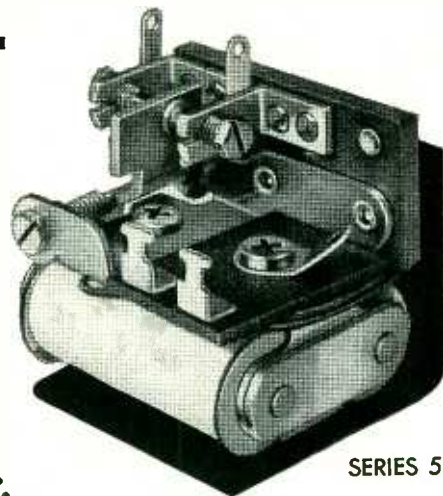
Business Booster that might appeal to other distributors of electronic equipment is the Electronic Industrial Equipment Show recently staged for the third time in three years by Sam Poncher of Chicago's Newark Electric. Sam displayed the products of 27 manufacturers in Hotel Stevens rooms, served drinks and smorgasbord, attracted over 1,500 potential customers.

Gold Bricks are well known. Not so well known are recently marketed lead bricks simplifying the construction of shielding in radioactivity and other research projects.

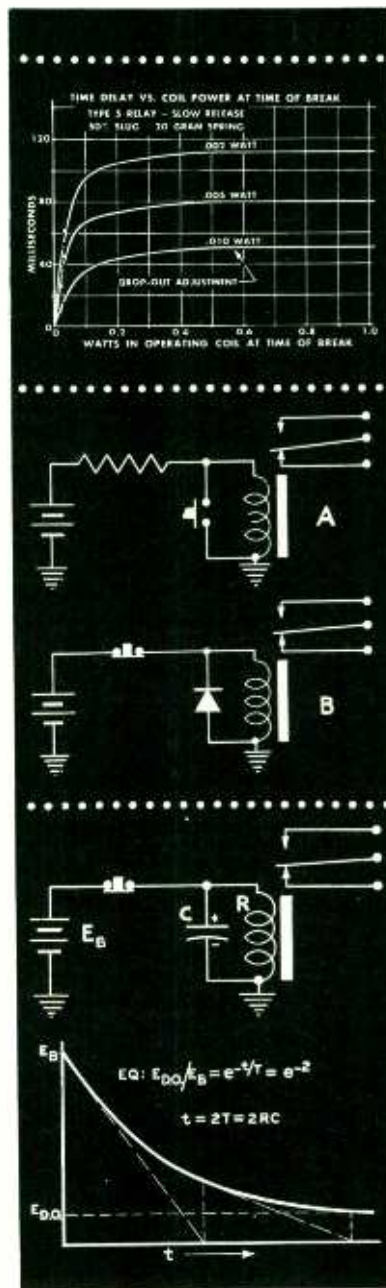
Computer Makers, we are told, soon learn to think in terms of microseconds and megabucks.

INTERVAL TIMING

with sensitive relays



SERIES 5F



Interval timing in the range 0.02 to 0.20 seconds is advantageously accomplished when a *slow releasing* relay can be used. Unlike *slow make* relays of which the operating time is an inverse function of voltage applied to the coil (which affects rate-of-rise of flux), *slow release* relays need only be operated in a saturated condition to give a time delay independent of applied voltage. (See curves applying to pictured relay, with 50% copper slug.)

Time varies as a function of drop-out setting, which on most sensitive relays can be closely controlled with screw adjustment. It also varies inversely with ambient temperature which affects the resistance of the copper slug. Bimetallic temperature compensation can be applied to the above relay to mitigate this.

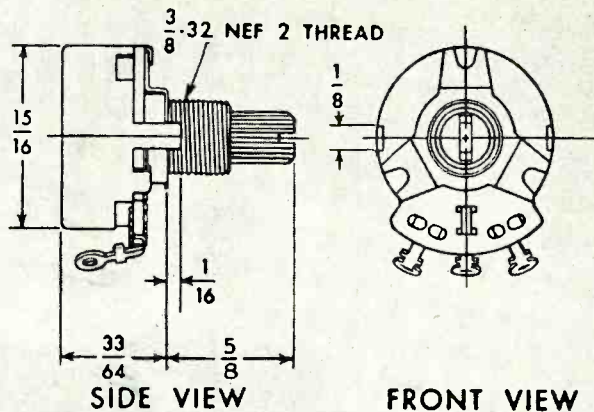
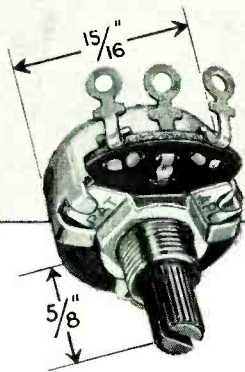
Variations of the same principle are presented at "A" and "B", both involving the use of short circuited operating windings as a "copper slug." At "A" a switch is used to control the relay by means of shorting its coil, resistor R limiting short circuit load on battery.

At "B" a crystal diode shunting the coil is non-conducting to battery potential, but when the switch is opened, provides a low impedance path for the decay of coil current. A variable resistor in series with the diode gives adjustable control of the timed interval.

For intervals longer than attainable with the "slug" principle and where moderate precision is adequate, "RC" methods may be employed. Use of sensitive relays permits smaller capacitors or longer time intervals. In the circuit at left, time of drop out, t , is related to the time constant, $T = RC$, (T seconds R megohms C microfarads), the voltage will equal $0.37E_B$, not necessarily the dropout voltage. In the graph $E_{D.O.}$, the drop out voltage, has been chosen as equal to voltage attained after two time constants. The equation is shown solved on this assumption. Approximate solutions may be attained by taking 37% of E_B , 37% of the result, and so on until $E_{D.O.}$ is reached. The number of times this may be done multiplied by the time constant gives the release interval.

SIGMA Instruments, Inc.
SENSITIVE RELAYS
62 Ceylon St., Boston 21, Mass.

**Service
Beyond
The Sale!**



**15/16" MALLORY
MIDGETROL***

Electrical characteristics specially designed for critical applications in television, radio and other circuits. Insulated shafts are knurled for ease in adjustment. Current-carrying parts provide 1500 volt insulation . . . 15/16" diameter saves space . . . phenolic material eliminates mechanical noise. Precision-controlled carbon element provides smooth tapers, quiet operation, accurate resistance values, less drift in television applications.

*Trade Mark

**Design Standardization
By Mallory**
effects real customer savings!

Mallory goes beyond the basic research and development work which results in totally new products . . . and utilizes every opportunity to pass on to customers the savings effected by product standardization.

Such is the case with the well known Mallory Midgetrol. Standardizing its diameter and shaft design resulted in cost reductions for radio and television manufacturers. The standard molded phenolic shaft provides a combination hand knurl and screwdriver slot adjustment at no extra cost . . . and it is available with either 1/4" or 3/8" bushing length. In addition, the Mallory Midgetrol occupies less space than larger controls, with no sacrifice in wattage rating.

That's service beyond the sale!

Mallory's electronic component know-how is at your disposal. What Mallory has done for others can be done for you!

Television Tuners, Special Switches, Controls and Resistors

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CROSS TALK

► **COBALT** . . . The first real taste of shortage in the electronics industry due to conflict with military needs came last month when the supply of cobalt for civilian production was sharply cut back. Since Alnico 5 magnets are 25-percent cobalt, and since less than 30 days supply of this material was on hand, things looked (and still look) black for production of radio and television sets. An understandable hue and cry arose, to the effect that television and radio production would be shut down tight unless the government relented and diverted cobalt from jet engines to television.

Alnico is used in television sets in focusing magnets, centering magnets, ion traps and loudspeaker fields. Prewar loudspeakers used electromagnets; centering was accomplished by the d-c components in the scanning yoke. Prewar electrostatic electron guns required no focusing coil or magnet; early postwar sets used electromagnetic focusing coils.

If and when the Alnico supply is cut off completely, these older designs must be readopted. The principal problem appears to be the focusing unit, which takes several pounds of Alnico and would take several pounds of copper in a conversion unit. While copper is not so scarce as cobalt, purchasing agents report that getting extra pounds of copper for focus coils is out of the question in today's market. So we may be faced with a return to the electrostatic gun, much longer picture tubes and deeper cabinets.

Since a single jet fighter may be worth a lot of television sets in

months to come there is little point in screaming bloody murder. But if civilian production is to continue, both government and industry must adopt a cooperative and flexible frame of mind. Engineers must be ready and willing to redesign around shortages quickly and cleverly. The management must be willing to prepare for and pay the cost of such conversions. The public must foot the bill. The government must understand that advance notice of impending shortages is absolutely essential to permit conversions to be ready when the restriction order is issued. Otherwise our industry, and a dozen others essential to defense mobilization, will grind to a standstill before defense orders take up the slack.

► **TURNOVER** . . . Not many years ago, most engineers in the radio receiver business had a well-traveled look and a brand new mortgage, the result of too short tenure in too many jobs. Since the war, the turnover has been slower. Our guess is that the majority of radio engineers now 15 years out of college have been in their present job for at least five years. A record of some sort has been hung up by Mark Glaser of DeWald, who recently completed 20 years as chief engineer of that company. During this time he has designed over a thousand different radio and tv sets.

All of which brings up a question: How many different jobs, or changes of employment, should an engineer in electronics anticipate during his professional life? The different-job-every-year pace

that afflicted so many before the war is evidently wrong; it is fraught with insecurity. But is it not also true that the engineer who stays in one company for 20 years (chief engineers excepted) does so at a lower average salary level than the man who makes, say, three changes in that time?

Does the occasional change of job lead to the fuller life, pension rights to the contrary notwithstanding? We solicit opinions, especially from men over fifty (who have had the experience) and under thirty (who may be wondering what the answer is).

► **CURTAIN** . . . About a year ago, we received a letter from a reader who lives in Eastern Europe in which he described an idea for a new type of phototube. In his letter, he explained that he had no means for investigating his ideas, and furthermore, so strict were the rules and regulations behind the iron curtain, that he dared not reveal his identity. This letter was published in the *Backtalk* department of **ELECTRONICS**. After it appeared in print, we received a letter from engineers of the Rauland Corporation, S. Paksver and W. O. Reed, who had taken up the idea and had actually built a tube according to the proposed specifications. A series of tests were run, and while the results will probably not change the course of world affairs, they proved that the author's predictions were correct. A detailed account of the findings appears this month on page 126. Our correspondent is anxious to find a place in our industry. Any job offers?

MILLIMETER

There is a need for tubes and circuits that will operate in the unexploited millimeter wavelength region between microwaves and the infrared. Present unsatisfactory methods using incoherent sources are reviewed and new techniques suggested

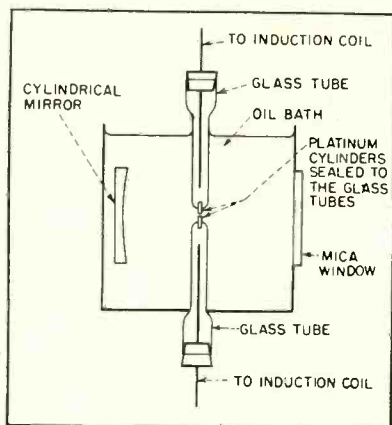


FIG. 1—Lebedew's 0.6-mm spark oscillator used in experiments at the University of Moscow in 1895

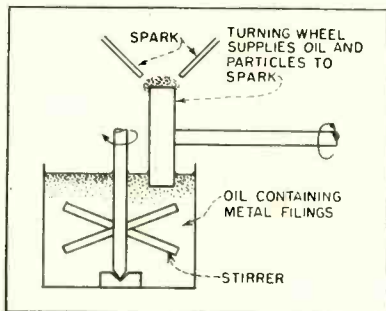


FIG. 2—Glagolewa-Arkadiewa's source of millimeter waves from which radiations from 129 to 50,000 microns were obtained

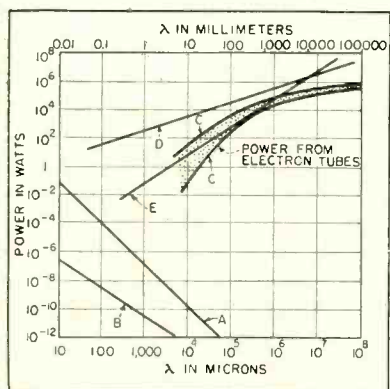


FIG. 3—Present state of tubes at millimeter wavelengths. The dotted area shows the range of average power output available from electron tubes. Pulsed tubes give higher average powers than c-w tubes

ELECTRONIC ENGINEERS and physicists have worked extensively with radiations at most wavelengths available in the spectrum. There is, however, a little-exploited gap, that between the longest infrared and the shortest microwaves. This is the region of millimeter waves.

As the physicist pushes his spectroscopic measurements to longer and longer wavelengths, the energy available from his hot source of illumination becomes less and less intense. There is little energy per quantum, not enough to eject electrons, and sensitive photocells give way to heat-detecting bolometers which employ thin wires or films of metals or semiconductors, or to Golay cells which measure heat by the expansion of a small body of confined gas.

Because little energy is available in a given frequency range, carefully designed and efficient lamellar or echelon gratings must be used which conserve all that it is possible to save of the scant energy. Further, energy must be integrated or collected over periods of the order of a second, and measuring equipment becomes sluggish. Finally, at wavelengths of around 1,000 microns or 1 millimeter, infrared spectroscopy peters out.

To pursue their interest at still longer wavelengths, physicists must have more powerful sources of radiation. One possibility is to use incoherent sources of radiation whose properties are similar to the hot-body sources used in the past.

A 60-cycle a-c generator and a vacuum-tube oscillator are coherent sources; they generate a smooth sinusoidal signal of a single frequency. The radiation from an incoherent source consists of many short wave trains of random or unrelated phase. Mathematical analy-

sis or measurement with a spectroscope or a frequency meter shows that such incoherent radiation covers a band of frequencies.

Incoherent Sources

Aside from hot bodies, the most familiar generators of incoherent radiation are spark-excited oscillators such as Hertz used in his original experiments. Indeed, P. Lebedew generated 0.6-mm waves with a spark oscillator at the University of Moscow in 1895 (Fig. 1), and in the 1920's Nichols and Tear generated 0.22-millimeter (220-micron) radiation with a similar device, thus invading the field of the long infrared with an electric generator. More recent spark generators have used tiny ball bearings bouncing between charged electrodes, or a stream of mercury droplets striking an electrode.

Mass radiators have also been used in the electrical generation of incoherent millimeter waves. From 1924 to 1929 Mme. Glagolewa-Arkadiewa of Moscow used a device in which metal particles suspended in oil were carried into a spark by a rotating wheel (Fig. 2) and obtained radiation of wavelengths ranging from 129 to 50,000 microns. Similar work has been carried out by Lewitsky (1924-27) and more recently by Cooley and Rohrbaugh (1945).

The exact mechanism of mass radiators seems somewhat in doubt. Recently H. A. Prime, following a suggestion of Frohlich, dropped copper powder through an arc and obtained enhanced radiation in the vicinity of an ionic resonance of the copper crystal.

Although spark generators or mass radiators might be used to extend the range of infrared spectroscopy, they suffer from the limitation of all incoherent sources.

WAVES

By **JOHN R. PIERCE**

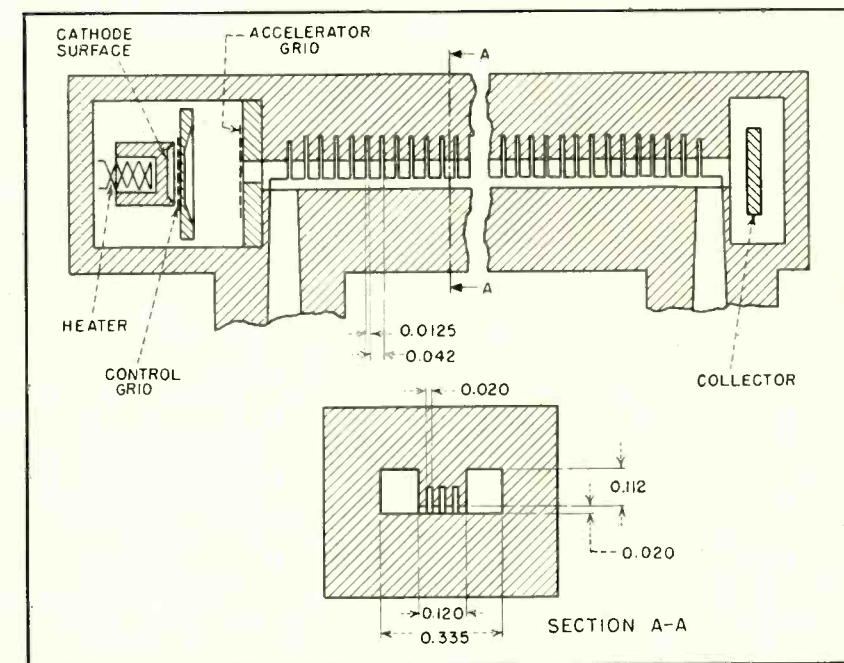
*Bell Telephone Laboratories
Murray Hill, N. J.*

The spectroscopist wishes to measure absorption or reflection versus frequency. For finer detail, a spectrometer of higher resolving power must be used and a smaller fraction of the total radiation selected. Thus, the spectroscopist who uses an incoherent source must build a larger spectrometer which will have greater resolution, but he has less energy left to work with as he does so. He envies radio-frequency and microwave spectroscopists who have available sources (electron tubes) which are essentially monochromatic (single-frequency).

Need Coherent Source

With a monochromatic or coherent millimeter source, physicists could obtain the higher resolutions they need to untangle the behavior of matter. Physicists are delighted that molecules in vapor form in the atmosphere and molecules of liquids and solids as well absorb millimeter waves for this enables them to study these molecules. Although this pronounced absorption of millimeter waves is something of a nuisance to communication engineers, it is not such as to rule millimeter waves out of consideration for short-range communication through the atmosphere or perhaps even for longer-distance communication through evacuated or gas-filled waveguides. Thus, both physicists and engineers are anxious to obtain electron tubes which will operate in the millimeter range.

Unfortunately, as electron tubes are made smaller to operate at shorter wavelengths, they are harder to build. Circuit losses increase as the square root of the frequency, an irremediable defect which can prevent some sorts of tubes from operating at all. The required small cathodes can scarcely furnish the currents neces-



Cross-sectional view of a spatial-harmonic traveling-wave tube operating at 1.25 cm

sary to make the tubes operate. Millimeter-wave tubes thus tend to be inefficient and short lived. But worst of all, the tubes can scarcely dissipate by conduction or radiation the large part of the electric input which is converted into disorganized heat rather than into millimeter-wave energy.

Spectrum Range

Curve A of Fig. 3 shows the characteristics of the radiation per cm^2 from a black body at a temperature of 5,000 Kelvin for infrared radiation. This is in a frequency range of one percent, which would allow a spectral resolution of one part in 100. Curve B is for the same black body at the same temperature but with radiation per cm^2 lying in a bandwidth of one megacycle, a broad band in terms of radio, but a narrow bandwidth in terms of spectroscopy.

The dotted region of Fig. 3 is intended to include, roughly, the average powers presently attainable with electron tubes, in an easily assimilable form. The spread is partly a confession of ignorance or uncertainty. However, at the shorter-wavelength end of the

range the spread is such as to include the average power of pulsed tubes as well as that of c-w tubes. Pulsed tubes tend to have the higher average powers, but their radiation is not monochromatic; it covers a bandwidth of around a megacycle.

Electron tubes as millimeter-wave sources have an advantage beyond that of being monochromatic or coherent; they also give a power tremendously greater than that available from hot bodies for any reasonable bandwidth or resolution. The fact that physicists have been able to use thermal sources at all for measurements, even in the slightly submillimeter range, is a tribute to their care and ingenuity in making slow and painstaking observations.

The other striking feature is the rapidity with which the power output of tubes falls off at short wavelengths, see curves C of Fig. 3.

Suppose we consider an electron tube of a given type, say, a magnetron, which has a diameter D , which operates at a voltage V , a current I and a magnetic field B at a wavelength λ , and gives at that wavelength a power output P . Now

imagine that we made a magnetron just half as big in every respect. Suppose the circuit Q (or loss) were unchanged by this scaling (something which will be disclaimed later). If the operating conditions in the following table were observed, the power output would, as indicated, be unchanged.

	Original Tube	Scaled Tube
Diameter	D	$D/2$
Voltage	V	$V/2$
Current	I	I
Magnetic field	B	$2B$
Wavelength	λ	$\lambda/2$
Power	P	P

Of several things wrong with this picture, the worst is that of carrying away the heat produced because the tube is not a perfectly efficient converter of direct current into alternating current.

In the scaling process the size is proportional to the wavelength. Moreover, in millimeter-wave tubes the size tends to be comparable with a wavelength. For a given structural part, the heat conducted through it for a given temperature difference is proportional to the linear dimension. Curve *D* of Fig. 3 shows the power conducted through a copper cube a wavelength on a side for a temperature difference of 1,000 C.

Power can also be carried away by radiation, and curve *E* of Fig. 3 shows the power radiated from a black surface a wavelength square at 1,000 Kelvin. It is no coincidence that the available power tends to be low at short wavelengths, where the conducted and radiated powers are small.

Need for Large Tubes

A typical miniature pentode which can be used at a frequency of 500 megacycles is about an inch long. The grid is wound of wire 0.001 inch in diameter, and the spacing between cathode and grid is about 0.002 inch. The following table shows what the dimensions would have to be if the tube were scaled for operation at 6 millimeters (50,000 mc).

	500-mc Tube	50,000-mc Tube
Length	1 inch	1/100
Grid wire diameter	1/1000 inch	1/100,000
Cathode-grid spacing	1/500 inch	1/50,000

This is clearly ridiculous.

The vital circuit portion of a 6-

millimeter traveling-wave tube of somewhat less power output scaled for operation at 500 mc, would be 6 inches by 17 inches in cross-section, and 17 feet long, which is equally ridiculous.

All of the tubes used in the millimeter range are large for the wavelengths at which they operate. Klystrons, magnetrons and traveling-wave tubes are used in the millimeter range in preference to triodes not because they are better tubes in any fundamental sense, but because they are large enough to be built and to carry away the heat generated in their rather inefficient operation. If a tube could be evolved whose smallest part or closest tolerance was still larger compared with the wavelength of

the circuit loss varies inversely as the square-root of the wavelength. This, combined with compromises as to current density and feasibility of construction make it hard to build operable tubes of some types (notably, klystrons) for the millimeter range.

Pulsing offers a way out of this dilemma. Momentarily, cathodes will emit large currents, and while the temperature of the parts rises steadily during the microsecond or so of operation, the parts have a chance to cool down again in the interval between pulses. Finally, high-voltage tubes are larger and easier to build than low-voltage tubes, and pulsing enables one to go to high voltages as well as high currents.

Experimental Tubes

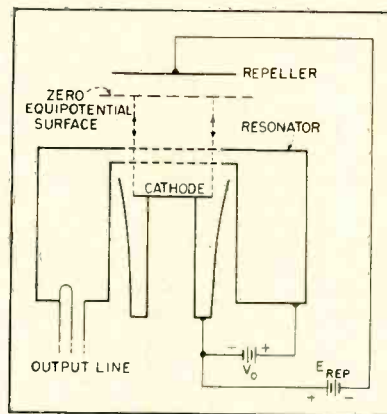
Some of the best tubes in the millimeter range have been pulsed magnetrons. The table below shows some of the results which have been achieved at the Columbia Radiation Laboratory.

Wavelength in mm	Peak Power in kw	Efficiency in percent
6.3	30-40	15-20
4.3-4.8	5-15	4-10
3.0	1-2	1-5

Even higher frequencies have been obtained as harmonics of the frequency oscillation, the shortest wavelength being 1.45 mm (207,000 mc), as the third harmonic of a 4.35 mm tube. The powers obtained are, however, very small.

The output of a pulsed tube consists of a band of frequencies of width inversely proportional to the pulse length. For some purposes a steady, single-frequency signal is desirable. So far, reflex klystrons have been chiefly used to produce continuous waves in the millimeter region. Tubes operating at several thousand volts have produced several tens of milliwatts at around 8 millimeters wavelength and a few milliwatts around 5 millimeters. Tubes operating at 400 volts have also operated at wavelengths a little longer than 6 millimeters. In this part of the millimeter range, however, resonator losses are so great that the tubes barely oscillate.

While no tubes are completely immune to the bad effects of circuit losses, some, like the traveling-wave



Basic circuit of a reflex klystron, an oscillator which has been used down to wavelengths of about 5 mm

operation, on these grounds, at any rate, it would be a good candidate for the millimeter region.

Besides matters of thermal dissipation and of ease or indeed feasibility of fabrication, two important considerations are cathode current density and circuit loss. If the current density rather than the current were kept constant in going to shorter wavelengths, the current itself would vary inversely as the square of the frequency, and the power would vary accordingly, if the tube would oscillate at all. Usually, a sort of compromise is made, and the cathode current density is raised in going to shorter wavelengths, but not inversely as the square of the wavelength. This compromise tends to degrade the performance of the tubes.

Coupled with this is the fact that

tube, suffer less than others. In a traveling-wave tube, a beam of electrons moves along near to a circuit which can guide a slow electromagnetic wave. The electrons are given a velocity nearly equal to that which the wave has in the absence of electrons. If the circuit or the electron stream is excited, the signal is found to increase in amplitude as it travels along the combination of circuit and electron stream. The signal always increases if the circuit and stream are long enough; loss merely makes the increase somewhat less.

Traveling-wave tubes have been built in many physical forms for many frequency ranges. In the millimeter range, gain has been obtained around 6 mm both with a tube using a helix or coil of wire as a circuit, and also with a more rugged circuit consisting of slots or resonators cut in a ridge of metal.

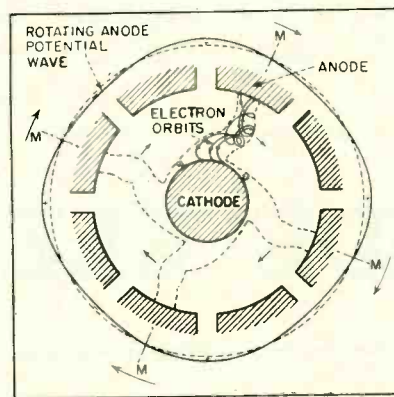
The traveling-wave tube can be regarded as made up of two systems, each capable of sustaining waves. One is the electromagnetic circuit, which can carry electromagnetic waves. The other is the electron stream, along which waves of charge density, velocity and potential called space charge waves can travel. When one system (the electron beam) moves with respect to the other (the circuit) at such a speed that the backward wave on the moving system is in synchronism with the forward wave on the fixed system, the waves interact or combine to form an increasing wave which gives gain. This suggests using two electron streams of different velocities rather than one electron stream and a circuit.

Possible Solutions

In the double-stream amplifier, two nearby or interpenetrating streams of electrons of different speeds interact to sustain a wave which increases in amplitude as it travels. This indicates a possibility of obtaining gain at millimeter waves without the fragile and lossy circuits which are used in other tubes. Unfortunately, circuits are still necessary to put the signal onto and take it from the electron stream. This, together with some difficulties in intermingling the electron streams, have so far stood

in the way of making double-stream tubes for the millimeter range.

In the double-stream amplifier, the two streams of electrons are drawn from two cathodes held at different potentials. Experimental and theoretical work by Haeff, Macfarlane and others indicates that gain can be obtained when all the electrons come from one cathode, provided electrons in different parts of the stream have different velocities, as they do because of space-charge effects. Both beams of electrons traveling in the direction of a magnetic field, and electrons traveling normal to crossed electric and magnetic fields, as in the magnetron, have been considered. As yet, such single-stream amplification is little explored and imperfectly understood, and it is pos-



Electron paths in a magnetron oscillator, showing spokes formed by bunching effect of r-f fields of the anode

sible that substantial progress is yet to be made.

Another device related to the traveling-wave tube is the multi-resonator klystron, in which a beam of electrons is shot past or through a series of uncoupled resonators and an increasing wave is so obtained. In one device, the easitron, the resonators are merely a series of half-wave wires, arranged like the rungs of a ladder.

The operation of the traveling-wave tube may be related in some way to the phenomenon of Cherenkov radiation. This radiation takes place when a charged particle moves through a medium at a speed faster than the velocity of light in that medium. In traveling-wave tubes the electrons travel faster than the increasing wave.

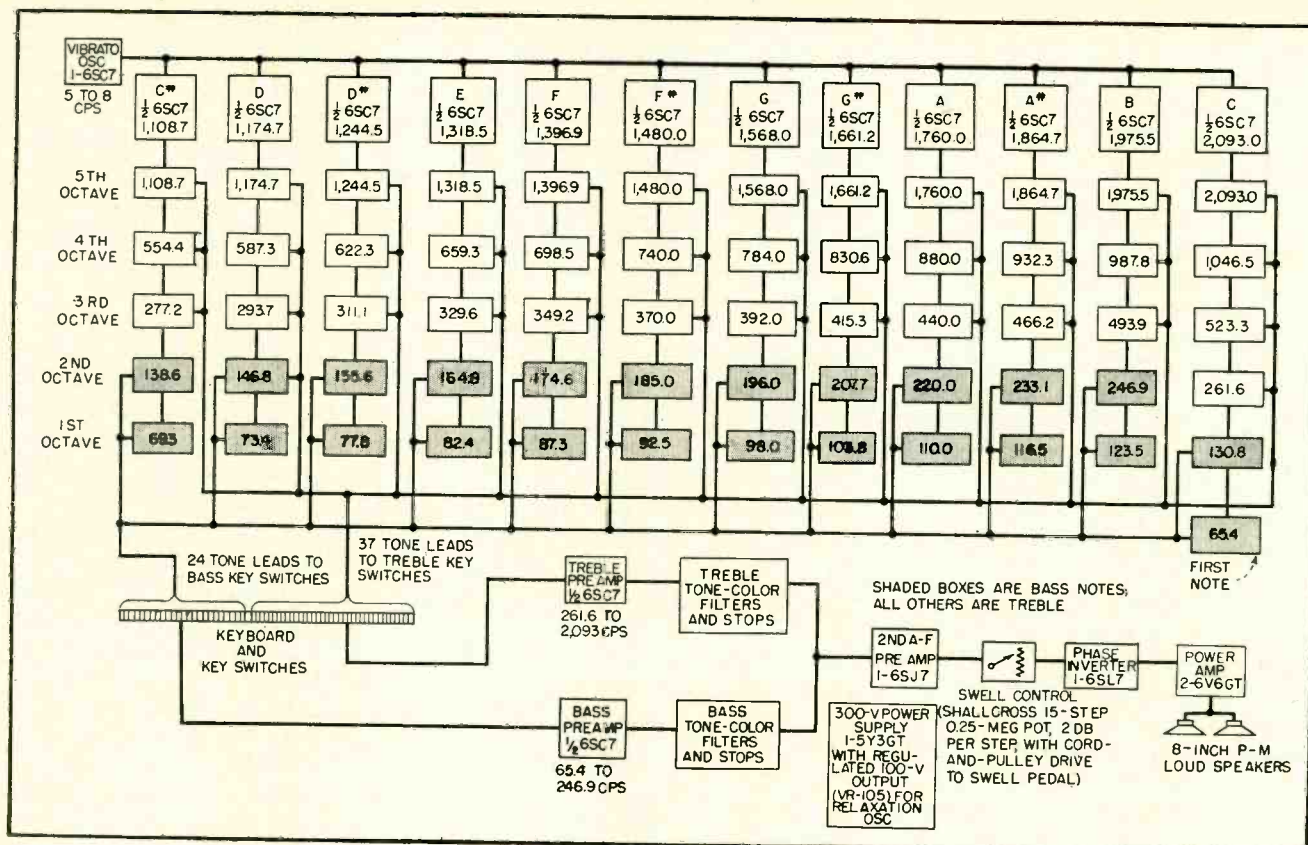
No more detailed comparison has been worked out. It has been proposed that Cherenkov radiation of electrons traveling close to the surface of a dielectric might form a source of millimeter wave power.

One scheme has been called the "relativistic doppler" method of generating millimeter waves, on which Coleman at MIT has been working. Electrons which oscillate back and forth radiate. If the electrons move toward the observer, the frequency of the received radiation is larger than the frequency of electron oscillation; this is the doppler effect. Suppose a stream of high-velocity electrons is shot between the poles of a series of magnets which alternately produce magnetic fields in opposite directions. These fields deflect the electrons back and forth (normal to the direction of motion) at a high frequency as the electrons travel.

Electromagnetic waves of an even higher frequency will be generated and radiated in the direction of electron motion. Fortunately, it turns out that most of the radiation lies in a narrow cone in the direction of electron motion. While some radiation will be obtained from the individual electrons of a smooth beam, the radiation is greater if the electrons travel through the magnetic field in groups or bunches, and hence it is planned to bunch the electron beam as in a klystron before it enters the magnetic field.

Electrons which circle in a magnetic field radiate at harmonics of the rotational frequency, and this radiation has been suggested as a source of millimeter waves. Finally, various combinations of electron acceleration and slowing of waves by dielectrics have and will be considered.

While the most pressing problem in connection with millimeter waves is that of generation, there are other problems as well. Methods of detection must be somewhat different from those which are used at longer wavelengths. Competing means of handling millimeter waves such as optical, waveguide, and others must be worked out and evaluated. Finally, there is the field of application, in spectroscopy, in communications and in radar.



GAS-DIODE ELECTRONIC

Chains of sawtooth tone generators using 10-cent neon lamps are synchronized to master oscillators for frequency control. Undesired harmonics are removed with tone filters to give five octaves of organ-like music with two vibrato stops and six tone-color stops

ELECTRIC-KEYBOARD musical instruments may be classified into two main groups according to their means of tone production: (1) electromechanical generators; (2) electric-circuit generators. Mechanical systems are either rotary or vibratory. Both means have been used to modulate electrostatic or magnetic fields or beams of light. Electric circuit types have employed both vacuum and gas-tube oscillators as tone generators.

Designers of new instruments have either imitated existing instruments or have devised completely new pleasing tonal qualities and controls. However, one of the greatest complaints against electric

instruments is that they are generally too perfect, and therefore unnatural. Variation is the essence of musical expression and variations in pitch, loudness, tone color and vibrato should be within easy control of the musician. On the other hand, too many controls confuse or discourage the performer. In general, new instruments should be easily operated by masters of similar existing instruments.

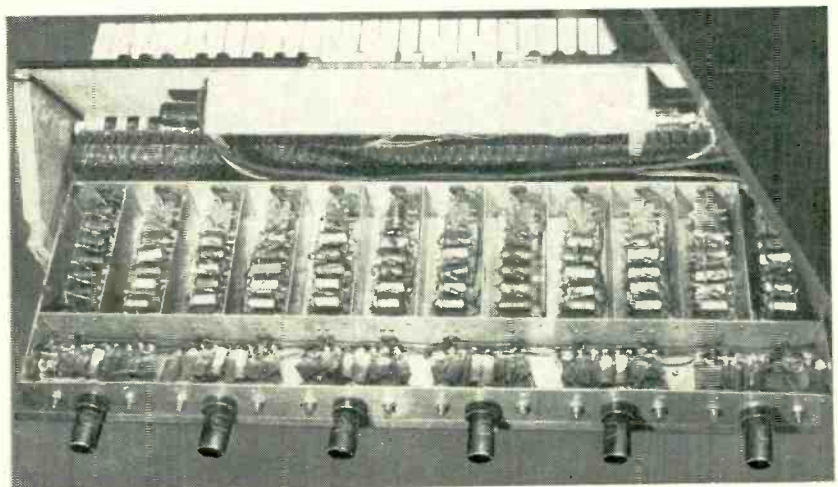
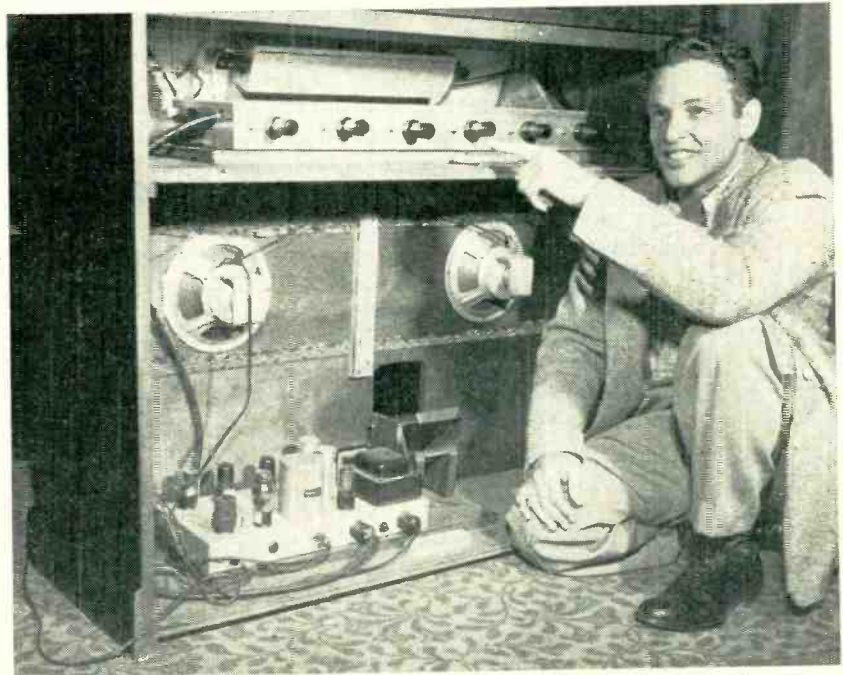
It was required to develop an organ-like electronic instrument that would retail for \$800, whereas the cheapest all-electronic organ then available sold for about \$3,000. Since mechanical economies in the design and construction of the

console and keyboard would classify the equipment as a toy rather than a musical instrument, it was necessary to retain the standard form of the other low-priced organ-like instruments. The main savings were effected in parts and production costs, with minimum sacrifice in performance. A standard organ keyboard of five octaves or 61 notes covering the range from C 65 to C 2,093 cycles is used. The controls consist of eight organ stops; two are used to select vibrato rates and the remaining six are for tone color. A swell pedal is provided for output level or volume control.

The cheapest double-triode vac-

FIG. 1—Arrangement of stages in complete organ. Frequency value in cycles is given for each master oscillator (top row) and each of the 61 synchronized NE-2 neon-tube relaxation oscillators comprising the five octaves. Shaded boxes represent bass notes

TOP: Complete organ being played; CENTER: Rear view of console, showing general arrangement of electronic units; BOTTOM: View of chassis containing the twelve master oscillators and twelve octave chains. Total tube complement is eight 6SC7, one 6SJ7, one 6SL7, two 6V6GT, one 5Y3GT, one VR105 and 61 NE-2 neon diodes



ORGAN

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uum tube, the 6SC7, lists for \$2.00. The cheapest gas diode, the NE-2, lists for 10¢. For this reason, gas-tube methods of tone generation were thoroughly investigated. As it happens, the sawtooth waveform of the gas-discharge relaxation oscillator has a high harmonic content, permitting wide variation in tone color by removing the undesired harmonics with suitable filters. The main difficulty was, of course, with frequency stability.

Actual Design

The block diagram of the complete instrument is shown in Fig. 1. The twelve separately-tuned master oscillators generate continuously

the twelve frequencies for the highest of the five octaves provided. For each master oscillator there is a chain of sawtooth tone generators, the first of which is synchronized to the fundamental frequency. Only these harmonic-rich sawtooth generators feed the preamplifiers and tone-color filters; the master oscillators serve only for frequency control and are not heard.

Each master oscillator synchronizes its corresponding submultiple notes in cascade fashion. Of course, octave submultiples are the only frequencies that may be synchronized in a musical instrument, since the others are not exactly related in the equally-tempered scale.

The 61 sawtooth tone generators are continuously in operation, with all their output leads terminating at the keyboard switches. Twenty-four of the generators feed the bass preamp, and the remaining 37 feed the treble preamp. When the musician depresses one or more keys, the corresponding key switches send the tonal combination to the treble and/or the bass preamp. Stops at the control panel select the desired combination of tone color. The bass and treble tone-color filters then separately modify the upper and lower portions of the keyboard and inject their combined outputs at the second preamp grid. The input level to the phase inverter is controlled by a step potentiometer operated by

the foot of the performer. The signal continues through the power amplifier to the dual-speaker combination.

The main factors affecting the frequency stability of gas-discharge oscillators were found to be applied voltage and incident light. Voltage was readily stabilized within 2 percent with a VR105 regulator tube. It was necessary to introduce a small amount of light for proper operation at the lower frequencies. This effect was accomplished by placing ordinary six-volt dial lights near the low-frequency gas diodes.

The necessary additional stabilization was obtained by subjecting the tubes to a small electrostatic field at the controlling frequency. By using a portion of the output from one oscillator whose frequency was already under control to synchronize another at a submultiple frequency, octave divider chains were developed. Three or four turns of hookup wire provided sufficient coupling for reliable control within plus or minus 10 percent of the free-running frequency.

Figure 2 shows a typical octave-divider chain. The charging capacitors for the first three stages are connected so that the output voltage to the treble preamplifier approaches -100 volts according to the relation:

$$V = 100 (1 - e^{-t/RC}) \quad (1)$$

The time for discharge is extremely

short compared with the time required for the voltage to increase from the extinction voltage V_e to the ignition voltage V_i , so that the free-running frequency of oscillation is mainly a function of the difference between these two voltages¹. Substituting V_e and then V_i for V and taking the reciprocal of the difference between the two corresponding values of t , the frequency of oscillation becomes

$$f_o = \frac{1}{RC \ln \left(\frac{100 - V_e}{100 - V_i} \right)} \quad (2)$$

This expression is approximate because V_e and V_i are themselves affected by frequency, incident light, temperature and magnitude of the discharge current.

At the point of ignition, in the first three stages, the output voltage rises very quickly to +100 volts. The last two tubes in the chain, V_4 and V_5 , are connected so that a positive-approaching sawtooth is produced. It was found that the steep time rise at the point of discharge in the negative sawtooth is much more effective in controlling the positive-sawtooth generators than other combinations. Because the lowest frequencies are the more difficult to control, the last two tubes in the chain are both controlled by the steep negative sawtooth. The first three tubes in the chain, V_1 , V_2 and V_3 , are controlled directly by the master oscillator.

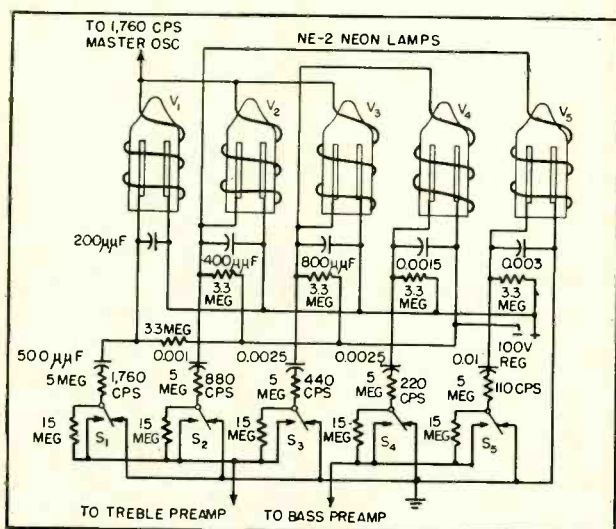


FIG. 2—Example of octave divider chain. For 6-note C chain, sync signals are injected in slightly different order so that the two lowest notes (most difficult to control) are triggered

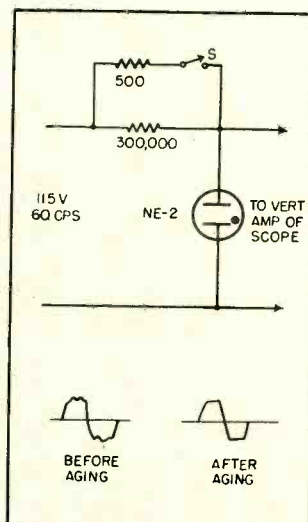


FIG. 3—Neon-lamp test and aging circuit for improving stability of sawtooth oscillators

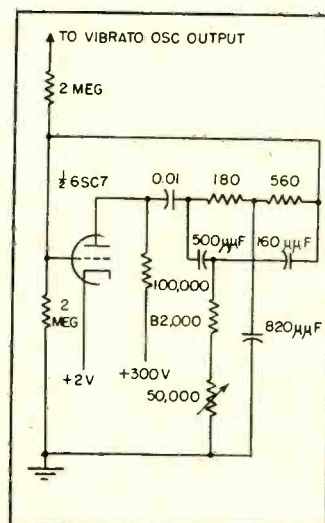


FIG. 4—Typical master oscillator circuit, with component values for the 1,760-cps chain

The charging resistance was adjusted to about 3.3 megohms in all cases. This value represents a compromise between higher values, which would be more unstable against temperature variations and would limit the discharge current, and lower values that operate the tube too near the border between oscillation and continuous glow. For all other factors remaining constant, Eq. 2 shows that if R is increased, C must necessarily be reduced if frequency is to remain constant. A reduction in C means less energy storage in the capacitor and therefore less discharge current. If R is too low, the charging current will be so high that the tube is unable to extinguish at the completion of capacitor discharge, which results in continuous glow.

Switches S_2 through S_5 are mechanically linked to the playing keys. When in the up position, these switches ground the outputs of all unplayed oscillators and also parallel the 15-meg resistors from grid to ground of the preamps, giving 0.625 meg and 0.405 meg respectively at the bass and treble inputs. As a key is depressed and the ground connection removed, a 28-db loss of available oscillator output for bass notes and 31-db loss for the treble is momentarily sent to the preamps. When the key has completed $\frac{3}{4}$ of its stroke, the 15-meg resistor is shunted, thereby allowing playing level. In this manner the loud transient click that would otherwise be present has been almost completely eliminated.

Despite these precautions against transients, key switches with silver alloy contacts caused considerable clicking. Evidently these high-impedance circuits were extremely sensitive to the slightest oxide coating at the contacts. Even the best silver forms a slight coating under normal conditions. The final switches were formed from Nichrome V wire. Clicking was unnoticeable and these switches have maintained their characteristics for a long period of time.

After the first experimental model had been in use for several months, a few oscillators drifted out of their range of control. It was determined that an aging process within the tubes had taken

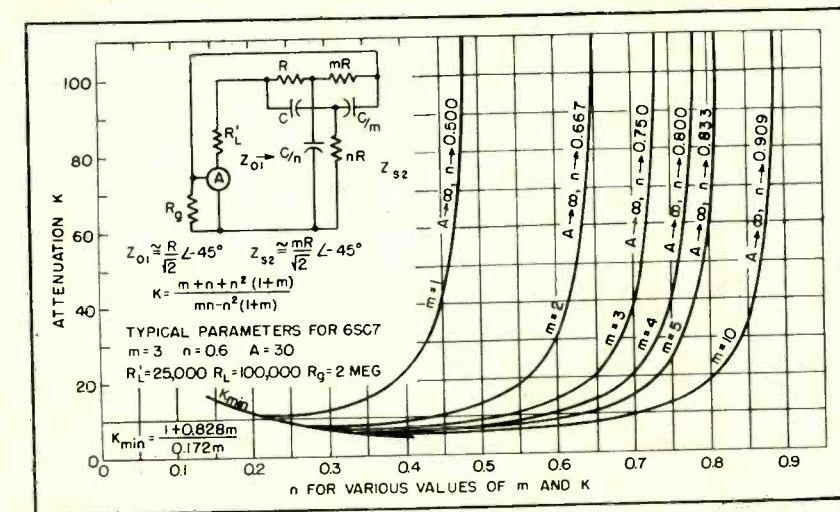


FIG. 5—Design curves for determining parameters of parallel-T networks in master oscillators

place. It was observed that the glow in troublesome tubes was irregular and unevenly spread over the electrode area. When these tubes were tested as positive and negative peak clippers in the circuit of Fig. 3 (switch S open), they failed to produce square and symmetrically clipped sine waves. When the switch was closed for several seconds, allowing about 200 ma to flow, the glow started unevenly but gradually spread over the entire area of both electrodes. At the completion of this spread, the switch was opened because continued application of this high current overheats the electrodes and destroys their photosensitive coating. After proper aging, the wave is always symmetrical and squarely clipped. Uniform characteristics throughout the remainder of their life were thereby assured. The experimental model has remained in synchronism for well over a year.

Master Oscillators

At the frequencies corresponding to the twelve notes in the highest octave, twelve stable oscillators were used to control eleven chains of five notes and one of six to account for the extra C at the low end. Because of its high stability and low parts cost, the parallel-T circuit was chosen. Stabilities of 0.1 percent are possible without supply-voltage regulation. Since only one triode per oscillator is required, two master oscillators may be housed in one double triode tube. Typical circuit constants of the

A-chain master oscillator are shown in Fig. 4.

To aid in determining the parallel-T network parameters, the curves for Fig. 5 were plotted from equations already derived². This presentation assumes zero generator impedance and infinite load impedance. Therefore, the network open-circuit input impedance Z_{01} should be much greater than the generator impedance R_g' and its short-circuit output impedance Z_{s2} should be much less than the load impedance R_L in order that the network balance conditions be least disturbed. After stage gain A has been determined by the tube and load resistor selected, n as a function of A for various values of m may be read directly from the curves.

For sustained oscillation, network attenuation K must be less than stage gain A . If there is no loading on the network and constants are to exact tolerance, K could be taken equal to A . This is, of course, impossible and for reliable operation, K should not be more than one-half A . In most of the literature on the subject, m is taken equal to one.^{3,4} It should be noted that increased selectivity as well as decreased K occurs as m is increased.

The more common method of increasing selectivity is to increase A only. With high- μ triodes the upper limit on A is about 35, so that if additional selectivity is desired, increasing m is a convenient method. With these limits in mind

the following criteria for the design of a single-stage triode parallel-T oscillator were therefore adopted: (1) A was determined from μ , R_L and r_p ; (2) K was set equal to $A/2$; (3) the highest value of m that will allow Z_{12} to remain much less than R_p was selected; (4) Z_{01} was made much greater than R_L' ; (5) at the chosen value of m , n was found for K calculated above; (6) only points well above the K_{min} curve and below where K changes rapidly with small changes in n were used; (7) $C = 1/\omega R$.

Although the design was time-consuming and the required low-tolerance components are expensive, the production cost per oscillator is less than for other types and stability is comparable with a laboratory standard.

Vibrato Oscillator

Vibrato in most musical instruments is produced by combined frequency and amplitude modulation. However, a rather pleasing effect may be obtained from frequency modulation alone. Figure 6 shows the vibrato oscillator, which is a standard four-section phase-shift variety.⁵ Frequency is adjusted to about six cycles per second and is controllable at the stop tabs by simultaneously varying two of the 1-meg resistors in the phase-shift network. Oscillator output is injected through the 2-meg resistors shown in Fig. 4 to the grids of all master oscillators. The extent of the frequency swing or vibrato depth is determined by the amplitude of the injected voltage.

Tone-Color Stops

The raw sawtooth waveform from the tone generators could hardly pass for music because of its improper harmonic distribution. After this sawtooth has passed through filter circuits that alter its harmonic structure, many pleasing tonal effects are obtained.

The highest note on the keyboard of this instrument is the 32nd harmonic of the lowest. A low-pass filter designed to remove certain harmonics of the treble notes would have negligible effect on bass notes. In like manner, another low-pass filter with a much lower cutoff point would be very effective in coloring bass notes and yet completely at-

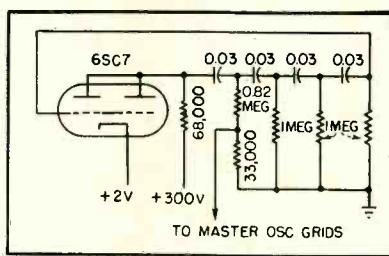


FIG. 6—Vibrato oscillator circuit. Output frequency is approximately 6 cps

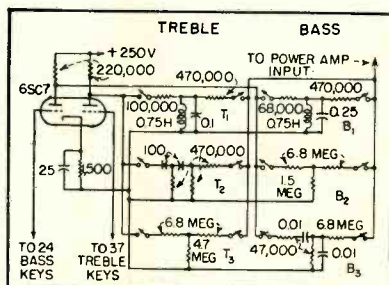


FIG. 7—Bass and treble tone-color filters, each using half of the 6SC7

tenuate the treble section. If uniform tone color were required, a separate filter for each tone color of each note would be needed. However, few instruments have the same tone color throughout their range.^{6,7} A satisfactory tonal balance was obtained by splitting the keyboard at middle C (261 cycles). Two filter sections were provided. The 24 notes below middle C were routed to bass stops or filters and the 37 above to treble stops. When a bass note is played and a bass stop is closed, a tone is produced that in pitch is determined by the note played, in color is designated by the stop closed and is at a level depending on the setting of the swell pedal. Figure 7 shows circuit constants of the tone color unit. One filter in each section is a resonant band-pass type designed to act as a formant-producing element. (Formants are caused by boosting partial tones around a particular resonance frequency.) The others are ordinary R-C networks. These combinations produce horn, string and reed effects. Large amounts of insertion loss were deliberately incorporated in each network in order that output level would be noticeably increased as more stops were closed.

Choice of Speakers

The distortion of the 8-watt amplifier used was held to a mini-

mum consistent with parts cost, but best speaker performance (oddly enough) was realized with one of the least expensive combinations tested. The final choice was a pair of 8-inch p-m speakers, one with a hard cone resonating at 150 cycles and the other soft for a 75-cycle resonance. When these were operated in parallel, their reciprocal damping effects appeared to reduce overall resonance and distortion to a low degree. An 8-watt test signal that produced objectionable distortion in a 25-watt high-fidelity speaker supplied by a prominent manufacturer was easily handled by the 10-watt combination used. The dual system was also chosen because it allowed a more uniform dispersion than could be realized from even a large single speaker.

Conclusions

It was pointed out that the purpose of this project was to design a low-cost, easily-operated organ-like instrument. Low manufacturing cost was accomplished by using inexpensive tone generators whose tiny size lend themselves to small identical subassemblies. Pleasing tone color was the main standard of performance. To this end, comments on the results of listening tests by many musicians and engineers have been most gratifying. Provided reasonable care is exercised in the selection of capacitors and resistors in the parallel-T networks, the instrument should remain in tune indefinitely. Eight organ stops provide 196 combinations of tone color. Any person able to play keyboard instruments can play this instrument with little or no practice.

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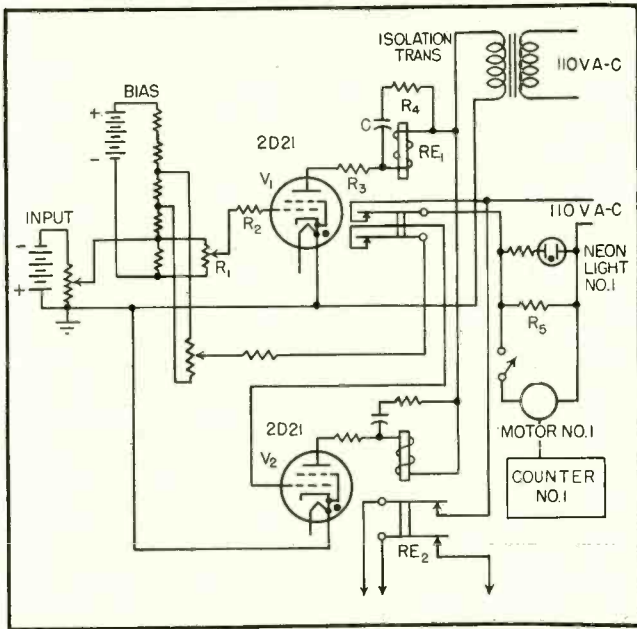
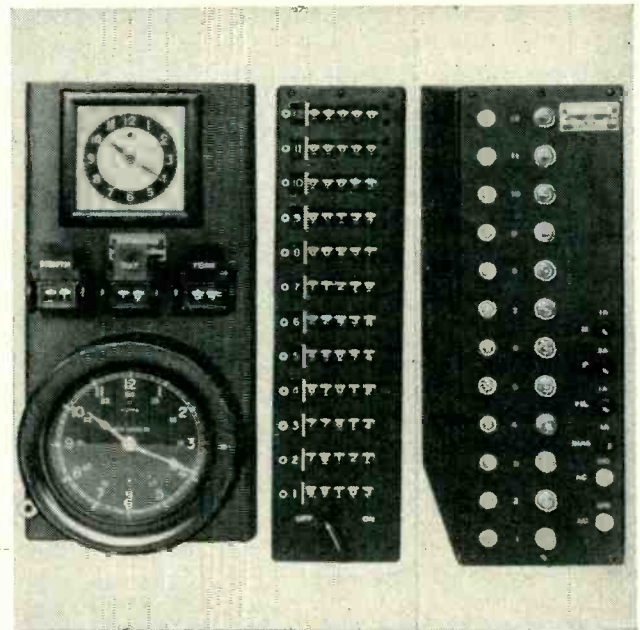


FIG. 1—Simplified schematic diagram of thyatron circuit. Fairly-sensitive, fast-operating standard telephone relays having coil resistances from 2,500 to 14,000 ohms have been used successfully



Mechanical counters (center) show total time signal exceeds each of twelve values as selected and indicated by potentiometers and neon lights in control unit (right). Clock panel is at left

Signal Strength Analyzer

System of thyratrons and mechanical counters automatically totals amount of time that any changing d-c voltage exceeds each of twelve chosen values. Provides greater accuracy at fraction of cost and complication of other methods

CERTAIN RADIO PROPAGATION studies require continuous records of the percent of time a signal is above, or below, selected values over a range of variation. For example, in measuring television signal strength, it is important to know what percentage of time a usable signal can be received in a certain location.

One method for determining this voltage-time information involves the time-consuming process of going over signal strength recorder charts and adding up the time intervals during which the signal exceeds each level step. The automatic method described here accomplishes the same purpose with improved accuracy and with considerable economy, as compared to

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other methods. Other applications for the basic principle involved can probably be made to advantage.

The equipment gives a direct reading of the total time that a fluctuating voltage exceeds each of twelve selected values. The total time for each signal level may be read at any desired time interval.

The analyzer is designed for long-term operation. Calibration drift is inherently small. The equipment consists of two units, a control unit and a minute counter unit, the latter showing the total time in tenths of a minute on a

separate counter for each voltage level. The counter-operating input voltage is determined by the bias on a miniature type thyatron with associated relay in the control unit. A separate permanent-magnet type synchronous motor, chosen for its fast starting and stopping characteristics, drives each counter.

In laboratory tests, average time measurement errors per on-off cycle have been measured as low as 0.01 second using square-wave keying on one circuit. Under more normal operating conditions, as with an input voltage changing at the rate of about 0.5 volt per second, the error may be as large as 0.1 second per on-off cycle. Test runs were made over various periods of time, from 40 minutes to 24 hours

using one on-off cycle per minute.

Input impedance of the control unit is on the order of 1 to 2 megohms, working against ground. When all the thyratrons are cut off, corresponding to maximum input, the input impedance is determined by the overall impedance of the wiring and components to ground. The minimum range of input voltage depends on the use. For signal propagation studies it appears to be on the order of 0 to -15 volts. A larger voltage range will, in general, reduce errors in measurement. Source impedance of the input should be as low as possible and preferably should not exceed 50,000 ohms.

Principle of Operation

The basic functions will be described with reference to the simplified diagram shown in Fig. 1. Thyatron V_1 is the first tube to be cut off as the input voltage is raised above zero. A fixed negative bias of something less than 2 volts is obtained from the bias supply and adjusted by means of potentiometer R_1 so that an input voltage of the desired value (assumed to be less than 1 volt) will cut off V_1 .

This de-energizes RE_1 , which does the following: (1) turns on the synchronous motor driving counter No. 1, (2) turns on the neon light No. 1 to give a visual indication of operation, and (3) connects the input circuit to the grid of V_2 . Tube V_2 has a higher positive bias than V_1 , hence requires a higher input voltage to cut it off. This operating sequence is carried through 12 stages.

The bias system shown permits an independent and wide range of choice of the input voltage required for operation of each stage. The orderly sequence of operation must be preserved. The fixed bias divider may be eliminated by the use of suitable taps on the bias battery.

Only one thyatron in the conducting condition, which is the only condition in which appreciable grid current can flow, is connected to the input circuit at any time. This fact, and grid resistor R_2 , keep the maximum grid current flowing in the input circuit down to less than

one microampere for normal bias adjustments of a few volts difference between adjacent stages. The conducting condition is maintained by leaving the grids floating when the tubes are not connected to the input circuit. Plate resistor R_3 limits the peak plate current to a conservative value. Resistors R_2 and R_3 are also important in suppressing spurious r-f radiation.

The smoothing filter R_4 and C , and the series resistor R_5 , are adjusted to give a minimum differential in grid voltage for on-off operation of the relay.

Stray a-c coupling in the wiring is likely to be sufficient to light the neon light when the counter motor is disconnected and the relay contacts are open. Resistor R_6 serves to reduce this voltage, by virtue of the relatively high impedance of the source, to a value insufficient to break down the neon.

The circuit in Fig. 1 can be modified to operate with substantially the same characteristics for a zero to positive input voltage. In this case, the motor-control contacts should be closed when the relay is energized and the grid to the preceding stage should be opened. With zero input voltage, the grids would all be connected to the input and

biased beyond cutoff.

A d-c amplifier can be used on the input in those applications where the added instability factor of the d-c amplifier can or must be tolerated.

Performance

The usefulness of the system is determined by (1) its stability with time, (2) the difference in input voltage required to open and close the relay contacts, and (3) the error in time measurement of grid controlled intervals.

The average time measurement error of the present equipment has been found to be less than 1/50 second per time interval, or on-off cycle, for time intervals of a few seconds or more. The fast starting and stopping characteristics of the synchronous motor used account for the small error. This motor has a low-inertia rotor, revolving at 100 rpm, which is damped by a permanent magnet in the field. The above time measurement error will not be detected except with square-wave input.

For maximum long-term stability of this system, the plate supply should be regulated. The 2D21 is relatively insensitive to ± 10 per cent change from normal heater

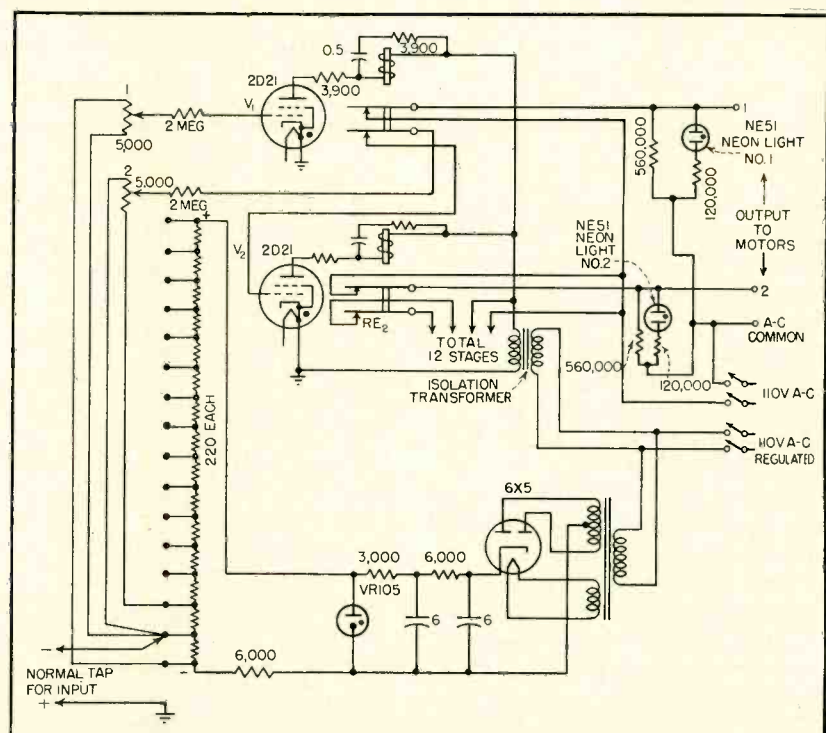


FIG. 2—In the actual equipment, the battery bias supply of Fig. 1 is replaced by an a-c supply as shown

voltage. The tube is operated at conservative values of plate current and should have a long life. The grid operating voltage of the 2D21 is satisfactorily constant over a wide range of ambient temperature. A set of 12 tubes in normal operating service has given satisfactory and trouble-free service during the past year. The bias supply and all resistors must be kept as constant as possible under all conditions.

Sources of Error

The inherent errors in this measuring system can be made relatively small, as will be illustrated in the following example. Assume a calibration error of ± 0.1 volt including operating differential and drift, and a desired maximum error of 0.5 db in a signal recording application. This implies that a change in receiver input of 0.5 db must result in a change of not less than 0.2 volt in the receiver output.

To cover a wide range of signal fading, the receiver output should be a logarithmic function of the input, in which case the output change will be 0.4 volt per db change of input. If the system is calibrated in 6-db steps, starting at 6 db above $1\mu\text{V}$ per meter for instance, the 12 steps in the analyzer will accommodate a range of 72 db and require a maximum input voltage of 28.8 volts. In such practice, it is desired to operate the lowest-level stage as low as possible if very deep fading is to be encountered.

The calibration error assumed in the above example is conservative and may be much lower under favorable conditions. During a 7-day test the input voltage required to operate the relay, including the operating differential, was constant to within ± 0.06 volt. The line voltage was not regulated and varied between 107.5 volts and 110 volts.

Less than 5 percent of over 100 type 2D21 tubes tested were found to have an appreciable change in operating grid voltage depending on the time the tube was previously in the conducting or nonconducting condition. A half-minute in each condition before checking the on-off operating grid voltage has been sufficient to show this fault.

Hum pickup in the grid circuit of the 2D21 thyratron must be kept at

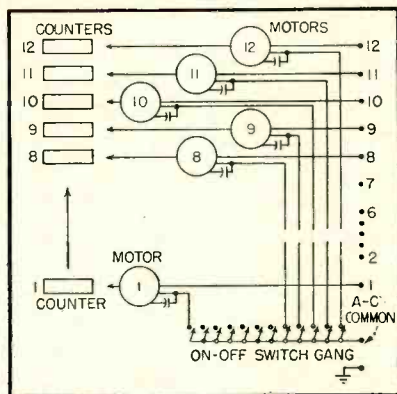


FIG. 3—Separate on-off motor switches are used to eliminate common a-c coupling through motors which would cause all neon lights to light when any motor control relay is closed

a minimum for optimum operation. This requires some care in the arrangement of the input circuit and wiring. The relay should also be so arranged that a separate stack of contacts is used exclusively for switching the grid into the input circuit.

Control Unit

The circuit diagram of the control unit, Fig. 2, is essentially an expansion of Fig. 1 to include the necessary switches, power transformers and an a-c operated bias supply to replace the bias battery used in the simplified version.

A floating, a-c operated, regulated bias supply is used. This supply introduces some hum in the input circuit. The source of this hum is of fairly high impedance and therefore has more serious effects when a high-impedance signal input source is used.

In some cases the hum has been reduced by introducing a compensating voltage to ground from one of the transformer windings not connected to the bias circuit. The electrostatic shield was found to be useless in these transformers. The choice of the a-c plug polarity influences the hum and therefore has an effect on the relay operation and operating differential. An average operating differential not exceeding 0.1 volt was obtained with a 50,000-ohm input signal source.

Tube noise in a signal recording application may give an annoying variation in the signal input operating voltage and operating differential. This is particularly troublesome with weak signals and high

receiver gain. A partial remedy may be had in the use of a low-pass filter in the diode output of the receiver. In this case the resulting slower response of the analyzer must be taken into consideration.

Counter Unit

The counter unit is usually turned off when making calibration adjustments on the control unit. Each motor in the counter unit (Fig. 3) must be disconnected separately to eliminate a common a-c coupling through the motors, which would cause all neon lights to be lighted when any motor-control relay contact is closed.

With five wheels, each counter will register a total of 9,999.9 minutes, or about 166 hours. Zero can be reset manually if desired.

Each counter is driven by its respective motor through a gear system giving a speed reduction of 100 to 1, so the right-hand counter wheel rotates at 1 rpm and reads direct to 1/10 minute. The numbers on the counter wheels are about $\frac{1}{4}$ inch high. The loads on the motors are so light that they are capable of starting and running backwards if there is a slight chatter in the closing of the relay contacts. This was avoided by means of a simple ratchet stop engaging 4 teeth cut in the hub of the worm mounted on the motor shaft. Thus, if started in reverse, the motor is stopped in not more than $\frac{1}{4}$ revolution at which point it starts in the forward direction. The maximum resulting error, which will occur rarely, will be about $\frac{1}{2}$ revolution or 0.3-second time lost.

The compact arrangement of the counter unit permits as many as 3 counter units, and a panel containing reference time clocks, to be set side by side so that a photographic record of three measuring systems can be made with one camera. Signal-strength recording systems in use at present employ a 16-mm movie camera with an exposure rate of 1 frame every hour. A synchronous, motor-driven timer turns on flood lights a few seconds before operating the camera shutter. A 7-day clock and a 60-cycle line-controlled clock are used so that errors due to power failures will be apparent.

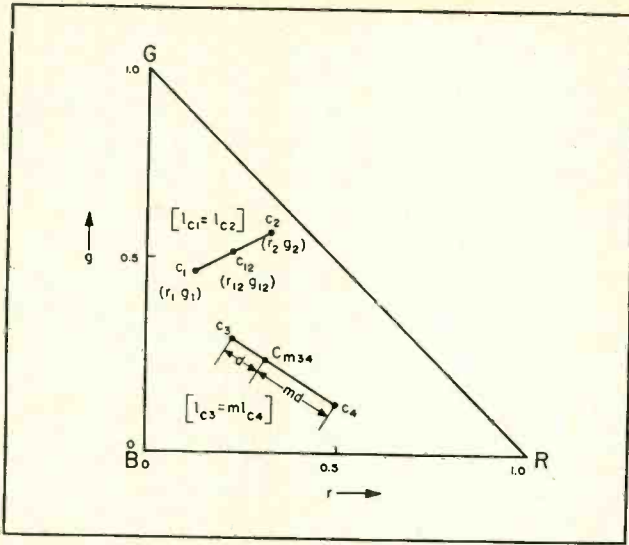


FIG. 10—Color mixture properties of the RGB chromaticity diagram. When two colors are combined, the point representing the mixture color lies on the line connecting the points representing the two combined colors

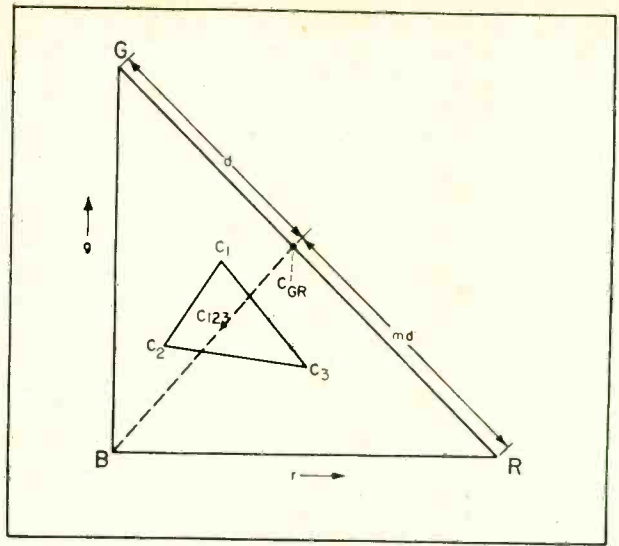


FIG. 11—Color mixture when three colors are combined. If the colors are present in equal amount, the mixture color falls on the center of gravity of the triangle. Dashed line represents finding mixture of primaries to match a given color

COLOR FUNDAMENTALS

In this second installment, the color mixture properties of the RGB chromaticity diagram and its transformation to the XYZ form are described. The spectral locus is identified, and the color gamut covered by three primaries is investigated. Specification by dominant wavelength is defined

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DERIVATION of the RGB chromaticity diagram in terms of colorimeter measurements was outlined in the previous installment. This diagram represents the hue and saturation of all colors that can be matched by combinations of the selected primary colors R, G, and B.

Mixture Colors on the RGB Diagram

The RGB chromaticity diagram, in addition to providing an array of points whose coordinates represent

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the hue and saturation of every color capable of being matched by the selected primaries, constitutes a highly useful basis for computing the hue and saturation of mixture colors arising from the additive mixture of any number of other colors.

To show the method of combining colors, consider two colors, c_1 having coefficients r_1, g_1 and c_2 described by r_2, g_2 (Fig. 10). When these two colors are added, in equal amount, ($l_{c1} = l_{c2}$) and the resultant mixture color c_{12} is matched against the selected primaries in a colorimeter, as described in Part I, it is found that the coefficients of

the mixture color are

$$r_{12} = \frac{r_1 + r_2}{2} \quad (5)$$

and

$$g_{12} = \frac{g_1 + g_2}{2} \quad (6)$$

As shown in the diagram, the point representing the mixture color c_{12} is located at the center of the line joining c_1 and c_2 .

Similarly if colors c_3 and c_4 are mixed in unequal proportion, such that the flux l_{c3} is m times the flux l_{c4} , the mixture color c_{m34} lies on the line joining c_3 and c_4 , but the distance from c_4 to c_{m34} will be m times the distance from c_3 to c_{m34} shown in Fig. 10.

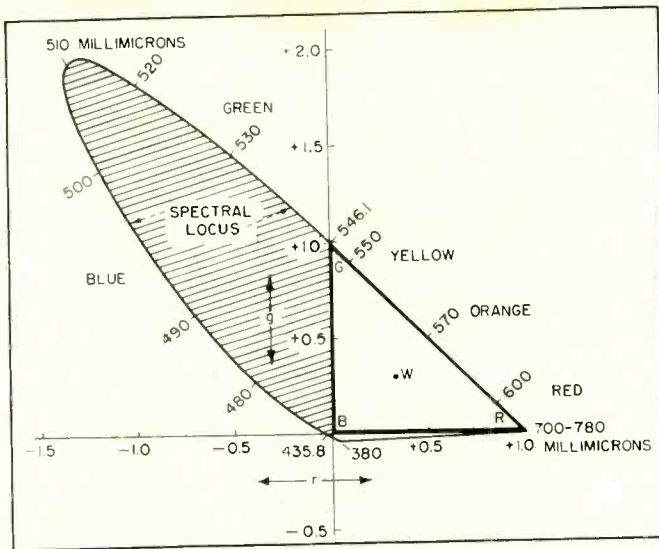


FIG. 12—The spectral locus, shown on the RGB diagram, represents the color coordinates of each color in the spectrum. Numbers on locus indicate corresponding wavelengths

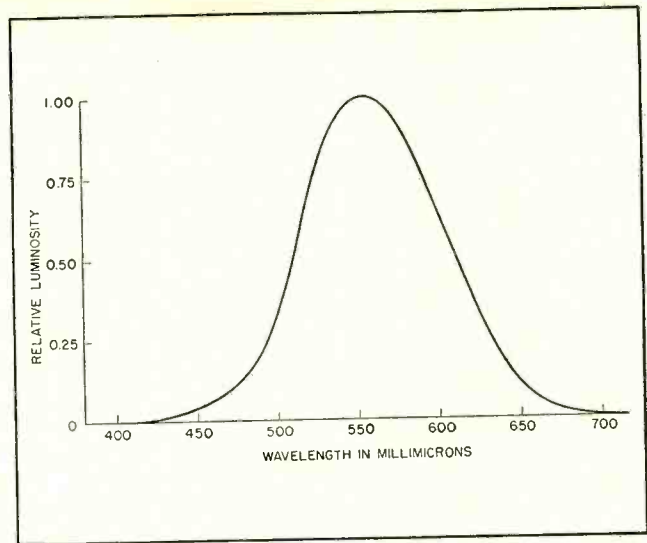


FIG. 13—Relative luminosity of the spectrum colors, as defined by the I.C.I. standard observer. This curve can be used to compute the relative luminosity of different primary colors

for TV Engineers

PART II of a series

When three or more colors are combined, they may be taken in pairs, each pair in the manner of c_1 and c_2 , above. The mixture color c_{12} of this pair is then combined in the same manner with c_3 to find a third mixture color c_{123} , and so on until all the colors are combined. The same point is ultimately reached, regardless of the order in which the colors are combined.

Figure 11 shows a typical example involving three colors in a mixture. The mixture color c_{123} lies at the center of gravity of the triangle formed by c_1 , c_2 and c_3 when all are present in equal amount. When the component colors are present in unequal amount, the mixture-color point lies within the triangle, but the color point is displaced toward the predominant color point or points.

The process of combining primary colors to find the resultant mixture color can, of course, be reversed, so as to find a combination of primary colors which will match a given color. In this case, there is an infinite number of possibilities depending on the relative amounts of the primaries taken. A typical

case is shown in Fig. 11. In this case, a line (shown dashed) connecting one primary and the color to be matched is extended until it strikes the opposite side of the triangle RGB. The point of intersection with this side represents a mixture color of the remaining two primaries. The inverse ratio of distances from the intersection point to the apexes gives the relative amount of each of these primaries required to complete the match.

The Spectral Locus on the RGB Diagram

The RGB diagram described has been set up using the I.C.I. standard primaries*, which are spectral colors. Other spectral colors can be located on the diagram, and the line passing through all the spectral points is known as the *spectral locus*. Figure 12 shows this locus, with the wavelengths of the various spectral hues marked on it. It will

* A similar diagram can be based on any three primaries, spectral or otherwise, saturated or desaturated, provided only that each primary cannot be matched by a combination of the other two. If one can be matched by the others, the triangle degenerates into a straight line.

be noted that the left-hand portion of the figure (shown shaded) lies outside the triangle RGB. This means that the corresponding spectral hues (the saturated blues and greens) cannot be matched by combining the three selected spectral primaries. Rather, these spectral colors can be formed only in desaturated form by combinations represented by points within the triangle RGB. This limitation of matching with primary colors is not a serious matter, because highly saturated green and blue colors represented at the left of the line BG seldom need to be reproduced with high accuracy.

The procedure for finding a point on the spectral locus is as follows: Consider the spectral light of wavelength 500 millimicrons.

To find the corresponding quantities r , g , b in Eq. 1-3, Part I, we must perform two color matches, one between the primaries and the equal-energy standard white, and the other between the primaries and the 500-millimicron spectral hue, the amount of flux l_w of the white light being equal to the flux l_c of the spectral hue.

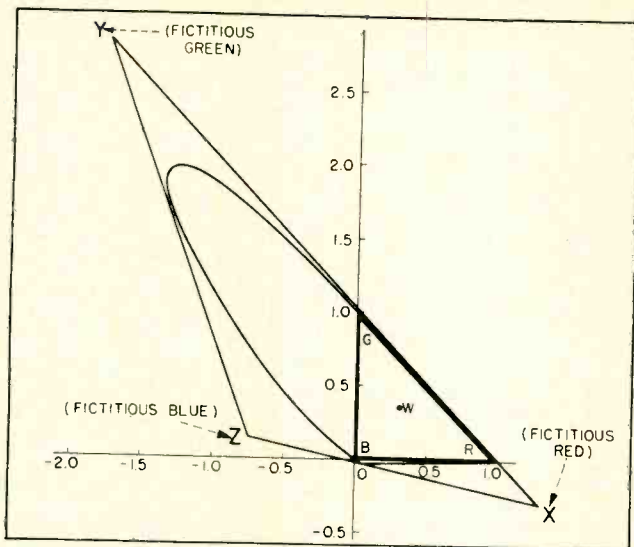


FIG. 14—To transform RGB diagram, triangle XYZ is circumscribed about spectral locus as closely as possible (compare with Fig. 12). Locations of points X, Y and Z are chosen to simplify calculations

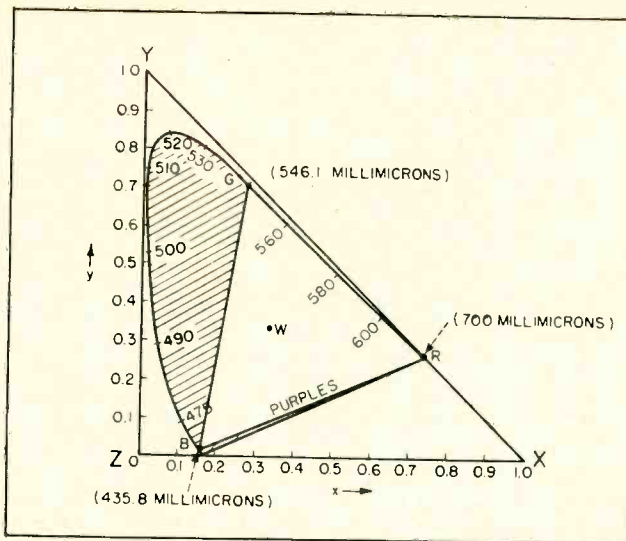


FIG. 15—By use of three linear equations, diagram in Fig. 14 is transformed to XYZ diagram, shown here, thereby eliminating negative values of quantity r . Triangle RGB assumes new shape, but retains color mixture properties of Fig. 10 and 11

The first step is to convert from the power units to light units, that is, to convert from watts to lumens. This conversion is performed with the aid of the "relative luminosity curve", shown in Fig. 13, which gives the response of the normal eye (that of the I.C.I. standard observer) to a given amount of energy of each wavelength in spectrum. The area under this curve is proportional to the number of lumens (l_w) produced by a given number of watts of the equal-energy standard white light.

From the same curve we can find the relative luminosities of the standard I.C.I. primaries; these are in the ratio red: green: blue = 1.0:4.6:0.06. Finally, from Fig. 8 (Part I), we can find the relative amounts of the standard primaries required to match the 500-millimicron spectral hue. These are in the ratio red: green: blue = -17:0.40:0.17. Taking the luminosities in corresponding pairs to form the ratios l_{rc}/l_{rw} , l_{gc}/l_{gw} , and l_{bc}/l_{bw} in Eq. 1-3, we can find the values of r and g from these equations and thus plot the point for the 500-millimicron spectral hue. The negative amount of red light required in the match places the point to the left of the line BG , that is, r has a negative value.

The RGB diagram, with the spectral locus, can be used as the basis of color specification, were it not

for the fact that the saturated blues and greens lying between the spectral locus and the triangle involve negative values of the quantity r . If the negative sign is inadvertently omitted in the specification or computation of a color, the color point has the wrong position. To avoid such confusion, and to simplify color and luminosity computations, the RGB diagram is placed on a new set of coordinate axes, x , y and z , such that no negative values appear.

The XYZ Chromaticity Diagram

The transformation from the RGB form to the XYZ form of the chromaticity diagram is illustrated in Fig. 14. The triangle RGB is enclosed by a larger oblique triangle XYZ which fits the spectral locus as closely as possible. The size and position of XYZ are not chosen arbitrarily. The triangle is arranged to enclose all physically-realizable colors, and its shape is such as to simplify computations.

The diagram shown in Fig. 14 is transformed by three linear equations designed to produce, on the x - y coordinates, an oblique projection of RGB, such that the triangle XYZ becomes a right isosceles triangle, with point X at $x = 1$, $y = 0$, point Y at $y = 1$, $x = 0$, and point Z at $y = x = 0$. The transformed diagram is shown in Fig.

15. The transformation is so arranged that point W, representing equal-energy white light, appears at the center of gravity of the figure XYZ. We note that there are no negative values in the XYZ diagram, that no value of x or y exceeds unity. The transformation is arranged, moreover, so that $x + y + z = 1$.

The XYZ diagram is the internationally accepted representation of chromaticity values. The hue and saturation exhibited by any light source or colored object, illuminated by a particular light source, can be specified by the quantities x and y , which are known as the "trichromatic coefficients" of the specified color. These two coefficients, plus a statement of the brightness, give the complete specification of the color in physical terms.

The transformation from the RGB diagram to the XYZ diagram is a mathematical operation, without physical significance, designed to avoid negative values and to simplify certain calculations. Nevertheless, the XYZ diagram can be given a physical interpretation which serves to fix in mind certain of its properties. In this interpretation, the apex points X, Y and Z are thought of as representing the color coordinates of three *fictitious* primary colors, just as the points R, G, and B in Fig. 14 represent

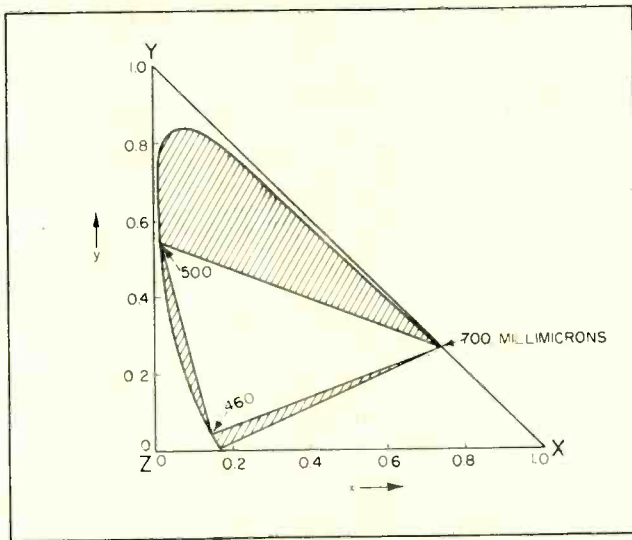


FIG. 16—If another set of primaries is chosen (spectral colors of 460, 500 and 700 millimicrons as shown), saturated blues can be matched but oranges, yellows and greens, in upper shaded area, cannot be matched

three actual primaries (the spectral colors of wavelengths 700, 546.1 and 435.8 millimicrons).

Following out this analogy, the X, Y and Z fictitious primaries are such that if they were physically realizable, and were used in a colorimeter to match the equal-energy white light and the unknown color, the amounts of these primaries needed to achieve the match in each case could be inserted in Eq. 1-3 and the quantities x , y and z computed directly from these equations.

On this basis, the equal-energy white point should fall, as it does, at the point $x = 0.333$, $y = 0.333$. The line YX represents the locus of all colors which can be matched by combining the X and Y fictitious primaries. None of these colors are real, since the spectral locus falls inside line YX.

We note that all the color-mixture properties of the RGB diagram are possessed by the XYZ diagram. The real colors are those enclosed by the spectral locus. Since this locus is not a closed figure, it is necessary to specify the limit of real colors in the open region. It might be expected that a straight line, joining the red and blue ends of the locus, would represent the limit of all the physically-producible colors in the purple region. Experiment verifies this.

The I.C.I. spectral primaries, located as shown on the spectral

locus, form the triangle RGB. This triangle covers only about two thirds of the area enclosed by the spectral locus. Colors represented by points outside this triangle (in the shaded area, Fig. 15) cannot be matched by additive combinations of the standard spectral primaries. These include the saturated greens and blues previously mentioned.

If another set of primaries had been chosen, say spectral hues of wavelengths 700, 500 and 460 millimicrons (Fig. 16), many of the saturated blues could be very closely matched, but the triangle formed by these primaries would not enclose the important region of saturated oranges, yellows and reds. For purposes of color reproduction, it is more essential to reproduce saturated reds, oranges and yellows than saturated blues and greens, since the latter colors occur less often in nature. Accordingly the I.C.I. spectral primaries are a better choice. The filters and phosphors used in color television receivers are chosen to be as close approximations to these I.C.I. spectral primaries as is feasible.

Following further the analogy of X, Y and Z as fictitious primaries, we can specify these primaries by a set of color-mixture curves having the same significance as the mixture curves for the real primaries shown in Fig. 8, Part I. The corresponding curves for X, Y and

Z are shown in Fig. 17. These curves completely describe the primaries, and correspond to the choice of the particular points X, Y and Z in Fig. 14. Since the shape of the triangle XYZ is subject only to the condition that it enclose the spectral locus rather closely, the corresponding color mixture curves (known as "distribution coefficients" and designated as \bar{x} , \bar{y} and \bar{z}) can be chosen in a correspondingly arbitrary manner, to meet the purposes of the RGB-XYZ transformation.

We note that the curves in Fig. 17 are generally similar to those in Fig. 8, with the following exceptions: First, there are no negative values of \bar{x} , \bar{y} or \bar{z} ; on this account no negative values of x , y or z occur. Secondly, the area under each curve is chosen to be the same; thus equal amounts of the primaries X, Y and Z are required to match the equal-energy white, for which $x = y = z = 0.333$.

Finally, the shape and ordinate scale of the \bar{y} curve are chosen to be identical to the relative luminosity curve, Fig. 13. Actually these two curves have quite different significance: \bar{y} represents the amount of a green (fictitious) primary color required to match each spectral hue in combination with two other fictitious primaries, whereas the luminosity curve represents the relative luminous effect on the eye of each spectral hue. If these two curves are identical, however, a single computation serves to produce two results, namely the value of the tristimulus coefficient Y (see Eq. 8) of a particular colored light, and the luminosity L of that light.

Thus the three curves in Fig. 17, with the spectral radiation curve of a particular colored light source, serve to make available the complete description of the color in numerical terms, namely values of x and y which specify the hue and saturation, and the value L which specifies the luminosity (brightness) of the color.

To illustrate the manner in which these computations are carried out, consider the color described by Fig. 18A. This is a spectroradiometric curve of a particular color, obtained by measuring (with a bolometer or

other radiation-measuring device), the number of watts radiated by the source at each wavelength λ in the visible spectrum. This curve is plotted with its maximum ordinate as W watts. To obtain the trichromatic coefficients of this color we proceed as follows: First we divide the $w(\lambda)$ curve by W , thus producing a maximum ordinate of unity. Next we multiply the $w(\lambda)/W$ curve by the \bar{x} curve. The area under the product curve, designated as the "tristimulus coefficient" X , represents the ratio l_{rc}/l_{rw} in Eq. 1-3, except that the color match between the color $w(\lambda)$ and the equal-energy white is now understood to be performed with the fictitious primaries X, Y and Z. Similarly, by taking the area under the product of the $w(\lambda)/W$ curve (maximum ordinate unity) with the \bar{y} curve, we find the tristimulus coefficient Y (having the significance l_{rc}/l_{rw}), and a similar process involving the \bar{z} curve gives the tristimulus coefficient Z (having the significance l_{bc}/l_{bw}).

Stated symbolically, the tristimulus coefficients are:

$$X = \frac{1}{W} \int_0^{\infty} w(\lambda) \bar{x}(\lambda) d\lambda \quad (7)$$

$$Y = \frac{1}{W} \int_0^{\infty} w(\lambda) \bar{y}(\lambda) d\lambda \quad (8)$$

$$Z = \frac{1}{W} \int_0^{\infty} w(\lambda) \bar{z}(\lambda) d\lambda \quad (9)$$

By analogy with Eq. 1-3, the

trichromatic coefficients x , y and z are then given by

$$x = \frac{X}{X + Y + Z} \quad (10)$$

$$y = \frac{Y}{X + Y + Z} \quad (11)$$

$$z = \frac{Z}{X + Y + Z} \quad (12)$$

From these equations we note that $x + y + z = 1$, and that the maximum value of x , y and z is unity, as previously stated.

The luminosity of the color $w(\lambda)$ is given by Eq. 8, since the \bar{y} curve is identical to the relative luminosity curve of the eye. Since the factor converting lumens to watts at the peak of the latter curve is 650 lumens per watt, the luminosity is expressed directly in lumens as

$$L = 650 W Y \text{ lumens} \quad (13)$$

The integrals in Eq. 7-9 are indicated as covering the whole wavelength range from zero to infinity. Actually, since the \bar{x} , \bar{y} and \bar{z} curves are zero outside the visible range from 380-780 millimicrons, the integration need not be carried outside these limits.

Specification by Dominant Wavelength

The values of x and y specifying the hue and saturation of a particular color, while of great value in technical specification, have the disadvantage that they offer no direct clue to the spectral hue which most

nearly describes the color represented. Thus a color described by the wavelength 550 millimicrons is more clearly recognizable than the same color described as $x = 0.3$, $y = 0.7$. To avoid this difficulty, an alternative specification of a color can be taken directly from the chromaticity diagram.

This specification is in terms of the *dominant wavelength* (or dominant hue), the *purity*, and the *luminosity* of the color. To find the dominant hue and purity of a color, we pass a line through the point C representing the color and the point W representing the equal-energy white light and extend this line until it intersects the spectral locus, as shown in Fig. 19. The wavelength corresponding to the point of intersection is defined as the dominant wavelength of the color, and the corresponding spectral hue is the dominant hue.

The purity p is a measure of the saturation of the color, that is, of the distance from its point to the white point, and is given by

$$p = 1 - 0.333 \left(\frac{1 - y_s/y_c}{0.333 - y_s} \right) \quad (14)$$

where y_c is the y -coordinate of the color and y_s is the y -coordinate of the intersection with the spectral locus. The purity ranges from 0 to 1. For example, color point C in Fig. 19 has a dominant wavelength of 560 millimicrons and a purity of 0.69.

From Eq. 14, colors near the

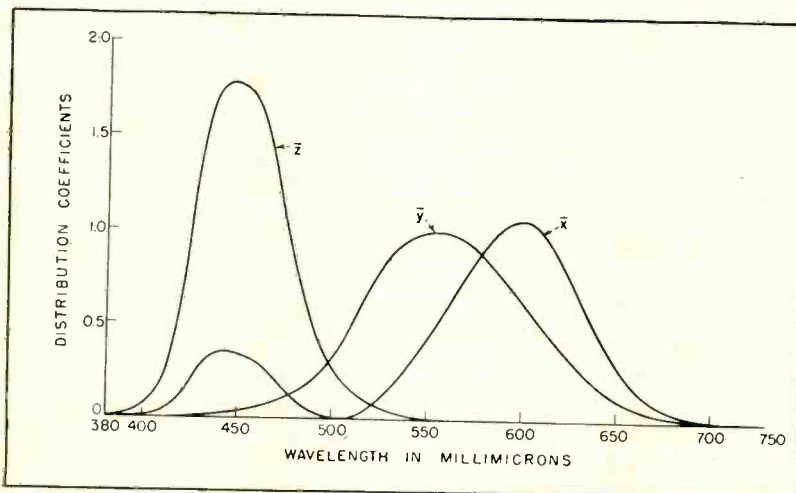


FIG. 17—Color mixture data ("distribution coefficients") for the fictitious primaries X, Y and Z. These have the same significance as the color mixture data for the real primaries R, G and B, shown in Fig. 8, Part I

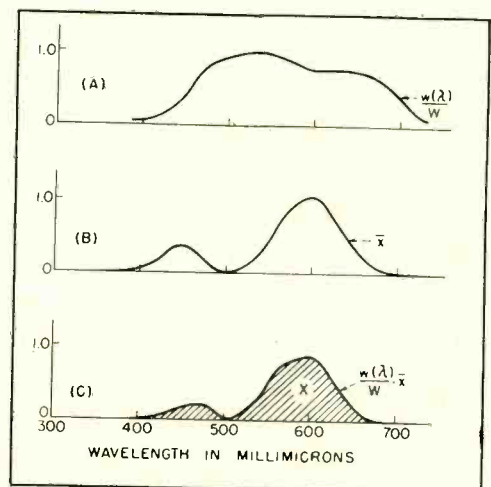


FIG. 18—Method of combining spectral radiation curve of light source with distribution coefficient to find tristimulus coefficient X

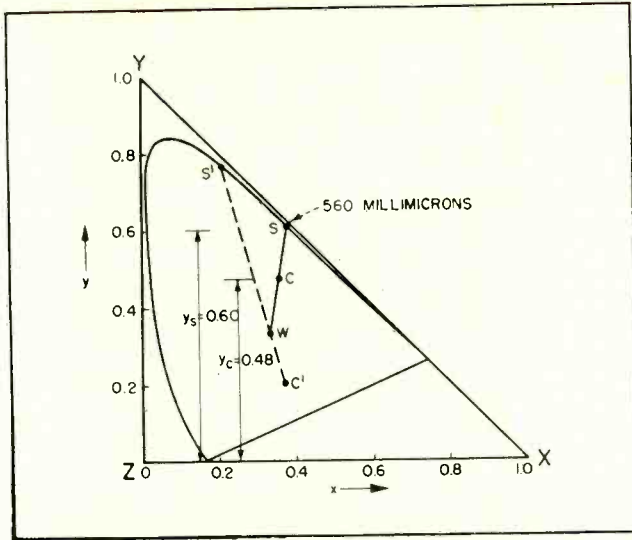


FIG. 19—Specification of color by dominant wavelength and purity. Line, passed through white point and color point to be specified, is extended to locus. Wavelength of intersection is dominant wavelength

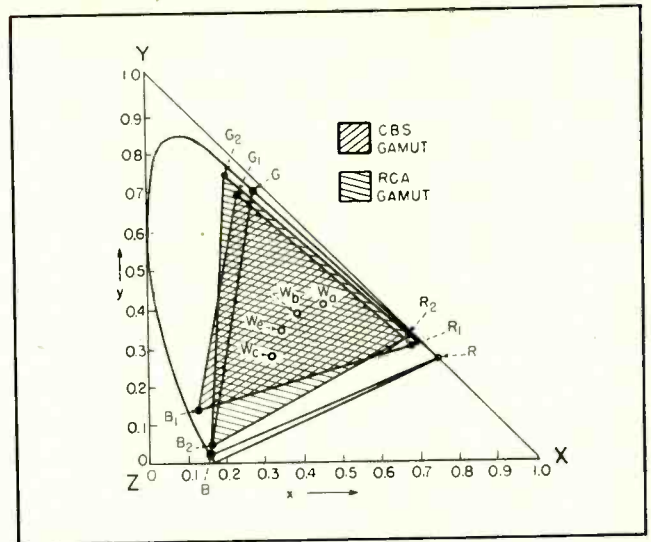


Fig. 21—Color gamuts of the CBS and RCA color television systems, as proposed to the FCC during the recent hearing, compared with the range covered by the standard spectral primaries

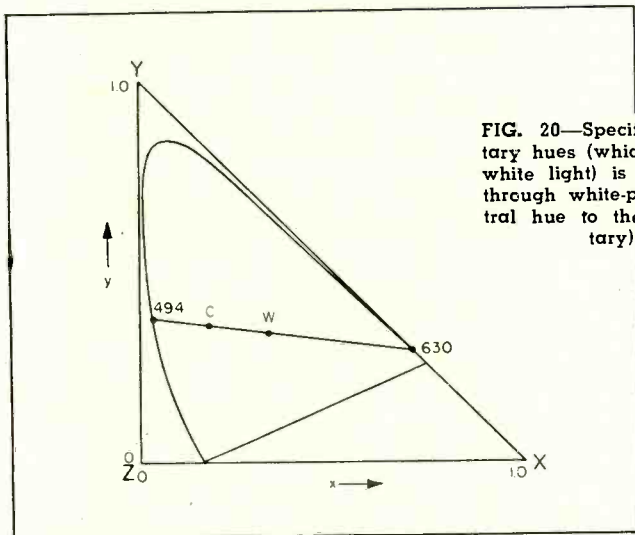


FIG. 20—Specification of complementary hues (which when mixed produce white light) is found by passing line through white-point W from one spectral hue to the opposite (complementary) spectral hue

spectral locus (y_c nearly equal y_s) have a purity near one, whereas colors near the white point (y_c near 0.333) have a purity near zero. The purity is, in other words, a direct measure of saturation.

This system of specification falls down when the color is one of the purples, that is, when its point falls below the white point in such a position that the extended line does not pass through the spectral locus, as point C' in Fig. 19. In such cases the line is extended in the opposite direction, as shown, intersecting the spectral locus at a wavelength representative of the dominant hue complementary to that of the given color.

Complementary colors are not a very satisfactory specification, since the indication of subjective sensation is lost. The purity of such purple colors is computed by Eq. 14, taking y_c as the y -coordinate of the complementary dominant hue. To distinguish the color so indicated from color having the same actual dominant hue and purity, the purity of purples is stated as a negative number.

The foregoing illustrates the ease with which complementary colors (colors which when mixed produce white light) can be identified on the chromaticity diagram. To find a complementary color to a given color C (Fig. 20), we pass a line

through C and W , extending it so as to intersect both sides of the spectral locus (or through the locus above and the saturated purple line below). The dominant hues so indicated are said to be complementary to one another.

With the properties of the x - y chromaticity diagram in mind, we are now in a position to locate certain colors on it and to show the boundary of the colors which can be covered by color-reproduction processes. In Fig 21, the I.C.I. spectral primaries are shown as RGB , and the equal-energy white as point W_s . Three other standardized whites are shown. Point W_a represents the color of average artificial (incandescent) illumination, known as illuminant A. Actually this is the color of an incandescent lamp operated at a color temperature of 2,848° Kelvin. Illuminants B and C (points W_b and W_c) are two forms of daylight, the first being representative of conditions met in the higher latitudes, the second of the middle and the lower latitudes. Also shown in Fig. 21 are the primary colors proposed for color television receivers. The points R_1, G_1, B_1 represent the receiver primaries standardized by FCC for the CBS field-sequential color system. Points R_2, G_2, B_2 mark the primary coordinates proposed to the FCC for the RCA dot-sequential system.

Capacitive Slip Ring

The problem of multiple temperature measurements on aircraft supercharger impellers at speeds greater than 20,000 rpm has been solved with thermistor elements capacitively connected to an r-f bridge. Under optimum conditions it is possible to determine temperatures within ± 0.25 C

THE DETERMINATION of temperatures at selected stations on a high-speed rotor, like that of an aircraft engine supercharger, has been a very difficult problem.

One system that has been used with some success employs thermocouples as electrothermal converters and d-c slip rings as transfer devices to the recording equipment. At speeds greater than 20,000 rpm, however, the brush pressure must be so great to secure a continuous contact that brush life may be only a few minutes. The slip ring often must be refurbished after 15 minutes of operation. Possible thermoelectric action at the slip ring must also be properly understood.

Somewhat better results have been obtained when thermistors replaced the thermocouples. A thermistor is a thermally sensitive but otherwise stable resistor that can have the same physical size as

a thermocouple. Instead of measuring voltage one now measures electrical resistance which is a known function of temperature.

Commercial thermistors in thermocouple size (about 6-mil spheres) can be purchased with resistance-temperature calibration possessing values ranging from about 2,000 ohms to 10^9 ohms at 70 F. Thermistors possess a negative temperature coefficient of ten times that of platinum at ordinary room temperatures, but this decreases as the temperature increases. They have upper temperature limits where their stability is no longer satisfactory.

Much longer brush and d-c slip ring life has been obtained by employing thermistors having resistance of about 15,000 ohms at the operating temperature. Resistance can be measured with a Wheatstone bridge or ohmmeter. If one can measure the resistance of the thermistor within ± 1 percent, then uncertainties of thermistor temperatures may be no greater than ± 0.25 C. Variable contact resistance or contact potential at the slip ring plays a relatively unimportant role when a high resistance level is maintained. Caution must be exercised, however, for too high a resistance level may result in spurious electric pickup when certain types of electronic measuring instruments are employed. To avoid difficulties inherent in mechanical contacts a capacitor type contact can be used.

Of the two types of noncontact coupling available, capacitor coupling seems much simpler than magnetic coupling. Simplicity becomes paramount when one must have a coupling device for each measuring station. A simple and dependable

selector switch capable of positive switching into specified measuring stations by small actuating forces at high speeds would be difficult and expensive to make.

High-frequency measuring techniques make it possible to use a capacitor ring. The thermistor lends itself to a-c as well as d-c excitation as there is no significant skin effect. A General Radio type 516-C r-f bridge may be used to measure the impedance transferred to the stationary reference frame although the newer type 916-A bridge is more advantageous.

A test rig was built simulating the geometry of an actual supercharger impeller. The elementary equivalent electric circuit of this rig is displayed in Fig. 1A. The requirements to be met in the circuit are that the reactance of the stray capacitance in shunt with the thermal resistor be about 10 times the value of that resistor (for a 1 percent unidirectional error at this point), that the rotating capacitor be as high in capacitance as possible and still quite independent of rotation or axial translation, and that the variable impedance between moving ground and stationary ground be reduced to a low value.

Figure 1B illustrates a cylindrical slip ring capacitor whose capacitance is not very sensitive to end play or to eccentricity of rotor member. The axial length of the capacitor is 1.5 inches, with a 4-mil average air gap. The rotor diameter is 1 inch. It is believed that improvement would result if the stator were split into two 135-degree arcs, each adjusted in position by set screws under rotating conditions to secure a minimum gap.

There is an unavoidable parallel

* Formerly at the University of Connecticut.

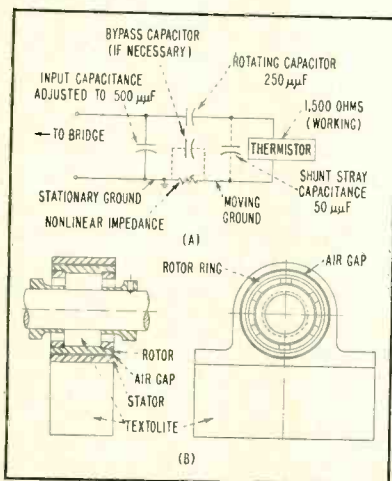


FIG. 1—Thermistor and slip ring connections looking into bridge (A) and mechanical layout of the capacitive slip rings (B)

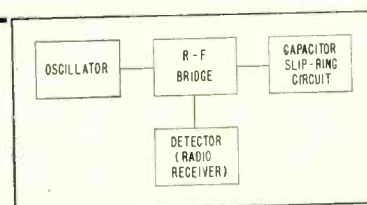
for Instrumentation

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Arrangement of the r-f bridge equipment for thermistor measurements via slip rings

input capacitance at the points where the bridge is connected owing to the physical arrangement of parts. This inherent capacitance may have to be appropriately increased so as to reduce the equivalent resistance that the bridge can accept. In the present case the resistance must be no higher than 111 ohms. The newer type 916-A r-f bridge can accept 1,000 ohms at 1 mc. In the test rig, the input capacitance was maintained at 500 μf . This value must be known and enters into the formula found in the instruction manual supplied by the manufacturer of the bridge. It is clear that the bridge does not directly read the thermistor resistance but the latter may be derived from the bridge dial settings by computation or, better still, by prearranged charts or nomographs including the thermistor calibration.

The shunt stray capacitance is minimized by sufficiently separating a No. 36 Formex wire from the ground plane by laying down some Bakelite insulating cement and then finally cementing the wire. The wire is staked to the capacitor ring at one end and fastened to the thermistor at the other. The free thermistor terminal is grounded. It is desirable to use a low value of thermistor resistance at the working temperature, for example, below 2,000 ohms so the shunt stray capacitive reactance has little effect.

The frequency is a compromise in an attempt to keep the shunt stray reactance high and the rotating-capacitor series reactance low. If there is sufficient instrument sensitivity, lower values of frequency can be used. The oscillator, preferably a crystal type, delivers one

stabilized frequency at 100 mv.

If several rings are to be used, the return path is always through a common ground. If ball bearings are used to support the dummy impeller, a parasitic variable impedance is set up between moving and stationary grounds that inhibits a bridge balance. A satisfactory bypass is effected by placing a large stationary grounded shield close to the moving impeller. In an actual supercharger assembly, such a shield is inherent in the construction.

The 516-C radio-frequency bridge is operated at 500 kc with an associated oscillator. The detector is a suitable radio receiver used to secure an audible minimum in conjunction with a modulated oscillator. A 500-kc unmodulated oscillator is equally satisfactory since the rotating capacitor modulates the carrier so the audio note is an additional indication of frequency. Since a meter indication is superior in noisy areas to an audible note, a wave analyzer that filters stray frequencies may be added to the radio receiver to give a sensitive visual null. In an actual installation such formal equipment as a wave analyzer or commercial crystal oscillator could be replaced by simpler and less expensive electronic equipment.

When the test rig was run up to speeds of 20,000 rpm by an air turbine bridge sensitivities of one part in a thousand were observed over the whole speed range. This is the significant part of the test. Good correlation was observed between thermistor measurements and readings of a stationary standard thermometer arranged close to an axially located rotating thermistor.

A direct measurement of resistance in this case is inherently limited by the calibration error of the bridge and also by the residual parameters. Although the sensitivity of the instrument is about one part in a thousand, a precision greater than ± 3 percent in resistance probably cannot be expected even when balancing out the residual parameters, including residual resistance in the r-f paths.

If the bridge and circuit as a unit is first calibrated over the range (maintaining constant oscillator frequency) by substituting small calibrated resistors for the thermistors, or by making a controlled heat run under stationary conditions with thermistors as well as other temperature sensing elements of known characteristics in place, a ± 1 -percent measurement of resistance and a thermistor temperature within ± 0.25 C should be attainable. Such measurements are best made on an actual impeller assembly free from its enclosing case.

This work was a portion of a general project on instrumentation completed in December 1946 by the authors in collaboration with G. S. Timoshenko and L. E. Williams of the University of Connecticut. The project was sponsored by the Pratt and Whitney Division of the United Aircraft Corporation. R. E. Gorton and E. M. Moffatt of the Corporation served respectively as project coordinator and technical advisor.

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PERMANENT-MAGNET

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WITH THE ELECTRON MICROSCOPE finding new uses in every field of science and in every industry, the need for a simpler and more reliable microscope has been growing rapidly. In order to fill this need, the permanent-magnet type was designed.

The instrument, Fig. 1, requires little technical skill to operate. As a natural consequence of the simplification of design and function, external appearance is both simple and functional.

At a third of the expense and complexity of larger electron microscopes, the permanent-magnet electron microscope solves ninety percent of the problems applicable to electron microscopy.

Electrical System

The source of illumination in the microscope, Fig. 2, is a beam of high-energy electrons. The electrons are released, accelerated and aimed in the gun which is situated at the top of the microscope column. A fifty-kilovolt potential applied between the filament and the anode of the gun gives the electrons enough kinetic energy to pass through the specimens used in electron microscopy.

Fifty kilovolts potential is used because at lower voltages a considerable number of the electrons are stopped by the specimen, which consequently heats up, frequently to its own destruction. Excellent voltage stability is a necessary requirement of the high voltage because the focal length of a magnetic lens such as the one used in the microscope depends upon the energy of the electrons as well as upon the magnitude of the magnetic field. Image defect produced by fluctuating voltage is analogous to chromatic aberration in light optics. In order to achieve a resolution of 100 A with the permanent-magnet electron microscope it is necessary to stabilize the accelerating voltage to one part in ten thousand.

The gun on the microscope is energized by an external and remotely located high-voltage supply which is connected by means of a length of x-ray cable.

The high-voltage unit, Fig. 3, divides into two sections, a control unit, and a rectifier unit. The con-

trol unit is small enough to sit on a table beside the microscope column and provides electrical control at the point most convenient to the operator. The rectifier unit, Fig. 4, houses the high-voltage tripler and the filament oscillator and transformer. It may be placed on

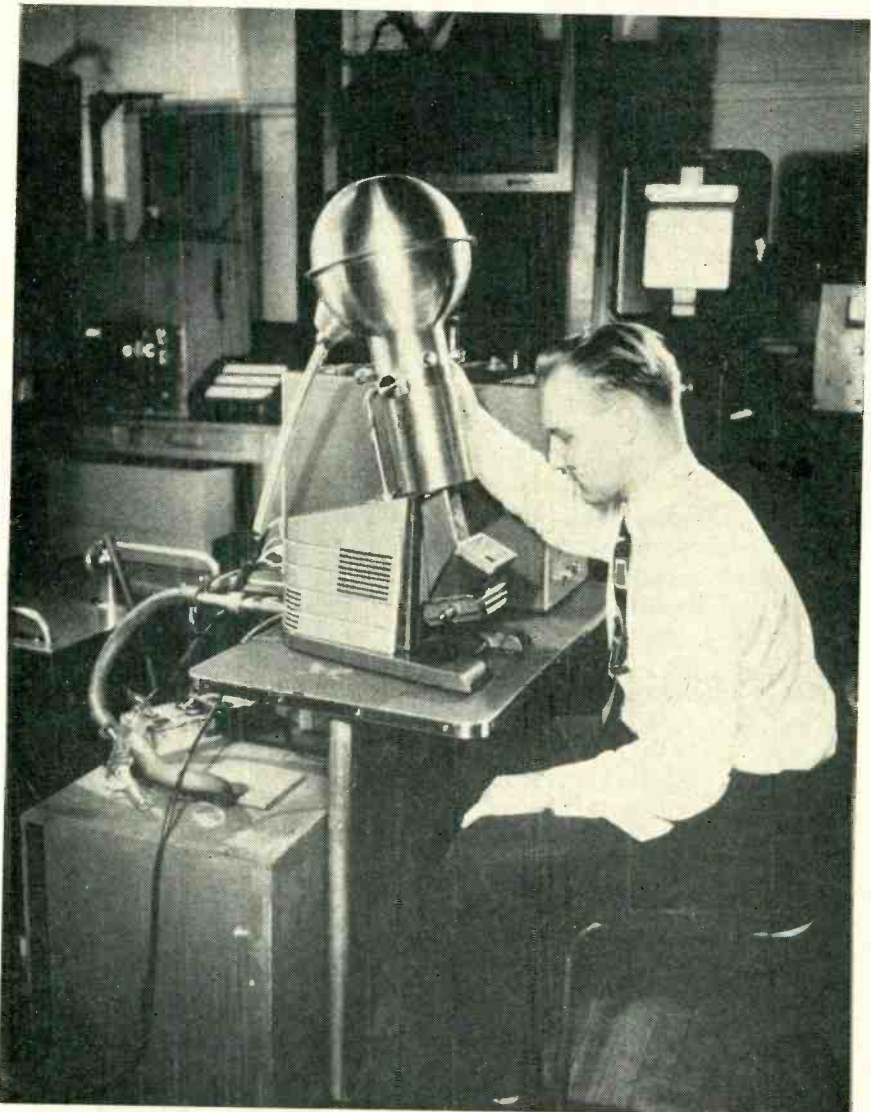


FIG. 1—Permanent-magnet electron microscope in use in a laboratory, control unit in the background on the table and power supply on the floor

ELECTRON MICROSCOPE

Use of Alnico 5 instead of conventional electromagnets to energize the lenses, and other design innovations, provide a handy, economical and comparatively trouble-free instrument suitable for 90 percent of all applications. Specimens are readily manipulated and photographic plates made without extensive pumping-down

the floor or under a table.

Referring to Fig. 3, oscillators V_1 and V_2 produce an 80-kc r-f signal. This signal is applied across the series-resonant high-Q L-C circuit L_1C_1 producing a 17-kilovolt signal across L_1 . On one part of the cycle C_2 is charged through rectifier V_3

then, during the next half cycle, the voltages across C_2 and L_1 are additive and charge capacitors C_3 and C_4 through rectifier V_4 . The signal across L_1 also causes C_5 to charge through rectifier V_5 . The voltage across C_5 , C_3 and C_4 in series is thus triple that across L_1 . The

ripple in the output is filtered through a resonant filter to ground.

Stabilization of output voltages against line and load fluctuations is accomplished by d-c amplifier, V_6 and V_7 , operating series regulators V_8 and V_9 . Resistors R_1 and R_2 provide a bridge element between the d-c and high-voltage output and a reference voltage established by glow tubes. Tube V_{10} calls for full power to the oscillators through the regulators until the negative high voltage produces a negative bias at the junction of R_1 and R_2 , whereupon the d-c amplifier regulates the output voltage by reducing oscillator plate voltage.

Focus of the microscope is accomplished by changing the accelerating voltage, which changes the focal length of the lenses. Potentiometers R_3 (coarse) and R_4 (fine) vary the reference voltage, which causes the voltage-regulating system to readjust itself to a corresponding output voltage. The output is continuously variable from 45 to 50 kilovolts.

Gun Filament Transformer

In order to solve the problem of termination of the high-voltage cable at the rectifier in the minimum amount of space, the high-voltage bushing which connects the x-ray cable to the high-voltage output is also the filament transformer, as shown in Fig. 4. The voltage gradient from the high point of the rectifier unit to its wall is in the direction which the conductors in an output cable must occupy, while the gradient in the cable proper is radial to those wires and therefore perpendicular to the gradient toward the wall. To make the transition in fields without reaching a

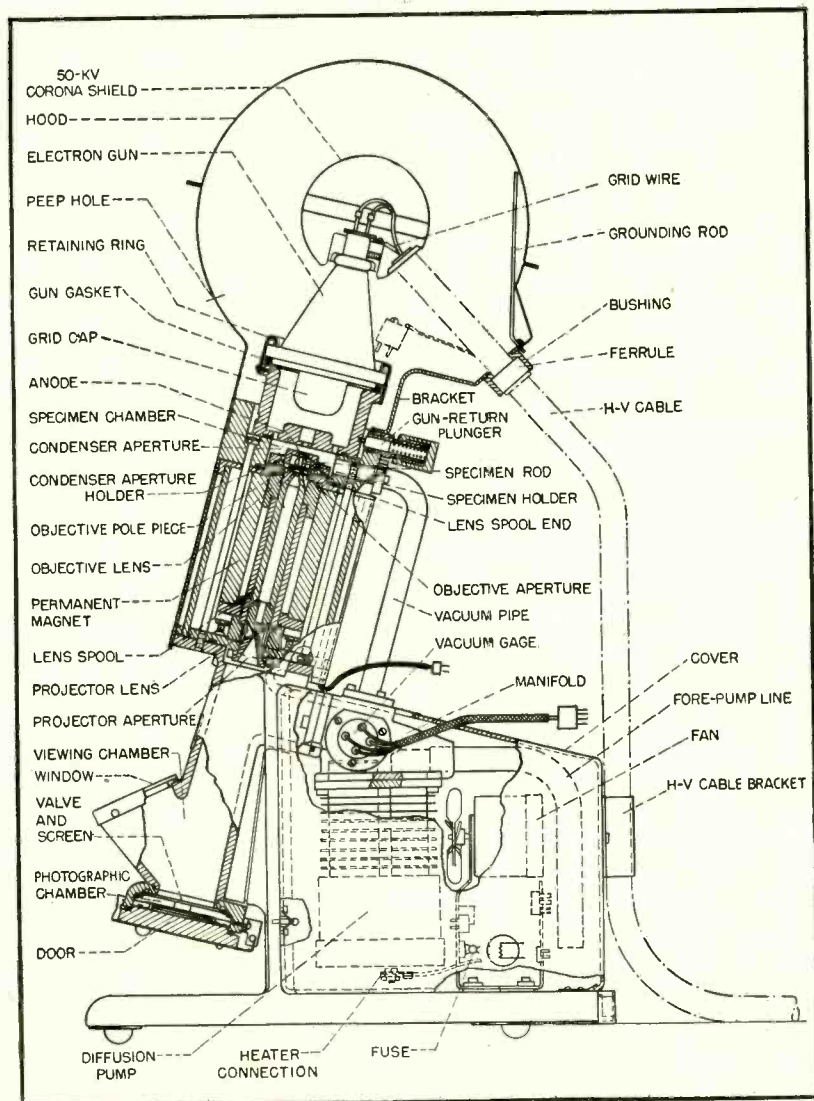


FIG. 2—Cross-sectional drawing of the microscope column, showing the location of component parts

gradient above the corona point an annular corona ring is mounted axially with the outgoing cable and therefore parallel to the field from the wall.

Physical transition to the cable is made through a hard-rubber insulator with the surface cut in the usual manner to increase the leakage path. The inside diameter of the hard-rubber piece is large enough to take the rubber insulation of the x-ray cable. The cable extends into the bushing a distance of six inches to prevent breakdown along the interface of the two insulators.

Inside the bushing extra space is provided for a secondary coil, the means of energizing the filament. The outside surface of the bushing, from the point where it contacts the corona ring to its termination at the metal cable shield, is at ground potential by virtue of an Aquadag surface. This equipotential surface on the rubber prevents corona starting between the rubber and an otherwise necessary ground electrode. It has the additional function of shielding the high-impedance output from the r-f fields inside the cabinet. The primary of the filament transformer, actually the inductive element of a Colpitts oscillator, is wound on the outside

of a laminated Bakelite core, which also serves as a support and alignment bushing for the hard-rubber cable connector. The cable assembly actually includes the hard-rubber connector. Connection to the high-voltage supply is effected by sliding the rubber connector into a hole on the top of the rectifier cabinet.

The filament transformer is energized by a 200-kc oscillator. The relatively high frequency is utilized to improve coupling in the transformer, which contains no iron.

A system of fail-safe circuit-completing interlocks prevents turn-on of high-voltage power unless all components are correctly in place and shielded. When protective hoods are removed grounding rods short out the high voltage before access to the voltage compartments is possible. The power supply is protected during such shorting episodes by its high internal resistance and by overload relays which cut off plate power. All cables carry a ground lead for protection against short-circuit shock.

Vacuum System

The kinetic vacuum system is made up of two pumps in series, an oil-vapor or diffusion pump and a

mechanical fore or rough pump.

In earlier instruments the vacuum pumps were cut off from the microscope column during specimen and plate changes. This necessitates complex valving and pumping systems to protect the diffusion-pump oil from decomposition by the oxygen in the air. Some instruments employed systems of air locks and auxiliary pumps. The permanent-magnet microscope has eliminated much of this valving and pumping complexity by first reducing to a minimum the air admitted with a specimen and plate, and second by utilizing recently developed chemically stable silicone diffusion-pump oil that does not readily decompose.

The total evacuated volume of the instrument is one liter. An oil diffusion pump mounted as shown in Fig. 2, can pump the system to operating vacuum (5×10^{-1} mm) in twenty-five minutes from a cold start. The oil diffusion pump, a thermal device, is air cooled by a small magnetically shielded fan situated with the pump under the rear cover of the instrument. The pumping system will recover from the admission of 0.06 cc of air with a specimen in six seconds, and from the admission of 80 cc of air with a photographic plate in a little over

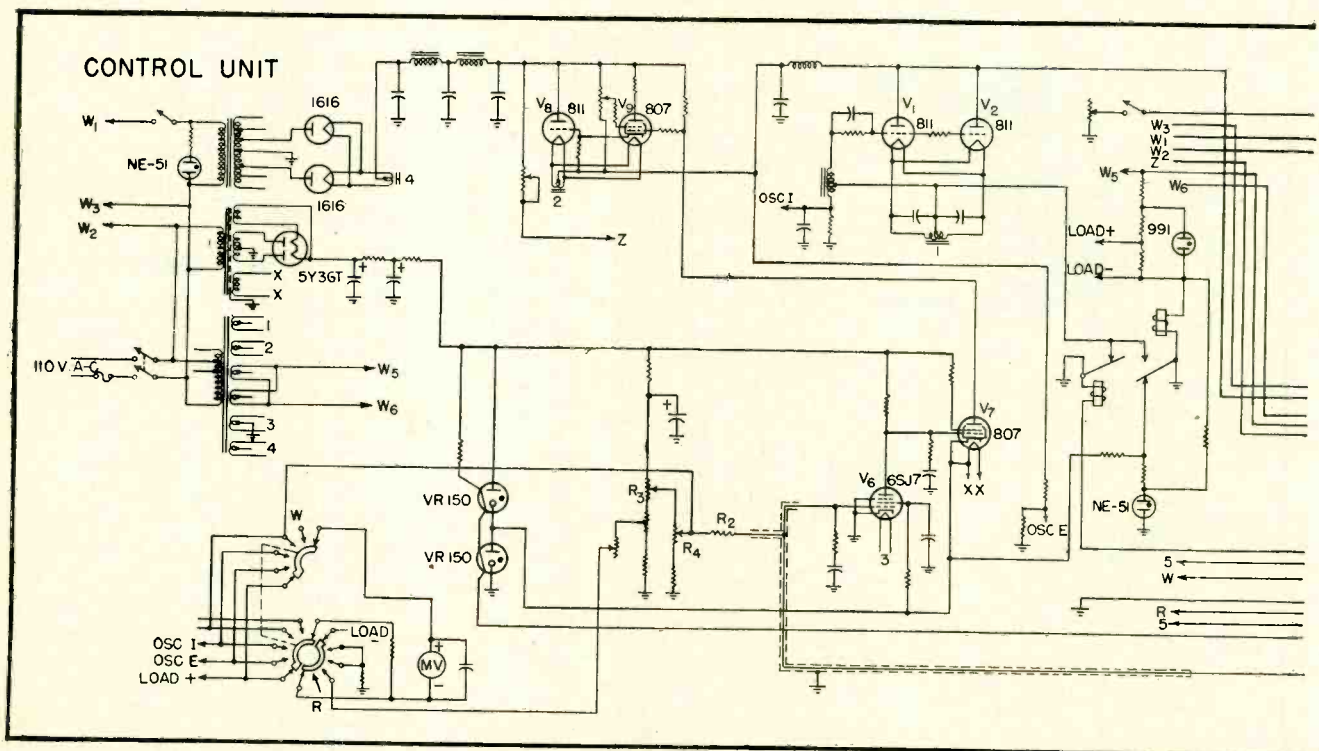


FIG. 3—Simplified schematic circuit diagram of the three-unit permanent-magnet electron microscope. Plugs

a minute. A thermocouple-type of vacuum indicator, attached to the microscope column, reads on the test meter of the high-voltage control unit.

Optical System

The exterior appearance of the microscope column makes the position of the optical elements nearly self-evident. In reverse order to that in the ordinary light microscope, the source of illumination is at the top and the image is formed at the foot of the microscope.

The electron gun is situated under the spherical hood. The hood has been removed in Fig. 5 to show the gun and a grounding rod which shorts out the high-voltage power when the hood is removed. The high-voltage cable is held in place by a bracket at the rear of the gun so that movement of the cable can exert no strain on the gun. The heavy rubber-covered cable enters the spherical corona shell on the gun through a large hole. Inside the corona shell, connection is made to the gun terminals by thin flexible leads which permit the gun to be moved transversely on the instrument without binding in the cable.

Two knobs directly below the gun position the gun transversely with

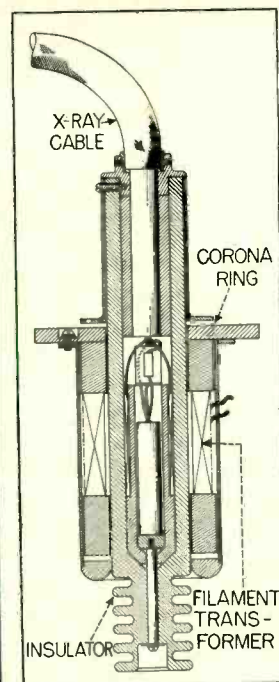
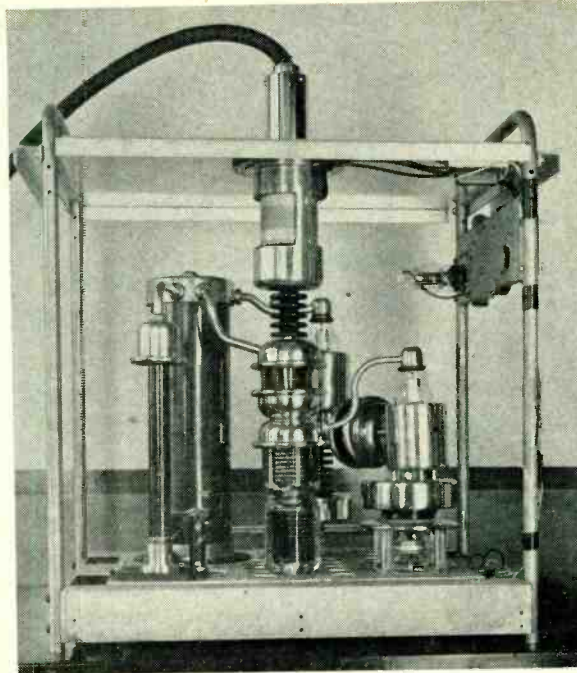


FIG. 4—High-voltage rectifier unit, with case removed, and cross-sectional drawing of the combined output connector and electron-gun filament transformer

respect to the axis of the optical system. By this means some element of the solid cone of illumination out of the gun which is parallel to the optical axis of the instrument may be found and centered over that optical axis.

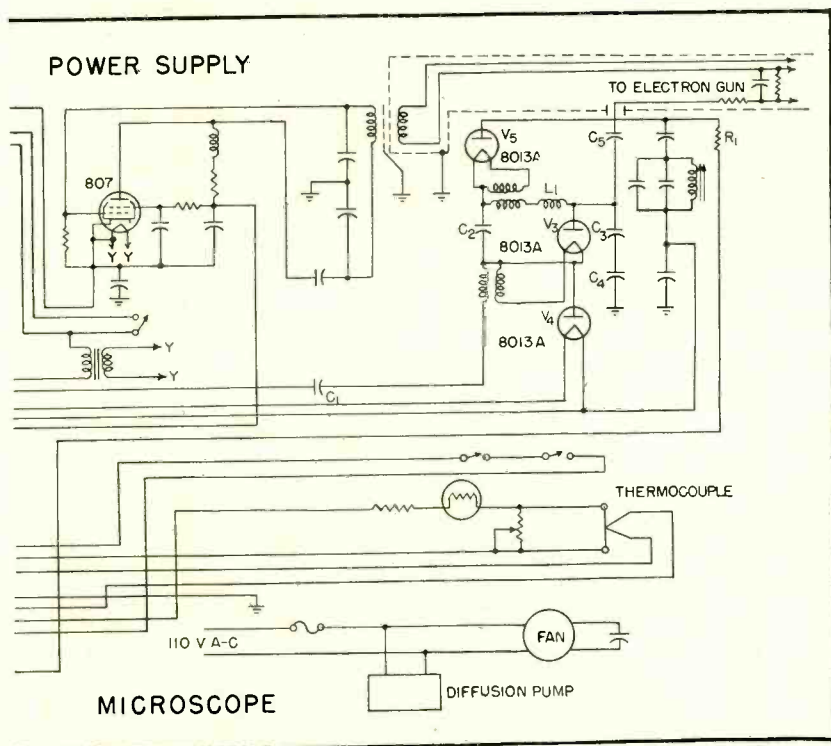
The gun comprises both the cast-glass insulator and the cylindrical

shaped metal element which supports the glass. This metal element is the anode, and is at ground potential. The adjustment screws press against the anode shell to cause the gun to move. The vacuum seal between the glass insulator and the anode is made by means of a neoprene gasket lubricated with stopcock grease. The transverse adjustment of the gun may be made while the beam is turned on since the neoprene gasket between the anode and the upper wall of the object seal provides a good sliding vacuum seal.

The electron beam leaving the gun is so wide and intense that it would destroy a delicate specimen unless restricted by a beam-limiting aperture, frequently called a condenser aperture by analogy to the light microscope. The hole in the thin platinum aperture disc has a diameter of 0.003 inch. Directly below this aperture is the specimen.

Permanent-Magnet Lens

A magnetic lens focuses the electrons passing through the specimen and forms a real magnified image in front of a second magnetic lens which forms a further enlarged image on the viewing screen or photographic plate. The magnetic lens is actually a magnetic field



are omitted from the diagram; several are used where this illustration splits

which is formed by a gap in a magnetic circuit. The field fringing out from such a gap, formed by iron pole pieces, interacts with the electron beam much as a glass light lens does.

The literature on the gaps or pole pieces used in magnetic lenses is extensive so the subject need not be discussed here. Of more interest because of its novelty and importance is the energization of the magnetic lenses by the permanent magnets from which the new electron microscope derives its name.

Permanent magnets are desirable because they eliminate coil windings, cables, power supplies, filters and multitube regulating circuits required with electromagnetic energization of lenses. The resultant advantages are lower cost and comparatively trouble-free service.

It is not generally possible to replace an electromagnetic element directly with a permanent magnet because the circuit is actually altered. In the case of the lens, simple replacement of windings by magnets to energize the lens gap produces stray fields which utterly destroy the microscope image. To use permanent magnets successfully, it is necessary to utilize the otherwise stray external flux to energize an additional gap. By positioning the second gap coaxially with the first



FIG. 5—Microscope column with protective hood removed

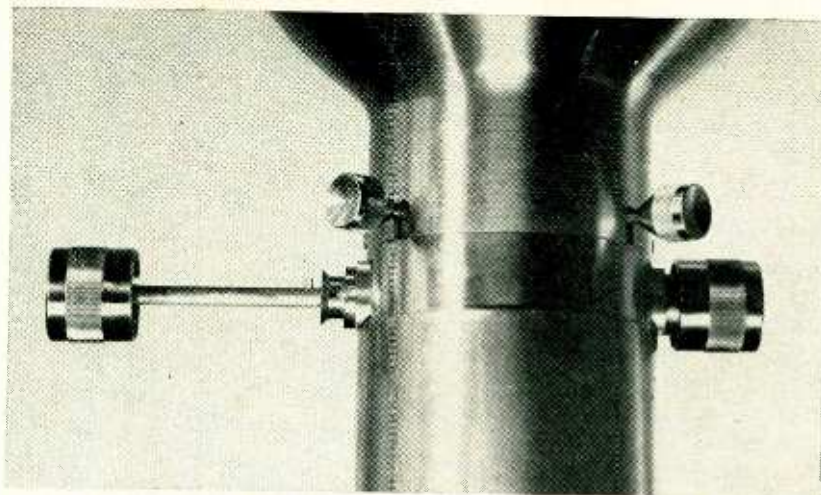


FIG. 6—Specimen-manipulation rod shown withdrawn

gap, two lenses may be energized from a single magnetic source. Most important, the two lens gaps, and all the intervening space, are covered by a surface of sensibly constant magnetic potential, so that destructive stray fields are eliminated. Since two lenses are necessary for high magnification the double-gap magnetic circuit proves to be doubly beneficial.

Alnico 5 is used as the magnet material in a high-demagnetization-coefficient circuit to give strong energization and great stability against demagnetization by removal of pole pieces. The upper or objective gap is energized to 1,300 gilberts and the projector to 900 gilberts.

The use of permanent magnets to energize lenses has the disadvantage of discarding the unique property of variable focal length of magnetic lenses. This property is frequently used to change the magnification of an electron microscope over wide ranges by merely turning a selector switch, or to focus an image by turning a knob.

Change of magnification is actually unimportant for any single type of problem. However, specific problems have certain magnifications which are most suitable. Tissue sections are best studied at low magnifications of about 1,500 x where fine structure may be related to gross structure most easily. Virus studies need high magnification of 6,000 x merely to be seen. In order to provide a wide range of magnifications in the permanent-magnet electron microscope, the

pole pieces are changed to provide any one of three fixed direct magnifications of 1,500, 3,000 and 6,000 times. Photographic plates exposed at these magnifications may frequently be enlarged to show new detail at magnifications of 40,000 times.

Focus is obtained by varying the accelerating high voltage.

Specimen Holder

The specimens used in electron microscopy are small. An object 0.0003 inch in extent will completely fill the field of view of the microscope at 6,000 x. Specimens are likewise very thin, less than 0.3×10^{-3} mm, and need to be supported on wire screens. Small particles are deposited on equally thin plastic films, in turn supported by the wire screens. For ease of handling, standard $\frac{1}{8}$ -inch diameter 200-mesh metal screens are used for specimen support. To insert a specimen into the microscope, the screen is clamped in a small holder and inserted in a hole drilled transversely into a $\frac{5}{16}$ -inch rod which slides in and out of the microscope across the optical axis of the system.

Figure 6 shows a specimen holder partially inserted in the specimen control rod. When the specimen holder is in place, the rod is pushed into the microscope. The specimen slides through a neoprene vacuum-sealing gasket which surrounds the rod. The only air admitted to the interior in the process is that in the open volume of the specimen holder. The rod slides until its end abuts the plunger driven by the large

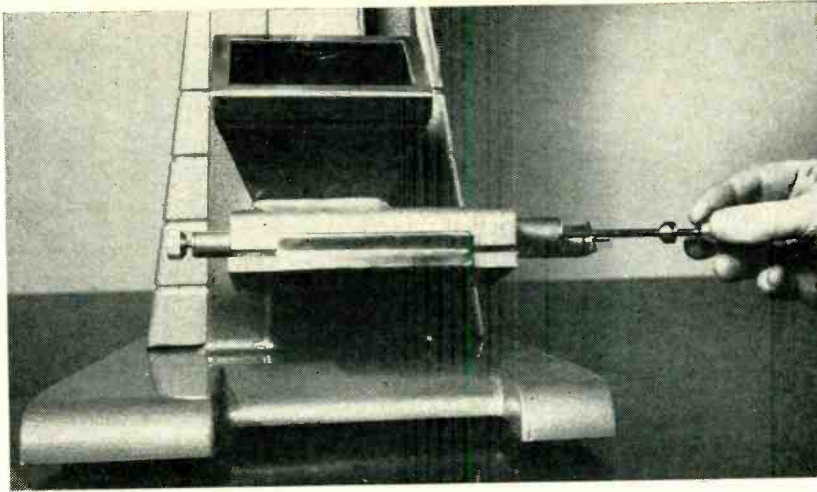


FIG. 7—Exposure of a photographic plate

right-hand knob on the upper part of the column. When this occurs, the specimen screen is over the axis of the microscope and the enlarged image of the specimen will be seen on the final screen.

Turning the right-hand knob drives the plunger in or out and the specimen follows with the rod which abuts the plunger. The specimen may be moved at right angles to this motion by rotating the rod by turning the large left-hand knob at the end of the rod. Since the specimen holder locates the specimen as far off the axis of the rod as possible, a rotation of the rod displaces all points on the specimen toward or away from the optical axis and also changes their distance from the objective lens. If the rotation is limited to three degrees from center, it is possible to scan three meshes in a direction perpendicular to the length of the rod and yet not move the specimen points out of range of focus of the lens.

This principle of using a single axis to produce both longitudinal and transverse movements as well as furnish a path for the introduction of specimens ranks along with the permanent-magnet lenses as a simplifying and economizing feature. Operationally, it has been found that the rod specimen stage has excellent stability in the face of heating from the gun, or from room vibration. The large control knobs permit ease of control and house additional mechanism. The left-hand knob contains a three-to-one friction planetary drive to increase the fineness of the trans-

verse specimen adjustment.

Final Image

The image is viewed through a front window wide enough for two people to make observations simultaneously. The phosphorescent material used to convert the electron image to a visible image is deposited on a surface perpendicular to the optical axis. Viewing the phosphor directly permits maximum brilliance in the image for a given beam intensity but requires oblique viewing. The fifteen-degree tilt in the microscope was applied to make comfortable viewing possible.

The photographic function of the electron microscope is essential to provide a permanent record, to provide an image which can be studied at length and measured accurately and to make use of the high resolution inherent in the electron image. It is practice to expose the photographic plate directly to the electron image which, like light, causes darkening in the developed negative. Direct exposure has the advantage of great photosensitivity, which permits photography of low-intensity images. Also, because of the fine-grain properties of the photographic plate, the detail in the image is all preserved on the plate. Photographic enlargements to ten times are frequently carried out. The drawback to direct exposure of the plate in earlier electron microscopes is the difficulty of inserting the plate.

In the permanent-magnet microscope, the functions of vacuum

valving, fluorescent screen and photographic shutter are carried out by a simple mechanical system comprising a sliding plate and a push rod. A circular groove in the bottom of the viewing chamber holds a neoprene gasket against which the valve plate presses to seal off the chamber during the periods when the door of the photo chamber is open for the insertion or removal of the plate cassette. Following insertion of the cassette and closing of the photochamber door, a knob at the right of the photochamber is pulled $\frac{3}{8}$ -inch to a stop. This motion slides the valve plate off the gasket, breaking the vacuum seal, and permits the plate chamber to be pumped out. The upper surface of the sliding plate is dished to hold a fluorescent screen, while a pin from the lower surface of the plate engages a catch on the cassette. When the valve-shutter rod is pulled to its extreme right-hand position, Figure 7, the valve plate is pulled from in front of the photographic plate. At the same time the light-tight cover of the cassette slides aside and the plate is exposed. Sliding the rod all the way back closes the valve and cassette. A relief valve on the left of the photochamber is used to admit air to the photochamber, permitting the door to be opened.

The simplification of operation of the electron microscope has been brought to a point where people can operate it usefully and confidently after less than an hour's instruction. The expense has been reduced to a point where small economic units can afford to use it. The performance of the instrument is such as to make it applicable in ninety percent of all electron microscopic problems.

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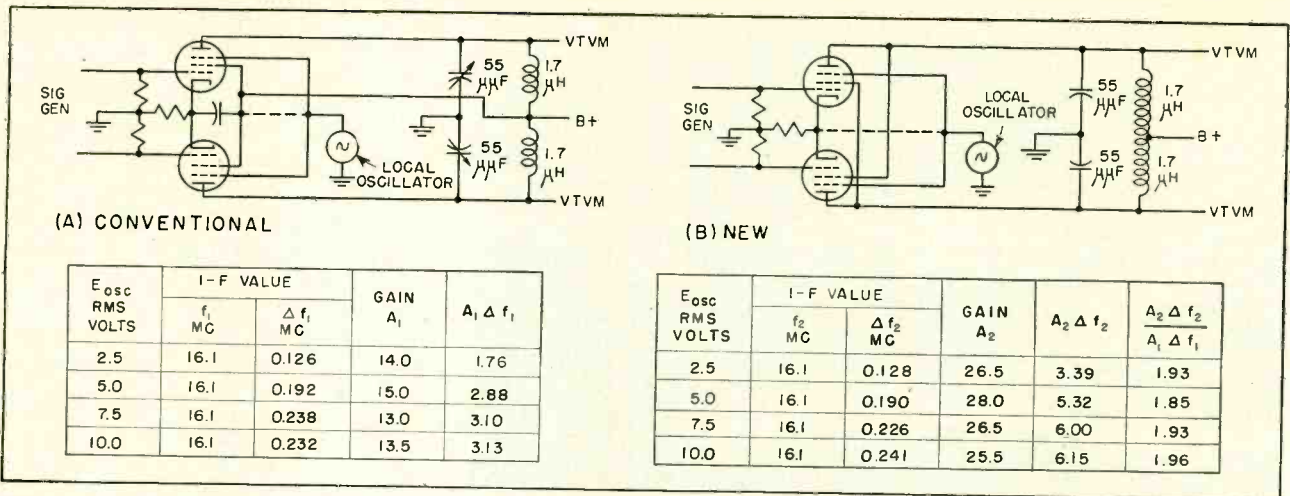


FIG. 1—Comparison of conventional balanced push-pull pentode mixer with improved method that places tuned circuit between screen and plate of each tube. Values of components are not necessarily the most desirable for the frequency and bandwidth used

GAIN-DOUBLING

Theory and experimental results for a method of obtaining twice the normal conversion transconductance from pentode mixers. Signal is applied to an inner grid, and No. 3 grid is used in an outer space-current local oscillator. Practical converter circuits for narrow-band broadcast receivers and wide-band f-m receivers are given

IN THE USUAL frequency mixer tube the conversion transconductance is approximately g_m/π , where g_m is the maximum signal grid-to-plate transconductance during the excursion of an oscillator cycle. The possibility of obtaining a conversion transconductance equal to $2g_m/\pi$ was first pointed out by E. W. Herold¹. In effect, his method involves changing the phase of the signal current 180 deg at the local oscillator frequency rate, using a beam-deflection tube or one having multihumped characteristics. The method to be described here achieves the same gain-doubling result more simply with a pentode mixer.

Analysis

The conversion transconductance g_c of a mixer tube, when considering a small signal modulating a

relatively large local oscillator signal of radian frequency ω , is

$$g_c = \frac{1}{2\pi} \int_{-\pi}^{+\pi} g_m \cos \omega t d(\omega t) \quad (1)$$

Solution of this equation does not give maximum conversion transconductance because the negative portion of the cycle subtracts from the positive portion. However, if the integral is observed from $\pi/2$ to $-\pi/2$ only, we obtain g_m/π as the maximum positive limit for conversion transconductance with conventional mixing. These limits are achieved in a triode mixer by imposing sufficient oscillator voltage on the No. 1 grid to cut off the tube during the negative portion of the oscillator cycle. In conventional pentode mixing with the oscillator signal on an outer grid, the same limits are obtained by diverting the space current to an inner grid of the tube during the nega-

tive portion of the local oscillator cycle. The goal, however, is to double this transconductance value.

With conventional triode and pentode mixing, the i-f signal is obtained from a tube element that is cut off for half of the tube-operating period. If by some means the sign of the integral of Eq. 1 could be changed for this cut-off half of the oscillator cycle, then the conversion transconductance would be doubled.

Consider a pentode mixer in which the incoming carrier signal is applied to the No. 1 grid and the local oscillator to the suppressor (No. 3) grid. Since a pentode maintains essentially constant current in the screen-plate region, each increase in plate current due to oscillator modulation of the suppressor must be offset by an equal decrease in screen current. As a

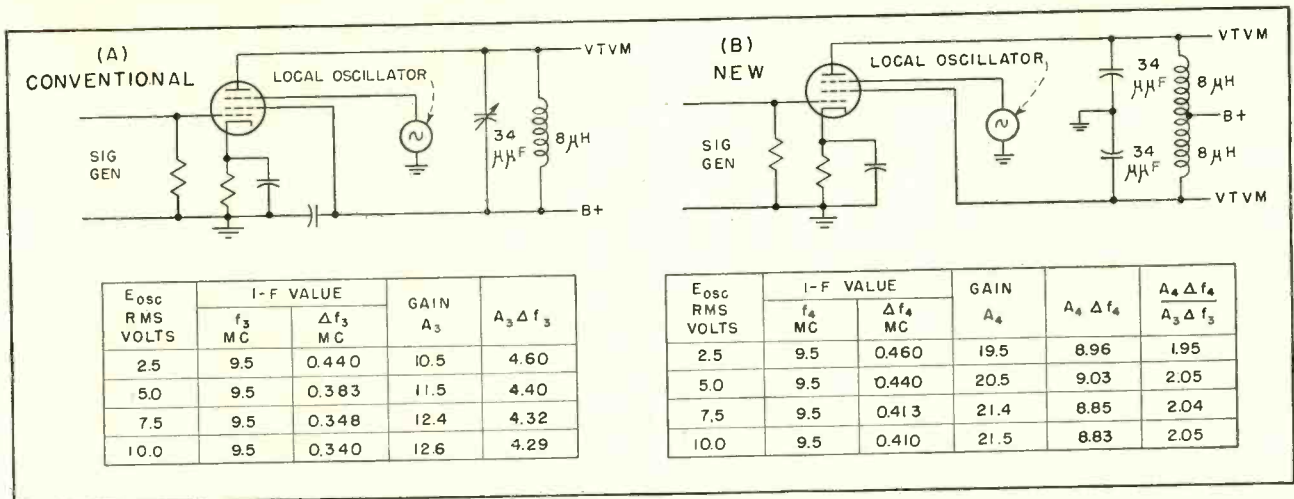


FIG. 2—Comparison of conventional single-tube pentode mixer circuit with improved method that eliminates screen bypass capacitor so tuned circuit is between screen and plate. Values of corresponding inductances and capacitances should be equal as indicated

Frequency Converters

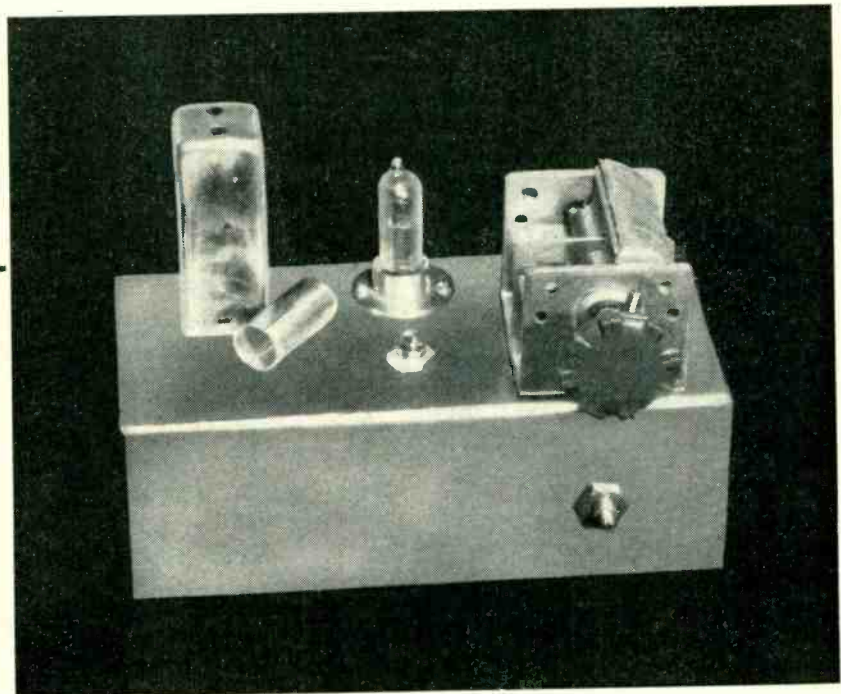
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result, the i-f components of plate and screen currents are 180 deg out of phase and can be added in a conventional push-pull manner to get twice the gain from the tube. Actually, the mere placing of a tuned circuit between the plate and screen changes the sign of the integral in Eq. 1 for half of each cycle to give the desired doubling of conversion transconductance.

Verification

Experimental verification of gain doubling with this frequency-mixing process is given in Fig. 1 and 2. Performance of a conventional balanced type mixer is presented in Fig. 1A and results for the new circuit, using the same tubes under the same d-c operating conditions, are in Fig. 1B. The tubes were developmental types with many-turns-per-inch suppressor grids. The



Subminiature pentode converter for broadcast band use, employing improved circuit of FIG. 5 to achieve more than twice the gain of a conventional 6BE6 circuit

oscillator voltage is used as a variable.

Since the voltage gain is inversely proportional to Δf and the two vary with oscillator voltage, the product of these two terms serves as a convenient means of comparison between the two sys-

tems. The last column of the tabulation in Fig. 1B indicates the ratio of $A_4 \Delta f_4$ for the new system to $A_3 \Delta f_3$ for the conventional system. These values center about a ratio of 2 to 1, which is predicted from the theory.

As a further check and compari-

son, the new frequency-conversion method was compared with the conventional method when using a single tube. Data for a conventional single-ended mixer circuit is given in Fig. 2A, and corresponding data for the new circuit in Fig. 2B. The ratios are again approximately 2 to 1.

The foregoing data were obtained with the suppressor grid operating at zero d-c bias rather than the grid-leak bias that is usually employed. Operating the grid

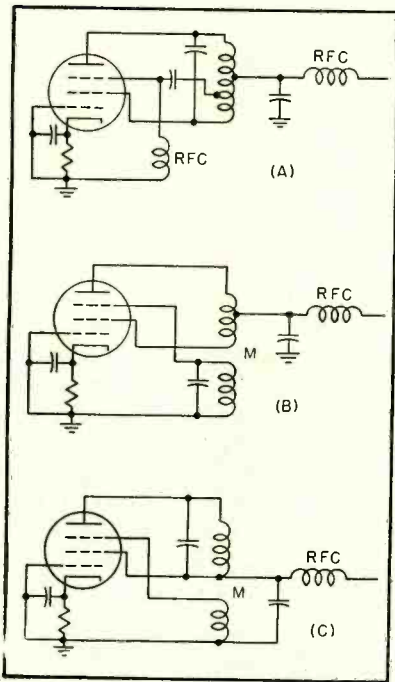


FIG. 3—Balanced and unbalanced oscillator circuits employing new gain-doubling technique

at zero bias results in a much greater peak g_m and thereby increases conversion transconductance. If sufficient oscillator voltage is impressed, the plate current is swung into saturation and g_c approaches the ideal value of approximately 32 percent of the peak g_m .

Isolation

Another interesting aspect of the circuit is the isolation it offers to signals that tend to pass through the mixer tube at the intermediate frequency. Isolation exists, since any signal on the No. 1 grid produces modulation of the same phase on the screen and plate currents, and will cancel out in the push-pull i-f transformer. This action makes

it somewhat difficult to align the i-f by the usual manner of placing the i-f signal on the signal grid of the mixer tube. In this case the signal can better be placed on the oscillator grid. The degree of isolation is determined by the degree of balance in the primary of the i-f transformer and by the transconductance from signal grid-to-plate relative to the transconductance of signal grid-to-screen.

In a pentode we are mainly concerned with shot-effect noise and partition noise. The former is due to time-varying emission from the cathode, and the latter is due to random distribution of cathode current to the positive electrodes in the tube.

Noise Suppression

Assume an ideal pentode in which partition noise does not exist. Assume also that there is a push-pull connection between plate and screen, and that the screen and plate currents are precisely equal. The noise in the plate and screen would then be of equal magnitude and identical phase, disregarding transit-time effects. With a perfect output transformer, there would be no noise output from the tube, because of cancellation within this transformer.

Now, imagine another ideal pentode in which no shot-effect noise exists, but in which partition noise does exist. In this tube any noise variation that takes place in the plate circuit must be accompanied by an equal and opposite noise variation in the screen circuit, since space current is perfectly constant. Thus, if this push-pull connection has in some way doubled the effective transconductance, the equivalent noise resistance of the tube has

not changed since the effective noise has also been doubled.

The pentode mixer circuit presented here is actually the combination of these two ideal cases. It therefore has somewhat smaller equivalent noise resistance in the circuit than does a conventional mixer, since the shot-effect noise has decreased while the affect of partition noise remains unchanged.

Converter Tube

In conjunction with this work on the mixer circuit, a program was also carried out to combine this circuit into a converter tube that performs the functions of mixer and local oscillator. In this converter, the outer space current oscillations that exist between the outer elements of a multigrid tube are utilized. The resulting converter circuit gives four times the voltage gain with 30 percent less cathode current relative to the 6BE6 converter. The equivalent noise resistance of this converter was below 18,000 ohms, which is less than one-tenth that of the 6BE6.

The tube characteristics most desirable for the oscillator are those of a pentode whose No. 3 grid-to-plate transconductance is relatively high. This No. 3 grid is used as the control grid, and the plate or screen as the oscillator anode.

The oscillator may be either the balanced or unbalanced type. In the balanced oscillator, shown in Fig. 3A and 3B, the plate-screen coil is center-tapped to r-f ground. This oscillator is suited to a balanced-type circuit since the current variations, as caused by No. 3 grid modulation, are 180 deg out of phase in the plate and screen. The plate voltage holds the same phase relationship to the controlling grid

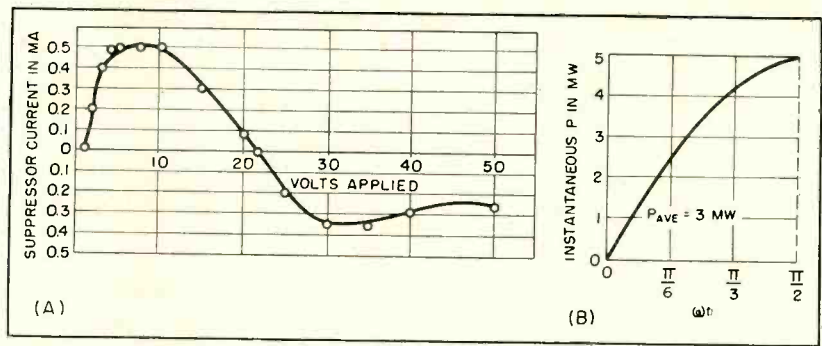


FIG. 4—Characteristic curves for No. 3 grid of typical experimental pentode

voltage as it does in a conventional oscillator.

For unbalanced operation, either plate or screen may be grounded to r-f as in Fig. 3C. Since the screen-plate current is nearly constant, the oscillations are confined to the outer space of the tube.

The No. 3 grid characteristics for a typical experimental pentode are shown in Fig. 4A. The negative resistance characteristic encountered above 10 volts tends to enhance oscillations. To find the required grid-driving power, a sine wave can be impressed on the suppressor grid and a time plot of current obtained from the grid characteristics. The product of instantaneous voltage and grid current is shown in Fig. 4B. A peak swing of 10 volts is used because this value produces plate current cutoff and is in accordance with characteristics that follow. The average power may be obtained by integrating the instantaneous power curve. The resulting average power is three milliwatts, which is very low and normally will be less than the associated circuit losses.

Converter Design

It is possible to calculate the tickler coil impedance required for a particular application. Suppose an oscillator is to be built at 20 mc in which a tickler coil is placed in the plate circuit to excite a tuned circuit connected to the No. 3 grid, and a total driving power of 15 milliwatts is required. The available exciting power is proportional to the external voltage drop, or in this case the reactive drop across the tickler coil. Then $P_{\text{exciting}} = I_{\text{eff}}^2 \omega L = 15 \times 10^{-3}$. The effective plate current for the development tubes used is approximately 4 ma. The required tickler coil impedance is then $\omega L = 15 \times 10^{-3} / (4 \times 10^{-3})^2 = 938$ ohms.

These outer space current oscillations may readily be obtained from a pentode as used in Fig. 5 and 6, and the application of a signal to the No. 1 grid will result in a simplified converter. In each circuit, a tickler coil is placed in series with the i-f transformer primary to provide feedback to the No. 3 grid, which is tuned to the local oscillator frequency. In Fig. 5 the

screen is grounded for r-f. Figure 6 represents a similar circuit in which the i-f is connected in push-pull between the screen and plate, and results in increased conversion transconductance.¹ The circuit of Fig. 5 is most useful in narrow-band applications, since the plate resistance in converter use is much larger than the effective plate-screen resistance. Conversely, Fig. 6 is more applicable to wide-band circuits.

The above circuits are operated with zero d-c bias on the suppressor grid. This type of operation is desirable since greater conversion transconductance will result owing to the larger peak plate current. A grid-leak bias on the grid of the oscillator is not necessary with the outer space current oscillator, as it would have little effect on the average current.

It is desirable that the peak swing be sufficient to produce plate-current saturation during the positive excursion of the local-oscillator cycle, and plate-current cutoff during most of its negative excursion, since these are the desired characteristics for maximum conversion transconductance.

Comparisons

The most important characteristics of a converter-type tube are probably (1) conversion transconductance, (2) plate resistance, (3) noise, (4) isolation between signal and oscillator circuits, which is indicative of antenna radiation, (5) voltage gain as a function of wide-

range tuning, and (6) automatic volume control, which indicates the cutoff characteristics of a particular tube and any undesirable detuning effects. These characteristics will be discussed in connection with a comparison of the new high-gain pentode converter circuit of Fig. 5 and a conventional 6BE6 frequency converter for the same narrow-band application (550 to 1,600 kc).

Before making comparative measurements, the oscillator voltage on the No. 3 grid was measured as a function of tuning. The oscillator voltage varied from 19 volts at 1,006 kc (the low end of the oscillator range) to 66 volts rms at the top frequency of 2,056 kc. This wide range of oscillator voltage is undesirable from the viewpoint of oscillator radiation, hence a series R-C circuit was used to load the oscillator. Values of 10,000 ohms and 6.8 μmf discriminate against the higher frequencies as desired to keep the range of oscillator voltage between 11 to 19 volts rms, which is within the practical limits of most converters.

Comparative sensitivity values are given in Fig. 5. With the experimental type pentode, the components were tuned for each individual measurement. The voltage gain was measured from the signal-generator terminals to the secondary of the i-f transformer. The i-f transformer used was designed as an output transformer, and consequently had closer coupling than that usually found in input i-f transformers. With the conven-

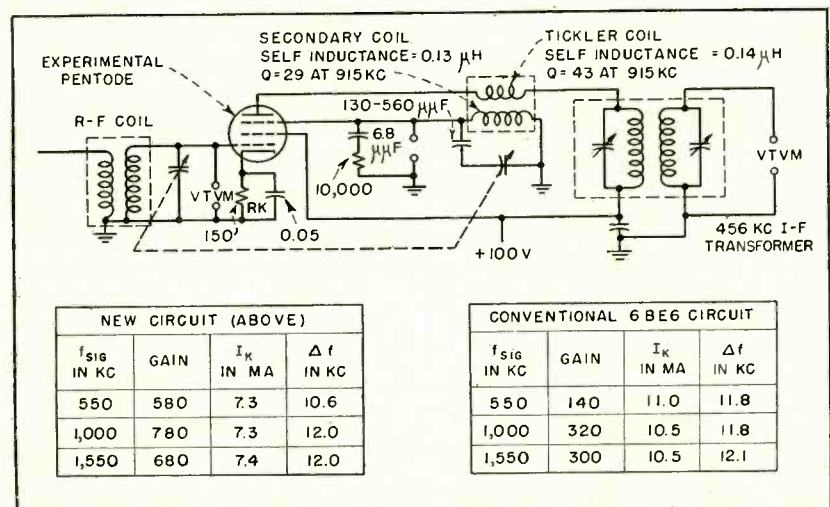


FIG. 5—Narrow-band version of new converter circuit, suitable for broadcast band, and comparative performance data on conventional circuit

tional circuit, plate and screen voltages were 100 volts, and the signal grid was biased to -1.5 volts. The circuit was optimized for voltage gain.

The comparative data shows that greater than twice the voltage gain can be obtained with the pentode with 30 percent less cathode current. The increased voltage gain results from the increased conversion transconductance.

The conversion transconductance of the experimental pentode was approximately $1,200 \mu\text{mhos}$. This conversion transconductance is easily determined for this type of operation by measuring the g_m of the signal grid with $+10$ volts on the suppressor grid, and taking 30 percent of this g_m value as the conversion transconductance. This is accurate to within a few percent.

The effective mixer plate resistance for the new type of operation is approximately three times the value measured for the tube as an amplifier. This value was $350,000$ ohms for the development tubes used, as contrasted with 1 megohm for the 6BE6. The conversion transconductance of the 6BE6 is $475 \mu\text{mhos}$.

Oscillator Radiation

Radiation back to the antenna from a converter tube depends on the capacitance and space charge coupling between the oscillator grid and the signal grid. In the circuit of Fig. 5, oscillator currents are confined to the outer space of the tube so there is little or no space-charge coupling. The capacitance from the signal grid to oscillator grid of the tube under these conditions is approximately $0.10 \mu\mu\text{f}$, while the corresponding capacitance for the 6BE6 is $0.15 \mu\mu\text{f}$. The relative coupling values from the oscillator to the signal grid at signal frequencies of 550, 1,000 and 1,550 kc are 0.01, 0.07 and 0.13 respectively for the 6BE6 and 0.01, 0.05 and 0.21 for the pentode.

The space-charge coupling within the tube acts with a 180 -deg phase shift relative to the direct capacitive coupling voltage. In most converters, these effects are controlled so that they are approximately equal on the broadcast band. This is the reason that the coupled volt-

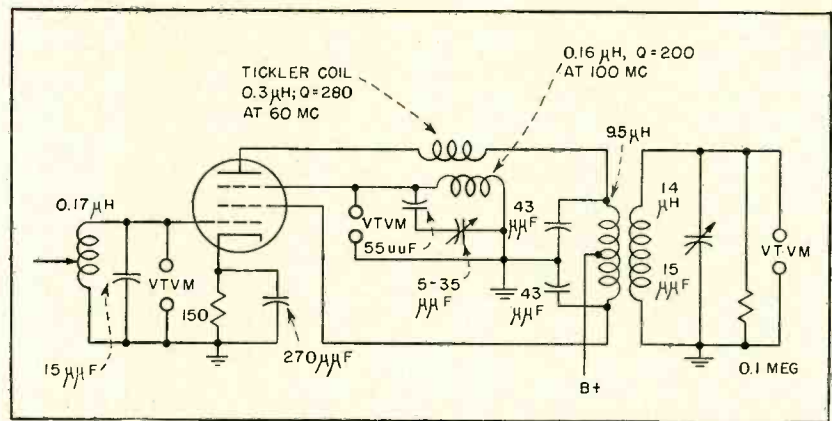


FIG. 6—Wide-band version of new converter circuit

age is slightly less with the type 6BE6 in spite of the fact that its capacitance and space-charge coupling are greater.

AVC Action

The action of an avc voltage on the signal grid of the experimental pentode changes the oscillator amplitude as well as the signal-grid g_m . This gives accentuated avc action, and may require a very remote cut-off characteristic for proper operation. Since extensive bias will ultimately result in a reduction of oscillator grid g_m to the point where oscillations will cease, extended avc application (1,000 to 1 reduction of gain) is not possible in this new converter.

In conjunction with avc, it is important to consider the amount of frequency shift that results from its application. To obtain this relative measurement, the gain of the two systems was decreased by the same ratio, and the frequency shift of the oscillator section was measured. The results indicated that the frequency shift was comparable in the two systems, but in opposite directions; the frequency of the 6BE6 converter decreased with decreasing gain and the frequency of the new converter increased with decreasing gain.

F-M Converter Circuit

Modifications needed in the new converter circuit to meet the requirements of the f-m band are given in Fig. 6. The relatively wide bandwidth permits the use of a push-pull i-f and derives increased gain. At 100 mc the voltage gain from the grid through a double-

tuned i-f transformer is 27.5. (The calculated gain of the 6BE6 under similar conditions is one-fourth this value.) The center of the i-f band is 10.7 mc and the bandwidth at the half-power points is 350 kc. The frequency drift of this oscillator circuit was compared with that of a triode in a Hartley circuit and found to be nearly equal. The converter had less frequency shift as a function of filament voltage, but more as a function of supply voltage.

Conclusions

Increased gain can be obtained by using a pentode tube as a converter, with the signal applied to an inner grid and the No. 3 grid used as an outer space current local oscillator. Four times the gain of the type 6BE6 may be obtained by using this less complicated tube, with 30 percent less cathode current. Simple tube construction, high conversion transconductance and low noise characterize this converter. The Sylvania type 5636 and SN1007B tubes are suitable for this application.

The author acknowledges the valuable assistance of B. F. Tyson and James Cooper who supplied measurements that confirmed the theory outlined here and John B. Grund of Sylvania's Emporium division, whose measurements in practical circuits contributed greatly to this project.

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Low-Reflection PICTURE TUBES

Face plates is first etched, either chemically or by liquid-honing abrasive-blasting method, to produce light-diffusing characteristic. Plates thus etched are then treated with hydrofluoric acid to restore transmission loss introduced by first etch

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THE HIGH OPTICAL QUALITY inherent in metal cathode-ray tube face plates has turned out to be more of a drawback than a blessing.

When these tubes were first introduced, glass tube manufacturers took steps to equal their face-plate quality by chromium plating and polishing the molds, with the result that both types today are prone to specular reflections. These reflections of external light sources in a room are more noticeable because of the dark glass now almost universally used in face plates.

Early Attempts

Attempts to reduce undesirable reflections by methods already employed in treating optical instruments have met with little success for various reasons. For example, one-quarter-wavelength thick films^{1,2} are difficult to mass produce. Moreover, such films are quite fragile and give a characteristic purple tint since they are actually designed for a minimum reflection at only one wavelength, usually 5,550 Å, which is the peak of the human eye sensitivity curve. Skeletonized layers, in which the constituents of the glass are etched out on the surface by hydrofluoric acid to leave only a film consisting largely of silica,³

are also corrective for only one wavelength and have some residual reflected color.

For picture tubes one can resort to other solutions to reduce reflections, such as a polarizing filter combined with a quarter wave retardation layer in front of the tube face. These filters, in addition to

the expense involved, absorb an appreciable portion of the useful light and the residual reflections are also tinted. Another possibility of reducing reflection involves scattering the light, and lacquer coatings have been tried to achieve this result.⁴ However, these coatings are not durable and in most cases they



Television picture taken from 12-inch metal tube. Reflected image of fluorescent lights from untreated portion of face plate shows advantage of process

Chemical Process with Acid Treatment

Liquid Honing with Acid Treatment

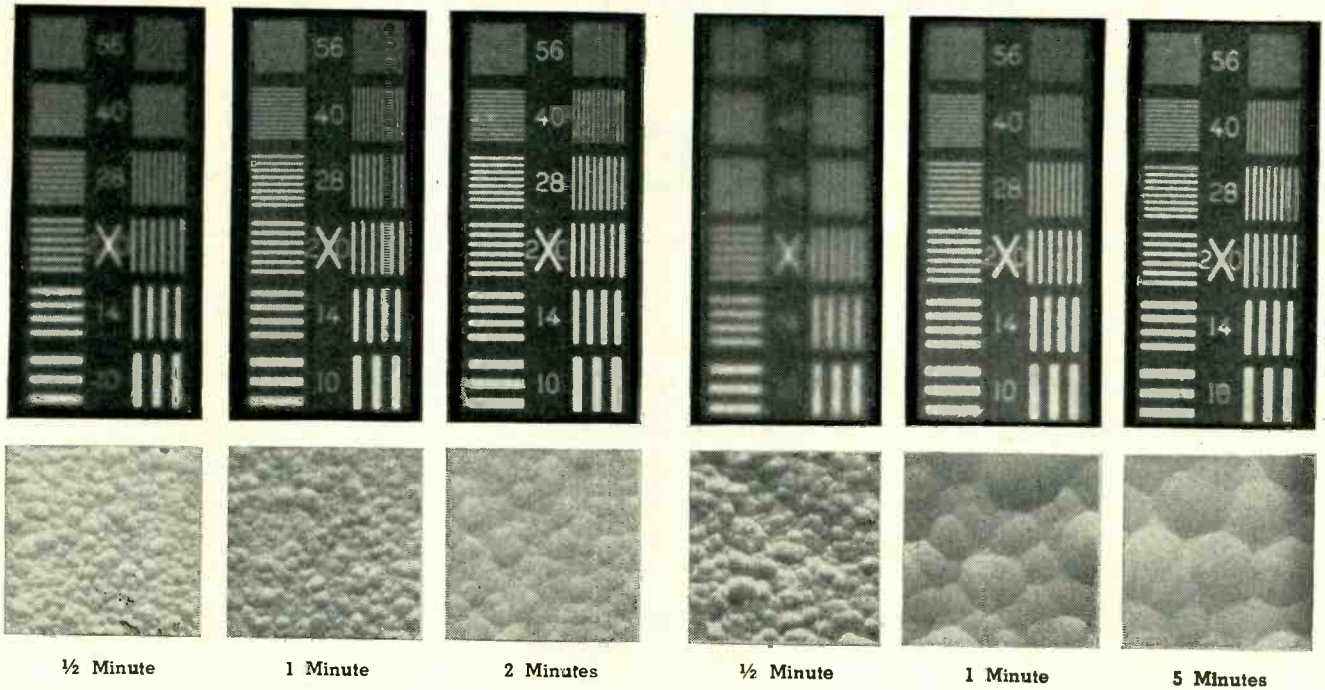


FIG. 1—Resolution test charts photographed through face plates having front surfaces treated by the two methods described and subsequently etched in hydrofluoric acid for periods of time indicated. Photomicrographs (approximately 125 microns square) below show processed surfaces

are too diffusive, thus impairing the quality of the transmitted image.

New Method

The method described in this paper when adequately controlled has none of the aforementioned disadvantages. The surface of the plate is first etched either chemically or by a liquid abrasive-blasting method known as liquid honing. The latter is a process in which the plate is subjected to a high pressure spray of abrasive particles suspended in water. Either of these processes creates a surface having a light-diffusing property, which reduces the specular reflection but also tends to deteriorate the quality of the transmitted image. The etched plate is then subjected to a treatment in hydrofluoric acid, either by dipping or spraying, until the transmitting characteristics are restored to the extent required by test resolution patterns. The result of this processing is shown in the accompanying photograph, which shows a television image as seen through a face plate only one-half of which is treated in the described manner. The untreated half clearly illustrates how the reflected image of fluorescent light tubes, for ex-

ample, can obliterate the transmitted picture information.

In Fig. 1 there are a series of resolution patterns as photographed through face plates which have been surface-etched by chemical means and liquid honing, respectively, and then subjected to hydrofluoric acid for varying lengths of time. From these photographs, it is apparent that control of the acid bath is necessary to preserve the image quality of the transmitted picture. In each case reading left to right, the first plate is considered to be unresolvable; the second is just resolvable, and the third is quite acceptable.

In order to investigate the surface structure of the treated face plates, photomicrographs of these same samples were taken and are shown. As the acid treatment is continued on any particular sample from a point of minimum reflection and maximum diffusion, the hill-like structures increase in diameter and become more flattened. The acid tends to dissolve the roughened edges and smooth out the surface to some extent. The surfaces etched by chemical means are much more uniform and give a greater number of and smaller hills for the same transmitting and reflecting quali-

ties than those etched by the mechanical method. Tests made with a surface analyzer also indicate that the chemical etch provides a much more uniform surface.

Reflection Characteristics

The reflection characteristics of these treated face plates have been studied quite extensively. Plates treated by the chemical etch method always exhibit a minimum reflection point before being subjected to acid, whereas in the case of liquid honing, the surface may be lightly etched, then brought to this minimum value by the acid treatment. This action of the acid can be seen in Fig. 2A, which is a plot of reflectivity as a function of acid treatment time. The reflection is specular before the minimum is reached and of a diffuse nature from that point on.

Measurements were made with a Weston photocell having a Viscor filter in a reflectometer built for this purpose. A collimated light beam is reflected from the surface under study at an angle of 35 degrees to the normal. A typical surface after being lightly liquid-honed has a reflection of 50 percent of that from the two sides of a conventional filter-glass face plate, or ap-

proximately 3.5 percent in terms of 100 percent from a perfect reflector.

It should be remembered that the combined reflection from the two surfaces of a clear glass face plate is approximately 9 percent. The filter-glass face plate now in general use has around 25 percent absorption, the reflection from the back surface is thus reduced to 2½ percent and the total from both surfaces to 7 percent.

Although still quite transparent, the liquid-honed surface has a misty appearance which produces a somewhat diffuse transmitted image quite objectionable for television applications. With subsequent acid treatment, however, the specular reflection decreases and the diffusion of transmitted light increases until the aforementioned minimum point of reflection is reached.

With further acid treatment the reflected light becomes almost entirely diffuse and the transmitted light becomes more specular. This behavior may be explained by the fact that the acid attacks the glass selectively wherever the surface has been broken and tends further to roughen the surface. After a period of time corresponding to the minimum on the curve, the acid becomes trapped and only the crests or high spots are attacked, thus producing a smoothing effect. This explanation is partially borne out by the fact that the negative slope of the curve is much steeper than the positive slope, indicating that the relative areas of roughened surface to smooth surface are much greater after the point of minimum reflection has been reached than before.

Limits on the residual reflection have been experimentally correlated with the resolution desired and the thickness of the plate. The resolution of a transmitted image in contact with the back surface of the treated plate is inversely proportional to the thickness. Furthermore, as the plate resolution increases, the reflection increases. In order to maintain high picture quality, these treated plates must resolve at least 2.2 lines per mm which corresponds to approximately 4.5 television lines per mm, or a definition of approximately 850 lines on a 12½-inch tube raster. It

has been found that metal tube face plates which will give this resolution have a minimum reflection of 21 percent of the combined reflection from the two surfaces of an untreated filter-glass face plate which, as explained above, would correspond to approximately 1.5 percent of the total incident light. For all-glass tubes where the thickness across the face may vary from ¼ to ⅜ inch, a minimum reflection of 35 percent must be tolerated to achieve the desired resolution.

Additional Tests

Several tests were made on completed television tubes having low-reflecting faces. It was found that there is no decrease in luminance from treated face plates as measured normal to the tube. There is, however, a slight falling off as the angle of observation is increased. This directional effect of various types of tube faces now in production is compared in Fig. 2B. It is evident that the plates treated by the liquid-honing process are slightly more directional than those treated by the chemical etch. This is due to the fact that the former gives a heavier etch, and more attenuation is to be expected as the light passes obliquely through it. Tests to determine whether or not any color shift is introduced by the etching process have proven that there is no effect either on the axis or at large angles of observation.

It is interesting to note that tubes with treated face plates appear to be mechanically stronger than those with untreated face plates, judging by pressure tests performed on both types of tubes. Similar experience has been reported in the manufacture of incandescent glass bulbs where acid treatment followed abrasion.⁵

Thus far treatment of the outer surface alone has been considered, the inner surface remaining specularly reflective. In order to reduce or mask the reflection from the inner surface to a negligible amount, the outer surface treatment must progress farther than desired. This reflection also can be eliminated by the low-reflection treatment of the inner surface. For a given reflectivity, the outer surface diffusion can therefore be made much less with a consequent improvement in the quality of the transmitted image. Of the two processes mentioned, the liquid-honing is more suitable for application to the finished tube, in which case only the outer surface is made diffuse. The chemical abrasive process can equally well be applied to the face plate before sealing it to the metal cone and, therefore, metal tubes can be easily fabricated with both surfaces treated, with the inherent improvement in resolution.

Tests show no loss of contrast for low-reflection treated tubes under normal viewing conditions. With intense external light, however, the residual light scattered back to the viewer has the effect of lowering the contrast ratio. But, multiple reflections within the glass are actually reduced by the combined abrasive etch and polishing treatment.

The authors are indebted to Joseph A. McCormick of the Dearborn Glass Company for his cooperation and persistent efforts in the successful development of the chemical etch process mentioned above.

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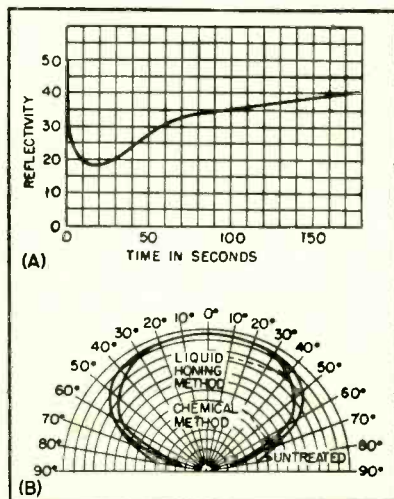


FIG. 2—Plots of reflectivity as a function of time of acid treatment after liquid honing (A) and polar distribution of luminance curves (B) for picture tube face plates

ADJACENT-CHANNEL

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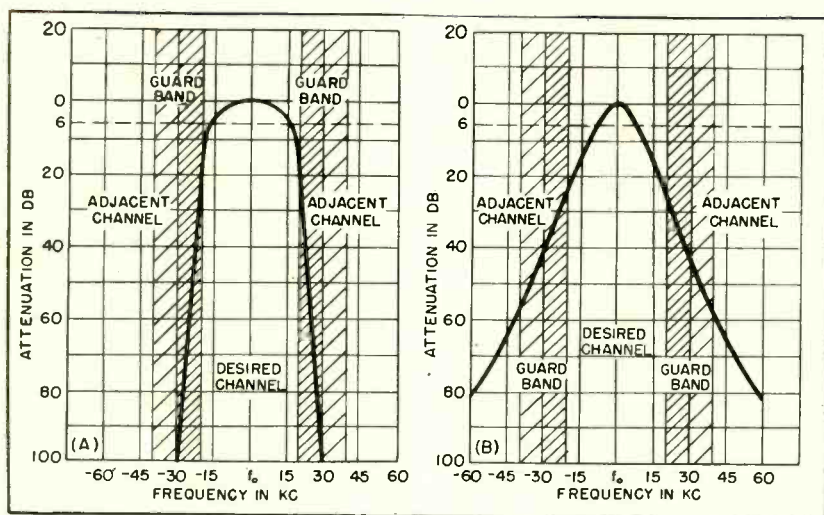


FIG. 1—Desirable selectivity curve is shown at A. The curve of a conventional Motorola receiver is shown at B

THE FREQUENCY SPECTRUM available for radio communications remains the same but the need for new channels is ever increasing as the number of applications and the number of users of electromagnetic waves increases. The problem of obtaining more useful channels is particularly acute in television and in mobile communication systems.

One solution to this problem would be to go to higher frequencies where more bandwidth is available. Some services such as radio relays and other point-to-point radio communication could be transferred to frequencies above 200 megacycles, but this is not necessarily the case with the mobile service. In this service the requirement of line-of-sight is not often fulfilled and so the ground wave must be relied upon. Such a wave is not propagated well even at frequencies as high as 200 megacycles and shadow effect becomes more and more pronounced as the frequency increases.

On the other hand, in thickly populated cities the waveguide effect of the streets may cause, at higher frequencies, considerable condensation of electromagnetic waves, usually accompanied by pronounced standing waves. In this special case, higher frequencies may be well suited for communication, but in general, mobile communication systems should

operate in the region below 200 megacycles. For this reason, closer channel spacing and the ability to use adjacent channels are both very important in the mobile service.

The receiver design principles to be outlined were first applied to receivers for the mobile service, and for this reason an f-m receiver working in the 152 to 162-mc band has been chosen as an example, although the principles are by no means limited to this field and could be applied with equal benefit to any a-m, f-m or television receiver.

Requirements

For successful adjacent-channel operation, a sufficient rejection of the unwanted signal should be achieved at the edge of the adjacent channel. The receiver should accept the band of frequencies required by the received signal and its modulation sidebands without appreciable attenuation. Therefore, a rather rapid transition from no attenuation to full attenuation has to occur. This transition has to occur within the so-called guard-band which is an unused narrow band between channels in which no modulation exists. Figure 1A shows a desired practical shape of selectivity curve. The ideal square selectivity shape is not practical because it has two discontinuity points and infinitely steep sides. The performance of such a square

curve would not be satisfactory because of nonlinear phase characteristics.

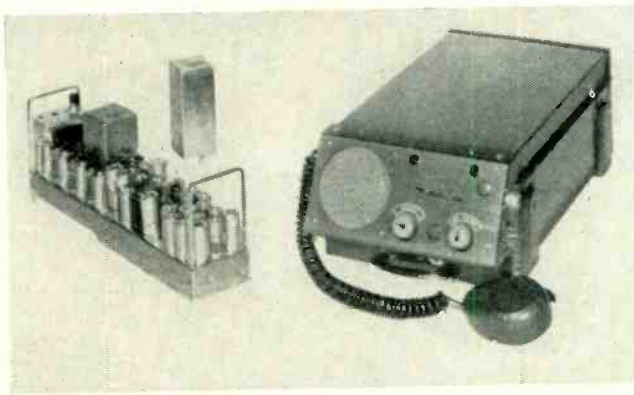
Figure 1B shows for comparison the average selectivity curve of an ordinary receiver* obtained by using several tuned circuits. Usually the top of the curve is not wide enough and the sides of the curve are not steep. It takes the whole adjacent channel, not just the narrow guardband, before substantial attenuation is obtained. In addition, the shape of this curve depends greatly upon the tuning of the individual circuits and it will vary from day to day due to change in temperature.

The minimum receivable signal can be easily determined from the theoretical noise and the noise figure of the receiver. For example, for a 40-kc bandwidth f-m police receiver, the theoretical noise is equal to KTB or $4 \times 10^{-21} \times 40 \times 10^3$ watts, or 158 db below a watt. Assuming the practical noise figure of a receiver to be 12 db, the noise level will be 146 db below one watt or 0.35 microvolt at the 50-ohm antenna input cable. A carrier giving 20-db quieting will, in this case, be of the order of 0.5 microvolt, which may be considered the weakest usable signal.

The strongest unwanted signal which can be rejected by the receiver depends greatly on the desensitization and intermodulation characteristics of the receiver. By desensitizing we mean the phenomenon occurring when a strong signal decreases the total gain of the receiver. This is generally caused by the grid voltage on one or more tubes swinging into the positive region and thus building up additional bias or loading the grid tuned circuit (or circuits) by grid current.

REJECTION RECEIVER

Desensitizing by strong local stations just outside desired-frequency guardbands, as well as intermodulation and spurious responses, is minimized by concentrating selective elements largely ahead of amplification. Hermetically sealed passive bandpass filter is heart of system



Strip receiver chassis, one filter and complete mobile unit which incorporates some of the design techniques described

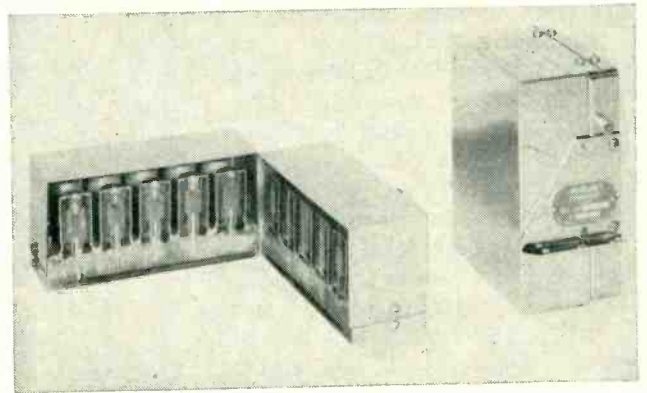


FIG. 3—Cutaway view of passive filter and a complete cased unit for a receiver

Situations frequently arise, particularly in mobile communication practice, where a police car, for example, has to receive messages from a remote station, or another police car, while it is operating in the close vicinity of the transmitter of a taxicab company, which may be on the adjacent channel. Under such conditions many receivers are completely desensitized or blocked by this high-level signal.

The amount of unwanted signal which can be tolerated depends greatly on the receiver construction. In an average receiver, the first r-f tube has a grid bias of the order of 0.7 volt, and this would be the peak voltage acceptable, the rms value being 0.5 volt. Assum-

ing an input tuned circuit step-up ratio of 5 to 1, a 0.1-volt signal at the antenna input is all that can be tolerated. This means that the selectivity that can be expected in the receiver is 0.1 volt to 0.5 microvolt or 106 db. Practically, most receivers have a much lower limit, because they build up the gain before selectivity, which is obtained in the last i-f stages.

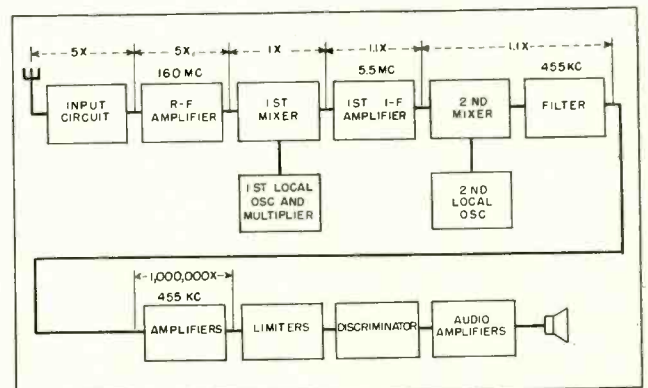
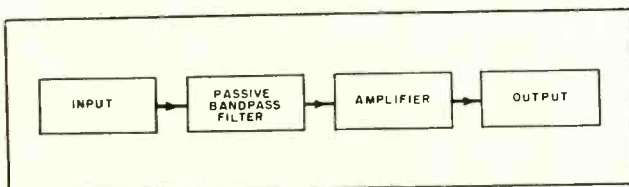
Intermodulation

Another problem resulting from crowding of the spectrum is intermodulation. If there are two strong transmissions on frequencies $f \pm \Delta f$, and $f \pm 2\Delta f$, where f is the receiver frequency and Δf is the channel spacing (or some multiple there-

of), then the second harmonic of the first transmission will be generated in the receiver because of nonlinearities in the amplifying tubes, usually the mixer stage and possibly the r-f stage. This second harmonic, whose frequency is $2f \pm 2\Delta f$, will beat with the $f \pm 2\Delta f$ transmission and create a beat note of frequency f . Once frequency f has been created in a receiver, no amount of selectivity of the i-f circuits can prevent interference. This interference may be weak, so that it merely opens the squelch in the absence of a desired signal, causing annoyance, or it may be so strong as to completely block the receiver. If the signals on adjacent channels are properly spaced

FIG. 4—Stages of a mobile receiver employing the design discussed in the text

FIG. 2—Block diagram of new receiver using the passive band-pass filter



frequency-wise, a very small non-linearity in receiving tubes is sufficient to create a pronounced interference, and consequently the intermodulation will exist with signals much weaker than necessary to desensitize the receiver.

The spurious responses of a receiver, such as image frequency, or frequencies obtained by beating with some multiple of the local oscillator (if crystal and multipliers are used), are not exactly connected with the adjacent-channel operation problem. It is nevertheless good practice to keep them down, since, with the present crowding of the spectrum, strong transmission at any frequency should be expected. If the selectivity of the receiver is such that it rejects a transmission on the adjacent channel 100 db stronger than the desired signal, then, consistently, all the spurious responses should be 100 db down.

Band-Pass Filter

A design illustrated in the block diagram of Fig. 2 features:

Separation of selectivity and amplification.

Placing all selectivity-determining elements in front of the amplifier stages.

Obtaining a suitable (approaching a square top) selectivity curve by using passive band-pass filter technique at a suitable low frequency.

Design of an input circuit, in front of this filter, consisting of one or more frequency converters with a minimum amount of amplification (consistent with good signal-to-noise ratio) and maximum spurious rejection.

The passive band-pass filter is the heart of the receiver and can be built by using several coils and capacitors in constant- K and M -derived sections. The center frequency of the filter can vary from 50 kc to some 20 mc, depending on the particular application (a-m, narrow-band f-m, wide-band f-m or television). The filter can be made with sharp enough slopes to assure at least a 100-db rejection at the edge of an adjacent channel.

The top of the filter response curve could be made very flat but, to obtain desired phase characteristics, the corners of the curve

should be reasonably rounded. Such a filter gives a stable and permanent performance since once the filter is factory adjusted and sealed there is no need or possibility of readjusting it in the field, and therefore the selectivity characteristics of the receiver remain constant. Should the need arise to change the width of the channel, or the selectivity characteristics, a simple exchange of the filter will permit this, since the filter is the only factor determining selectivity. Also, in television practice, the curve obtained by the filter can be of any desired shape, and as perfect a vestigial operation as may be required for good video reception can be had by properly designing the filter.

To illustrate how such a filter may be constructed, Fig. 3 shows a complete factory-sealed and adjusted filter used in a mobile communications receiver, and also a cut-away view. The coils of the filter are adjusted by iron slugs and then are sealed completely in compound, so that they will never change their characteristics. This particular filter is composed of fifteen coils arranged in more or

less conventional constant- K and M -derived sections.

Receiver Input

The head end starts with an antenna matching circuit followed by an r-f stage. The well-known cascode circuit can be used for maximum signal-to-noise ratio. The selectivity should be sufficient to reject the image frequency by about 100 db. Since the filter following the head end works on a relatively low center frequency, the image frequency is usually too close to the desired frequency. Therefore, in general, in f-m receivers two converters are used, one converting to a 5 to 10-mc first i-f, and the other to the filter frequency. In this way, sufficient image rejection can be obtained by using two or more loosely coupled tuned circuits in both r-f and first i-f stages.

The gain of every head-end stage should be held at a minimum consistent with good signal-to-noise ratio. If most of the noise is generated by the first tube and not by the antenna circuit, as often happens in vhf receivers, it means that the voltage gain between the first

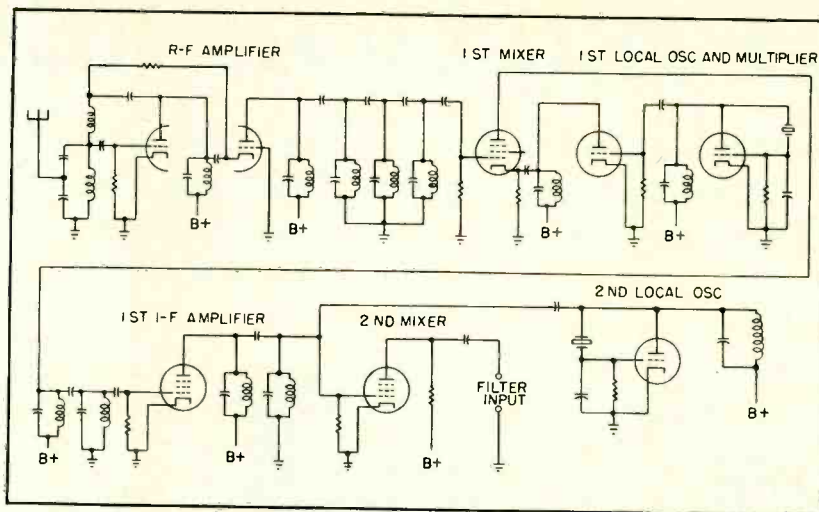


FIG. 5—Schematic of front-end for the receiver shown in Fig. 4

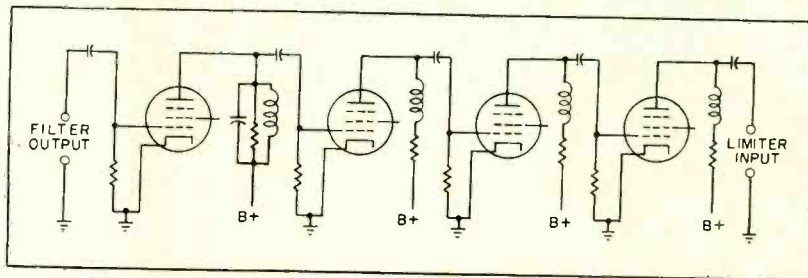


FIG. 6—Circuit of i-f amplifier

tube grid and the second tube grid should be approximately three, assuming that the same amount of noise is generated by both tubes. In this way the second tube will add only approximately five percent to the noise voltage of the first tube because the resultant noise is the square root of the sum of the squares of the voltages. This will practically not affect the signal to noise ratio.

From the second tube on, the gain should be unity since it is better to take some slight increase in noise voltage (roughly five percent per tube) than to amplify the signal and risk desensitizing and intermodulation. If one of the front-end tubes generates more noise than the first r-f tube, the gain in front of this tube has to be adjusted upwards accordingly. The low gain requirement permits use of several under-coupled circuits, thus converting extra gain encountered in the plate circuits into additional selectivity necessary for image and other spurious rejection. This also permits limiting the radiation of the local oscillator from the antenna since the under-coupled circuits will effectively prevent the local oscillator energy from penetrating into the antenna.

The design of the mixer stage requires particular attention. Low noise and minimum of distortion to signal and oscillator voltages are required since distortion produces the second harmonic which is essential for intermodulation.

An example of a mobile communication receiver is shown in the block diagram of Fig. 4. The schematic of the front end of this receiver is presented in Fig. 5.

The antenna circuit gives a voltage step-up of about 5. The r-f amplifier consists of a twin-triode cascode circuit with four under-coupled circuits as a plate load. The cascode circuit may be used as an r-f stage in place of a pentode but its advantages are less pronounced at lower frequencies and the complications connected with its use are not always warranted.

The first mixer uses cathode injection and is designed for a minimum of distortion. The first i-f consists of two pair of double-tuned undercoupled circuits, with the

gain of the amplifier adjusted to just overcome the insertion loss of the tuned circuits. By using high-Q tuned circuits and high first-mixer gain, or possibly by using another sealed filter in place of tuned circuits, this amplifier tube can be omitted. The second mixer is conventional, to change the center frequency from 5.5 mc to the 455-kc filter frequency.

The construction of the amplifier which follows the filter is not critical. No selectivity is required, and therefore resistance-coupled stages can be used although, sometimes, single-tuned stages provide better gain and stability. The total gain required is rather high but since the frequency is low no special problems are encountered. A typical amplifier is shown in Fig. 6. This four-stage circuit operates at 455 kc with an overall gain of about 120 db.

The output portion of the re-

ceiver follows the amplifier and consists of any conventional detector, or limiter and discriminator, followed by an audio amplifier. Its design need not differ from usually used techniques, although in f-m receivers, because of the very low filter and amplifier frequency, special circuits such as a frequency counter or slave multivibrator could be used in place of the discriminator.

Conventional Receiver Performance

When the gain and the selectivity of each stage of a conventional receiver is known, curves similar to those shown in Fig. 7 can be drawn. The abscissas of this drawing show convenient points at which the signal can be measured, such as antenna input, r-f grids, mixer grid, and all grids of the following stages. The ordinates show the signal strength at various stages. The 0.5-volt signal was arbitrarily chosen as 0-db level, since this is the maximum signal which can be tolerated by most receiving-type tubes.

Curve A shows the receiver noise. It is about -110 db at the first r-f tube since noise equivalent to 1.75 microvolts on the grid was assumed to be generated by this tube. This noise is amplified by the successive stages and finally it has an amplitude sufficient to saturate the last limiter (10 volts or plus 26 db assumed). A weak 0.5-microvolt, or -120-db, desired signal (curve B) can likewise be traced through the receiver. Curve B will be essentially parallel to, and will lie above, noise curve A.

Assume a somewhat stronger signal of 500 microvolts, or -60 db, on the adjacent channel, curve C. Since the signal is off frequency, the gain of each stage for this signal will be less by the amount of selective rejection by that stage. Unfortunately, the first stages of the conventional receiver are never very selective.

Curves of Fig. 8 show the relative selectivity of an antenna stage, an r-f stage, a first i-f stage, a second i-f stage, and the total selectivity of one conventional receiver measured. Resonance of the antenna tuned circuit is generally

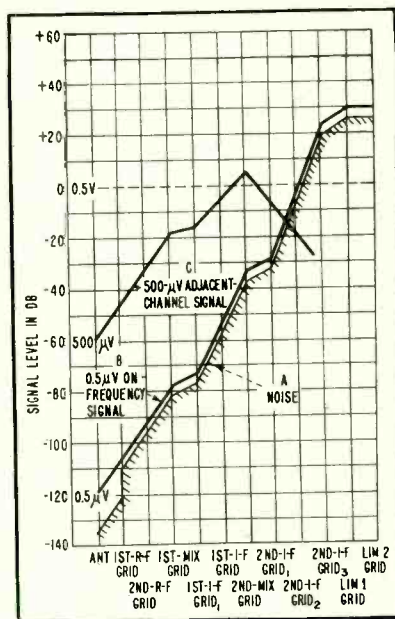


FIG. 7—Distribution of gain through conventional f-m receiver

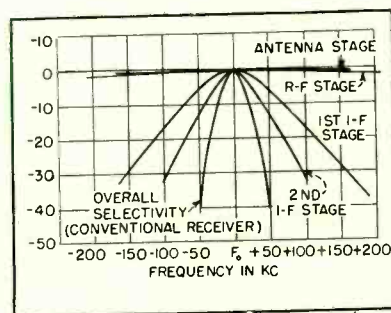


FIG. 8—Selectivity curves of a conventional receiver

very broad and the off-frequency signal will be amplified about the same amount as the on-frequency signal. Thus curve *C* of Fig. 7 runs parallel to curves *B* and *A* between the antenna and the first r-f grid. The same is true for the r-f stages if the disturbing signal is close by in frequency, and so curve *C* is practically parallel to curve *B* up to the i-f stages.

Curve *C* exceeds the zero-db level at the second mixer stage, and some serious desensitizing will occur at this stage. If the signal is on an adjacent channel, and is accompanied by another one on the next to the adjacent channel, a serious intermodulation will occur, probably at the second-mixer grid even if the signal should be weak enough not to cause desensitization. The intermodulation is very detrimental, and if stronger than the desired signal, will completely obscure it. The desensitization, if moderate, is not necessarily completely detrimental to reception as some additional gain is generally available, especially in f-m receivers and a-m receivers with agc. The most common result of moderate desensitization is deterioration in signal-to-noise ratio in f-m receivers and cross modulation in a-m receivers.

One more thing should be mentioned about receivers with distributed gain and selectivity, namely, the dependence of selectivity on the strength of the applied signal. If a receiver could receive a weak desired signal, say 0.5 microvolt, in the presence of an undesired off-frequency signal, say 60 db stronger, it may be unable to do so for desired signals of an order of 5 microvolts for two reasons. One reason is that the signal 60 db stronger than 5 microvolts may now completely desensitize the receiver to the point where one tube is biased off. The other reason in f-m receivers is that the last i-f stages, which contribute most to the selectivity, are now saturated and will not contribute to the selectivity of the receiver.

New Design Performance

The noise and signal curves for our new receiver are shown in Fig. 9. The noise (curve *A*) is ampli-

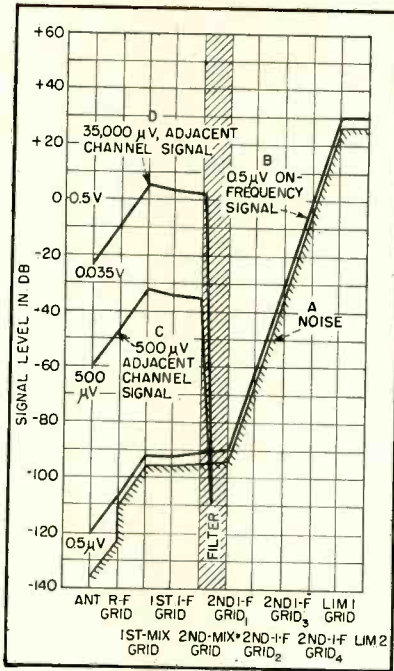


FIG. 9—Distribution of gain through new f-m receiver

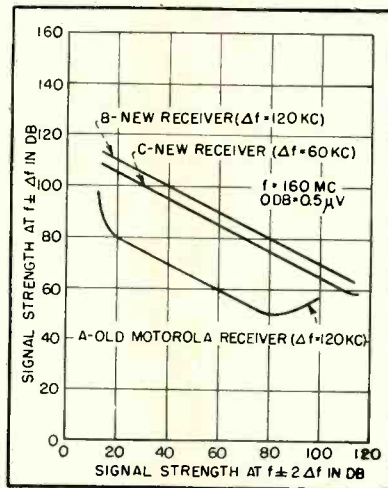


FIG. 10—Curves of intermodulation interference

fied only by the first r-f stage and is kept at this slightly higher level up to the filter. Amplification is necessary so that the noise contribution of other tubes may be insignificant. The desired signal (curve *B*) runs parallel to the noise curve. The big difference is shown in the off-frequency signal, curve *C* (as compared to curve *C*, Fig. 7). This signal is only slightly amplified in the first r-f stage, then it is slightly weakened by the following stages because they are adjusted to unity gain (for the desired signal) and have some selectivity, and finally is completely rejected by the filter (100 db or more) and drops

below the noise level before being amplified. The unwanted signal is never permitted to desensitize the receiver, and hits the first mixer grid at a relatively low level so that intermodulation, which most often takes place there, is lower than in conventional receivers. Even a much stronger signal of 35,000 microvolts (curve *D*), which would be ordinarily completely detrimental, barely exceeds the desensitizing level at the mixer grid.

The intermodulation curves show marked improvement despite the fact that no special means of improving linearity and decreasing intermodulation were used. Intermodulation curves of the first new receivers are shown in Fig. 10. Curve *B* is for signals 120 kc and 240 kc away at 160 mc. Curve *A* shows the intermodulation of the old Motorola receiver for comparison. Curve *C* is for the new receiver when the separation was decreased to 60 kc and 120 kc. This curve could not be duplicated on the old receiver because of insufficient selectivity.

For all curves, the coordinates are in decibels above an arbitrary zero level. This zero level was chosen as the power of a desired signal which is just sufficient to give 20-db quieting of the receiver. In this case it was 0.5 microvolt. The ordinates give the power level of the $f \pm \Delta f$ signal and the abscissas that of the $f \pm 2\Delta f$ signal. Each curve is the locus of points for which 20-db quieting, due to intermodulation, was obtained. The curve is linear over the greater portion of its length but curves at the ends where either of the two signals reaches a certain level. This effect is due to desensitization. The level of the $f \pm \Delta f$ signal has to be relatively stronger than that of the $f \pm 2\Delta f$ signal. This is to be expected since efficient generation of the second harmonic of the $f \pm \Delta f$ is necessary for intermodulation.

Gratitude is expressed to D. E. Noble, Vice-President and Director of Research of Motorola Inc., under whose direction the project was developed, and to James Clark, who made most of the laboratory measurements and constructed a successful laboratory model.

Solenoid Motor Control

Position of idler roll, raised or lowered by continuous strip of material moving toward wind-up roll, varies the direct current flowing through a saturable reactor in thyatron motor speed control circuit

By **GEORGE M. CHUTE**

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VARIABLE speed is required when a wind-up roll as used for cloth, wire or strip metal is driven from its center shaft. For automatic control of this speed, a small solenoid may be used, with its accessory electronic unit, to furnish the speed signal to the motor-armature circuit of a Thy-Mo-Trol electronic drive.

In Fig. 1, the armature of a solenoid is moved when a dancer roll is raised or lowered by a continuous strip or web of material passing onto a wind-up roll driven by motor *M*; in this way the material is wound under constant tension. As the roll becomes larger, the motor speed must be decreased if material is received at nearly constant rate.

If the roll pulls the web faster than it is supplied, the web raises the dancer roll, withdrawing the solenoid armature; this movement increases the current in both triode sections of *V*₃ so that more voltage is produced across *R*₁. Part of this voltage is used as a speed signal for the electronic drive; it raises the grid voltage of *V*₂, increasing the voltage across *R*₅. This lowers the *V*₁ grid potential and decreases the direct current in the saturable reactor *SX*, increasing its impedance.

The a-c windings of *SX* are in a phase-shifting bridge with *R*₆, to vary the phase of the a-c voltage applied to the grid transformer *T*₂. As the direct current in *SX* decreases, thyatron tubes *A* and *B* are phased off (fired later in their half cycles of anode voltage) so that the motor armature receives

less voltage. This reduces the motor speed so that the web holds the dancer roll and the solenoid armature at a new position; the whole circuit becomes a closed-cycle system that regulates the solenoid and the motor speed to match the increasing size of the roll.

Tube *V*₃ acts as a full-wave rectifier to produce a d-c voltage across *R*₁. Although *V*₃ is a high-vacuum tube, its grid circuits include a phase-shifting network comprising *R*₄ and the solenoid coil, connected across power transformer secondary *S*₁ so as to produce out-of-phase a-c voltage across *R*₂ and *R*₃.

The solenoid acts as a variable inductance. Withdrawing the armature decreases the solenoid inductance, letting more alternating current flow through its coil.

As the solenoid armature is withdrawn, the a-c voltage across *R*₂ becomes more nearly in phase with the anode voltage of the left-hand

section of *V*₃; similarly, the a-c voltage across *R*₃ becomes more nearly in phase with the anode voltage of the right-hand triode section. This increases the plate currents of both triode sections, so that more electrons flow from the centertap of *S*₂ through *R*₁, producing a pulsing d-c voltage across *R*₁. This is filtered by capacitors (not shown) in the electronic drive to make terminal *A* of *R*₁ more positive.

As terminal *A* rises in voltage and increases the current of *V*₂, less current flows in *V*₁ and the d-c winding of *SX*, so that the thyatrons of the motor control system fire later and apply less voltage to the motor armature. The motor receives constant field current through other tubes not shown.

Top speed of the motor is set by the speed control potentiometer in the electronic drive. Even with no voltage across *R*₁, the grid voltage of *V*₂ cannot be lowered below the speed control slider potential.

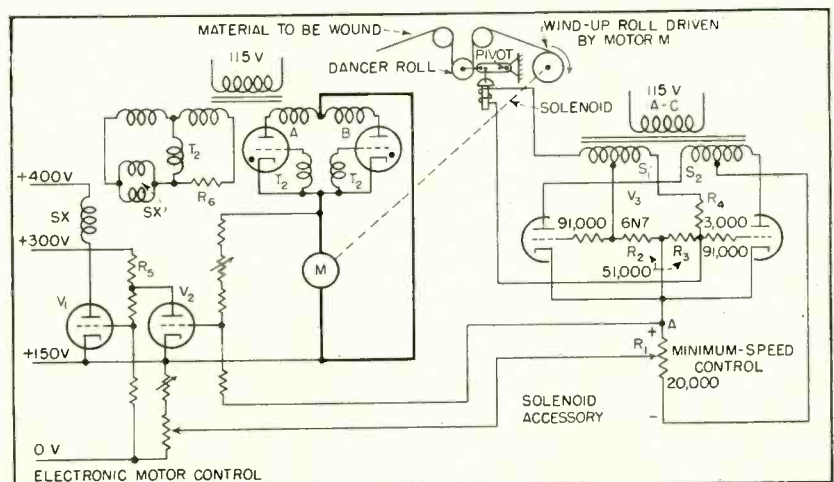


FIG. 1—Circuit of the electronic motor speed control and method of connecting solenoid attachment that is actuated by the dancer or idler roll

From a forthcoming book by the author to be published by McGraw-Hill Book Co., Inc., entitled "Electronic Motor and Welder Controls".

TELEVISION PICTURE FIDELITY

By

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WHAT IS MEANT by picture fidelity in standard home television?

The answer ought to be in the published standards on television, but a search of the IRE Standards, the RMA Standards and the ASA Standards shows only lists of factors that are said to affect picture fidelity. What it is, they don't say.

This lack of a published standard definition illustrates that picture fidelity involves something more than the simple physics of image formation, something more than the transmission system that connects the lens of the camera to the screen of the picture tube. That something more, that vital factor that standardizing committees can't agree on, is perception.

Perception opens the door to a better understanding of picture fidelity, by explaining how the television viewer, looking at his picture tube, sees what is before the lens of the distant camera.

In audio, fidelity is defined as the degree with which the output of a system accurately reproduces the essential characteristics of the input. Extending this to television, it might be said that fidelity is the degree with which the picture on the screen of the receiver accurately reproduces the essential characteristics of whatever is in the field of view of the camera.

It will simplify our thinking, to limit consideration of fidelity to

cases of live pick-up under controlled conditions, ignoring for the moment such things as spot news and sporting events, and the use of motion picture film at either end of the system.

The list of factors that the standards say affect picture fidelity is comprehensive, and includes 14 items, most of them self-explanatory. The list follows:

- (1) Number of scanning lines
- (2) Number of frames and fields per second
- (3) Percentage of time allotted to blanking
- (4) Geometric distortion
- (5) Aspect ratio
- (6) Focus
- (7) Interlace
- (8) Highlight brightness
- (9) Brightness range (contrast range)
- (10) Black level (d-c insertion)
- (11) Transfer characteristic (half-tone characteristic)
- (12) Resolution (resolving power, definition)
- (13) Electrical response (gain and phase vs. frequency, bandwidth, or transient response)
- (14) Noise and interference

To use the list, a standard test chart, a flat card with geometrical figures and gray scales, is placed before the camera. Equipment which is well adjusted in all 14 items often turn out pictures of all degrees of fidelity.

The standard list covers the physics of image formation rather completely (except for the spectral response of the camera tube, which might be added as a 15th item). However, three things that are missing from the standard list are:

- (1) Studio techniques (lighting, make-up, scenery)
- (2) Home viewing situation (size, surroundings, lighting)

- (3) Capacity of the individual observer to look at the picture and see what is not there

The key to picture fidelity is in these three missing factors. Imagine what would happen if the observer could see what really takes place on a picture tube—a flickering spot of light moving repeatedly over a flat screen, downwards at about 30 miles an hour, sideways at about 3 miles a second. If he saw that, there would be no television.

Perception Process

As a reproduction, a television picture lacks four things:

- (1) Continuity (flicker, line crawl, stroboscopic effects)
- (2) Size (not life size)
- (3) Color
- (4) Depth (distance)

These four things are the essential characteristics of the input. They are not transmitted, as such. They are contributed by the observer out of his own experience, without conscious effort, without appreciable delay. This act of contributing is a part of the process of perception. We all perceive by the same process, yet individual perceptions of a given picture or object do not always agree, because our individual experiences and skills at learning and recognizing are seldom the same.

The observer does not see the flickering spot dashing over the screen of the picture tube but he sees familiar objects (people, rooms, tables, windows), and he sees these objects in motion. He sees them as good solid objects, rounded where they should be rounded, and arrayed at different distances from him. He sees distance as a separate thing in the picture, and size as a separate thing, and illumination as a separate thing. These are his habits of vision, the facts of visual perception.

The practical consequence is that high fidelity is not automatic in television. It requires the skill and

PERCEPTION

The psychological factors which affect the excellence of a television image are here reviewed by one of television's outstanding engineers. Baldwin's classic study of the sharpness of television images, performed in 1939, freed the tv art from a servile attitude toward the equalization of vertical and horizontal resolution. In this brief paper he treats matters, not ordinarily considered by the engineers, which must be kept in mind to achieve maximum performance from a television system.

—The Editors

Consideration of the various factors involved in the physics of image formation on a television picture tube, and discussion of inherent limitations and attributes of the overall system and its production techniques

ingenuity of camera men, electricians, set designers, make-up men, sound men, and the whole production staff. At the receiver it requires favorable viewing conditions, not too much stray light, not too much image structure due to pairing or interference, not too much specular reflection from the tube face, and so on. In addition to these things that cannot be standardized, high fidelity requires a proper equipment line-up with respect to the 14 items in the list.

Consider some of the mechanical limitations of the present television system, and how these limitations interfere with picture fidelity. The most obvious limitation is that the system has, in effect, only one eye. This isn't as serious as it sounds, because binocular vision is by no means essential to the perception of depth and distance, as we shall see presently. However, when a two-eyed observer looks at a one-eye picture on a flat screen, he may receive conflicting cues to depth and distance, especially if his attention is drawn to the flat screen by line structure, or noise, or surface reflections. The next time you see a noisy picture, notice how little depth it has.

Another system limitation is in angular field of view. The natural field is about 160 degrees wide by 120 degrees high, without moving head or eyes. An image orthicon camera, with a 50-mm wide-angle lens, has a field 36 wide by 27 degrees high, and if the 135-mm medium-angle lens is used, the field is only 13.5 wide by 10 degrees high. The camera sees a great deal less than an observer in the studio. In particular, it never sees the main sources of illumination but puts them all outside the field, so that the shadows they cast may appear rather artificial and extreme.

Field of view is a limitation at the receiver, too. If you sit 4 feet away from a 10 or 12-inch receiver, the picture field is again only 13.5 wide by 10 degrees high, as com-

pared to your natural field of about 160 by 120 degrees. Your eyes adapt to the room light, not to the picture, and because you don't adapt to the picture, brightness changes in it may tend to appear rather extreme.

A final system limitation is the lack of mobility of the camera lens, both in focus and in rotation. The camera focus does not follow your line of sight the way the focus of your own eyes does. A fuzzy background in television stays fuzzy no matter how hard you look at it, quite unlike what happens in direct vision. Then again, when the camera moves, the lens moves rigidly with it, quite unlike what happens to your eyes when you move around. At slow speeds you seem to move about with the camera, but let it move a little too rapidly and you find yourself stationary while the background goes whizzing by.

These three system limitations, the use of a single lens, the restricted fields of view, and the lack of mobility in the lens, all conspire to interfere with picture fidelity by introducing conflicting cues and artificial appearances.

There are some 10 cues to depth and distance; 8 of them are monocular cues, only 2 are binocular. You are so accustomed to these 2 binocular cues that you are usually completely unaware of them. The first is double images—objects in your line of sight and remote from your point of regard always appear double if you think about them. This cue never occurs in television. The second is different images in the two eyes, a completely unconscious effect. In television this is a conflicting cue, since by means of it you may be able to see that the picture is indeed flat.

The remaining 8 cues to depth all work fine with one eye, or with one camera lens.

- (1) Overlap—near object overlaps far one. (*Life*, Jan. 16, 1950, for example.)
- (2) Motion parallax—near object moves against you, far one

moves with you. This cue results only from camera motion. There can be no motion parallax in the flat image on a picture tube.

- (3) Size—nearer object is the larger. The Zoomar lens utilizes this cue to distance. A Zoomar shot is not as realistic as an actual dolly shot because there is no motion parallax with the Zoomar.
- (4) Relative sizes of familiar objects.
- (5) Places where objects rest on the floor—the nearer the object, the lower is its resting place.
- (6) Brightness—nearer object is brighter.
- (7) Highlights and shadows—reveal contours and fine texture. Highlights and shadows are often not seen as such, but as shape and illumination separately.
- (8) Linear perspective. Man walking away actually subtends a smaller visual angle, but he is perceived as of constant size and increasing distance.

These 8 monocular cues to distance are all used by the studio technician to build fidelity into the television picture. Some, like overlap, require no skill at all. Others, like motion parallax and linear perspective, succeed in proportion to the experience and ingenuity of the studio crew. The use of highlights and shadows to create roundness and depth is an art.

The impression of distance is often enhanced by using short-focus lenses to exaggerate the perspective. An image orthicon picture, taken with a 50-mm lens, has correct perspective when viewed at only 2 times the picture height. One of the rewards of sitting further back is an increased illusion of depth in the picture.

A new definition of picture fidelity is proposed. In television, picture fidelity is the degree of perfection reached in creating the illusion of motion, the illusion of size, and the illusion of depth.

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Static Magnetic Memory

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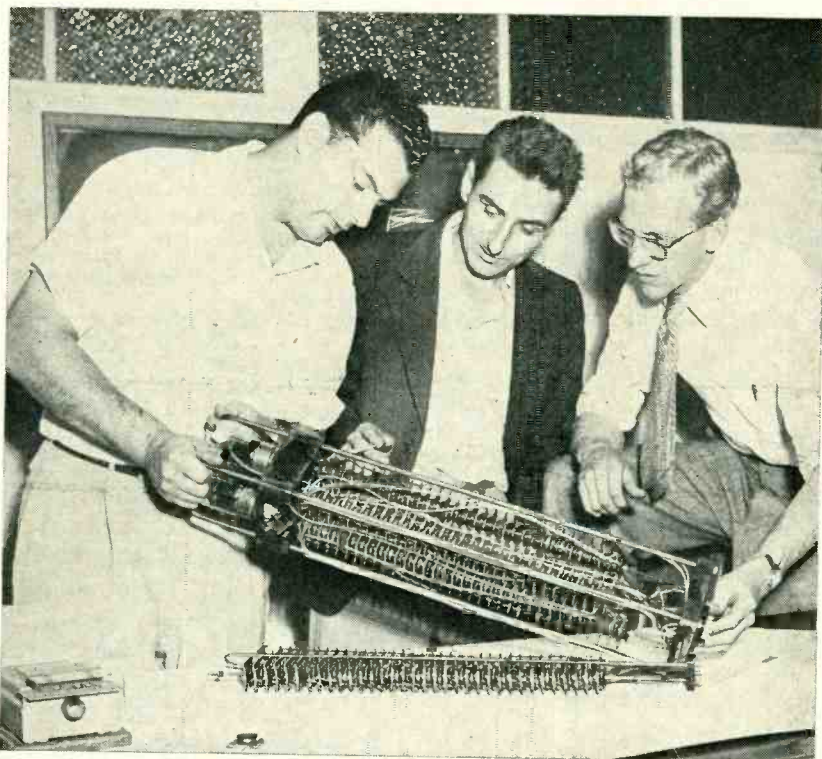
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Prototype model of a 100-core static magnetic memory unit for use in the Mark IV computer at Harvard Computation Laboratory is composed of four vertically stacked banks of magnetic cores

LARGE-SCALE digital calculating machines have made many valuable contributions to fields in which the information handled is both extensive and complex. Typical applications have involved the solution of complex engineering and mathematical problems, such as the evaluation of Fourier series, the numerical solution of differential equations, and the solution of linear systems.

The machines used in this type of large-scale information handling are characterized by high cost; in many cases, they represent expenditures of one-quarter of one

million dollars.

Progress made in this field has stimulated thinking concerning the possible application of less costly electronic computers to problems of information control and data-handling encountered in daily operation of business and industry. The high level of interest is indicated by the suggested application of computers to automatic continuous auditing, accounting and inventory systems, and automatic vending machines.

Less costly, less complex and practical machines for this type of business and industrial use certainly do not have to await ultimate

perfection of ultrahigh-speed techniques. Operating speeds of the order of 30 kc, entirely practical at the present time, are sufficiently high to make machines of this type valuable. Furthermore, many of the necessary techniques and components for the design and manufacture of machines for medium-speed business use are either now available or becoming available.

Magnetic Material

One of the newest components, called the Static Magnetic Memory, should permit substantial advances to be made in the improvement of computing machinery for business and industrial applications. The development of this device is an outgrowth of a discovery by German scientists during the last war of permanorm 5000Z, a material that has a rectangular hysteresis loop of low coercive force. A similar material known as Delta-max is now produced in this country by Allegheny Ludlum Steel Corp. Howard Aiken of the Harvard Computation Laboratory foresaw the possible use of such a material, because of its two stable-state characteristics, as a means of information storage in large scale digital computers. His basic idea has been implemented and carried out during the past two years by the work of Dr. An Wang and Dr. Way Dong Woo.

The device provides permanent information storage comparable to magnetic drum storage, but independent of mechanical mechanisms. A variable information handling rate is available ranging from zero to 30,000 pulses per second, with probable future increases in the present upper limit. Pulse storage is provided without

for Low-Cost Computers

Magnetic material having a rectangular hysteresis loop provides information storage independent of mechanisms, variable data-handling rate up to 30,000 pps and pulse storage without power. Aids in design of computing machines for business use

power being required.

The static magnetic memory operates essentially as a magnetic trigger pair, which requires no vacuum tubes to maintain position. The trigger-pair action depends on the state of the core material being represented by a point at either the top or bottom of the hysteresis loop, as in Fig. 1. This necessitates the use of a core material whose hysteresis characteristics approximate the ideal square loop, shown in Fig. 1.

Hysteresis Curve

The hysteresis curve of Deltamax, Fig. 2, shows that this material is quite suitable for this application, due to the rectangularity of its loop. Because of the flat top and bottom of the loop, once the core is saturated in a given direction, further application of current produces no further change in flux, and therefore will not produce any pulses in the output winding of the core. However, the first current pulse of an opposite polarity that occurs will cause an extremely large change in flux, thereby producing a pulse in

the output winding. The presence or absence of a pulse is thus determined by the previous history of the iron core.

With several cores connected as in Fig. 3, the state of the preceding core can be transferred from that core to the next, provided suitable rectifiers are added to the basic circuit to prevent the backward flow of current. Rectifier 1 allows the current produced in the output winding of the first core to enter the input winding of the second core, and prevents any flux generated in the input winding of the second core from returning to the output winding of the first core.

Rectifier 2 allows all current provided by the output winding of the first core to enter the second core and provides a path for the current from input winding of the second core to be dissipated in the resistor instead of upsetting the first core. By alternately pulsing the advance windings of even and odd-numbered cores the state of any core relative to the hysteresis loop (Fig. 1) may be transferred to the succeeding core. Typical pulse patterns of this operation are shown in Fig. 4.

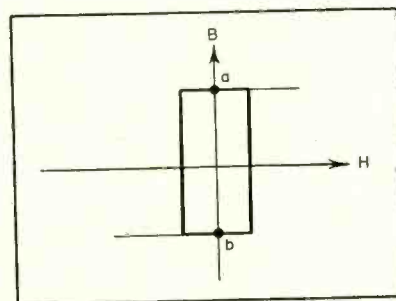


FIG. 1—Ideal hysteresis loop

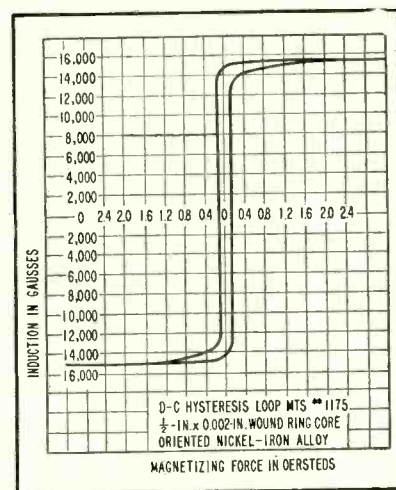
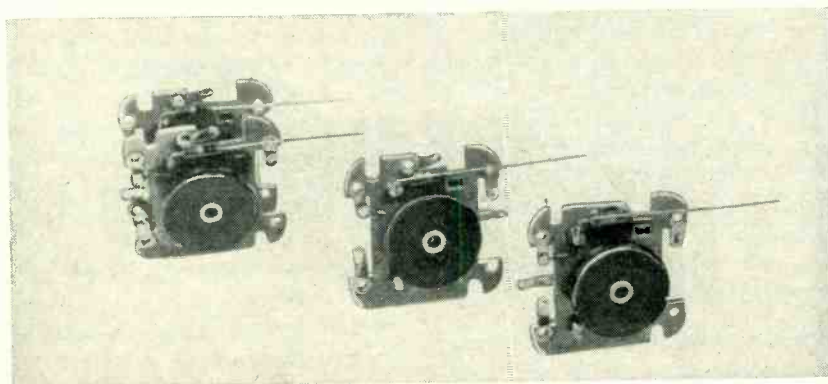


FIG. 2—Hysteresis loop of Deltamax core material



Single magnetic cores are shown in the center and at the right, at left is a pair of cores. The hollow rivets permit stacking

Magnetic tape, magnetic drums, acoustic delay lines and other devices all accomplish a similar storage function. In this device, after information has been once stored, the cessation of power leaves the stored information unaffected. Furthermore, signal regeneration is unnecessary, for the device can continually store and circulate the pulses without attenuation. Fundamentally, the static magnetic memory differs from functionally similar devices in that it accomplishes pulse storage by electrical means without

employing complex vacuum-tube circuits, in a manner completely independent of the mechanical operation found in some of the other storage devices.

The static magnetic memory device has already proved useful as a means of storing information, as a means of transferring information

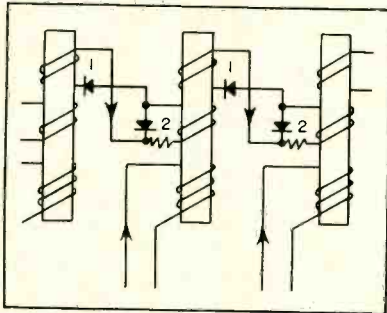


FIG. 3—Delay-line circuit of two cores per digit

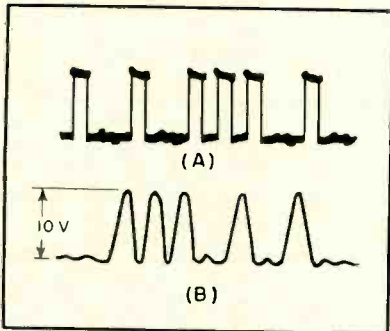


FIG. 4—Flux versus time curve in the two-core circuit. At (A), information 1010111010 is displayed at a rate of 2.5 kc. At (B), information 0011101010 is shown at 25 kc

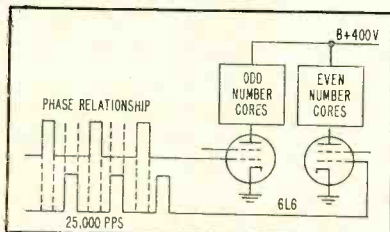


FIG. 5—Advance winding pulsing by means of tube plates. Evennumbered core advance windings are all in series

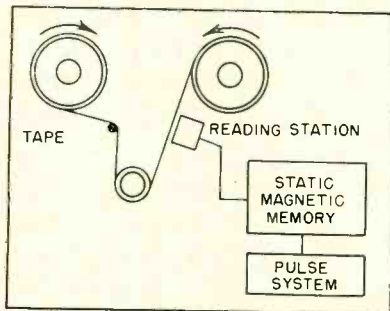


FIG. 6—Method of transferring high-speed pulses on magnetic tape to a slow-speed pulse system

between systems of different pulse rates, as a counter in which any configuration of pulses may be counted or circulated, and as a means of transferring information from serial form to parallel form, or vice versa.

Storing Information

Whenever a time delay of any length is necessary between incoming pulse information and its later use, this device can continuously cycle or dormant store the information pulses without attenuation until output is required. In its storage function it is particularly significant that the device requires no power to retain previously stored pulses.

Power interruptions or necessarily prolonged periods between input and output of pulsed commands or data thus do not impose limits on the storage function of the static magnetic memory for power is necessary only to pulse information in or out of the device.

One group is using these devices as a means of storing 16-digit decimal numbers. The number is determined by the presence or absence of a pulse. The static magnetic memory is involved in the relay circuit of a multiplier capable of obtaining a 46-digit product of two 23-digit factors. The equipment was constructed by the staff of the Computation Laboratory of Harvard University as an auxiliary to the IBM Automatic Sequence Controlled Calculator, usually known as the Mark I.

The single elements may also be assembled in such a manner that the two advancing windings are pulsed from the plates of tubes, thereby transferring the numbers in or out of a given register. A simplified schematic illustrating this arrangement is shown in Fig. 5. Any pentode type that will deliver 150 ma peak plate current will operate satisfactorily. At a lower repetition rate, however, more turns of wire may be added to each core and correspondingly smaller tubes may be used.

Systems of Different Pulse Rates

A second broad group of applications of the static magnetic memory involve its use as a transfer

medium between systems of different pulse input and output speeds. This means that the device operates essentially as a speed transformer. Pulse input speeds of the order of 25 kc in some cases might be of little value if output could not be effected at a much slower speed, as for example, to operate mechanical printing devices or telegraphic instruments. This function combined with its storing ability allows the coupling of medium-frequency pulsing systems to devices of much lower operating speeds and vice versa.

A system employing magnetic tape (Fig. 6) illustrates the value of a linking medium between systems of different pulse rates. While recording on the tape a pulse rate of 10 kc, for example, may be very desirable, yet output to typewriters, solenoids or relays is impractical at this speed. However, this process can be made entirely feasible by means of a rapid input pulsed into the static magnetic memory and pulsed out at the desired slower speed.

Conversely the same is true: a relatively slow input from punched cards or some mechanical source may be read out of the static magnetic memory at a higher speed appropriate to magnetic recording on tape. Wherever it is desirable to use a relatively high input speed to the device while a different output rate suitable for a mechanical operation is required later, (or the reverse of these conditions), this device can find many valuable applications.

Use as a Counter

The static magnetic memory provides a means of accurately recording pulses at rates up to 25,000 per second. In this application the device employs no complex vacuum-tube circuits, requires power only for circulation and none for storage of pulses, and imposes no restrictions because of inherent fragility. The unit may be applied to counting operations ranging from those using rapid electronic pulsing mechanisms to those of lower speed machine operations.

To be used in this manner the static magnetic memory uses as its input a single information pulse.

The number of advancing pulses that have been applied to the device is determined from the core location of the input pulse. For example, by using three units of 10 cores each and placing one pulse in each unit, the pulse in the first ring of 10 will operate a second ring of 10, which in turn can operate any other familiar counting device. An arrangement of this sort is shown in Fig. 7, in which an input of 25,000 pulses per second fed into a series of three units of 10 cores each operates a mechanical counting device at a rate up to 25 pulses per second.

Use of the static magnetic memory for counting purposes allows a peak counting rate of 25,000 pulses per second, in its present form. Any configuration may be cycled continuously by the device, and at this speed its value to decade counters, monitoring operations, and pulse control application in general is apparent.

Changing Information

An additional application of this device lies in its ability to change the form of input or output pulses. In certain instances, because of the particular circuit conditions involved, it is highly desirable for operation to be in either serial or parallel form. For example, large-scale digital computers utilize input information in both a serial and parallel manner. Furthermore, some means is necessary whereby the parallel output of a computer can be shifted to the serial form required if the information is to be recorded on magnetic tape. Hence the value of the device is its capability of changing input or output pulses from one form to the other.

By connecting gating circuits to every other core that makes every pulse obtainable through the unit (Fig. 8A) information may be introduced and transmitted in either a serial or parallel manner.

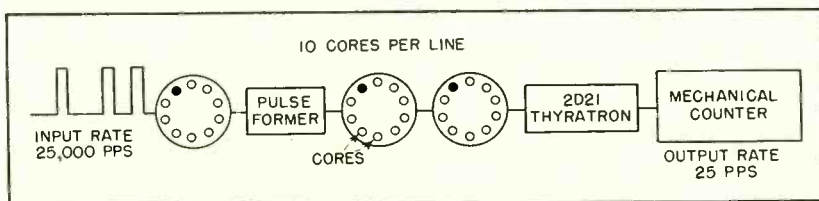
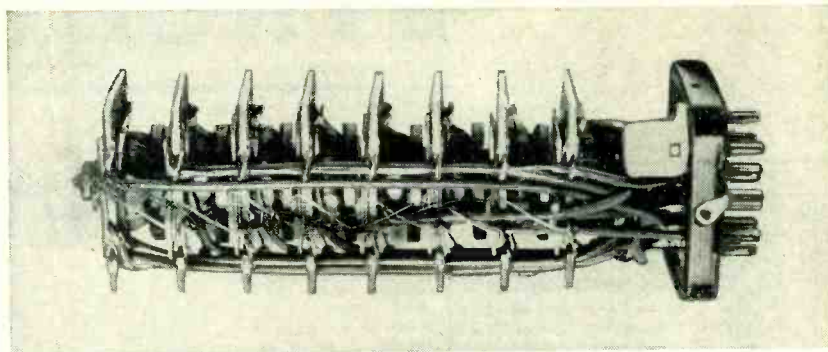


FIG. 7—Use of the magnetic memory device as a counter



Complete eight-core unit mounted on a 20-pin plug-in base

A gating circuit for this purpose is shown in Fig. 8B. Since each core can have an output of approximately 10 volts, satisfactory operation of the circuit is accomplished by using a type 6AS6 tube. By the addition of special windings to the cores of the device, the output voltage can easily be increased to a magnitude of 30 volts. This is sufficient voltage to bias and fire a typical 2D21 thyatron in a reasonably short time, and leads to relay operation such as that used in the Harvard multiplier previously mentioned.

Production

A major problem in the manufacture of this device involved the development of special techniques and

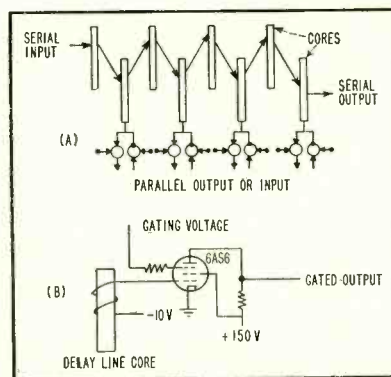


FIG. 8—Core connections for serial-parallel transformation, and delay-line output circuit for this purpose

methods for handling, processing and controlling the expensive and fragile core material. For example, difficulty was encountered in maintaining proper curvature in Delta-max strips 0.001-inch thick, so that the essential hysteretic character of the material would remain unaltered. In addition, inherent fragility of the material necessitated painstaking handling. For these reasons an almost shadowless lighting bench was designed and built, at which specialized assemblers work in rotating short periods.

Unit assembly is simplified and made rapid by the design of individual cores. A central tubular rivet in the individual unit allows them to be stacked about a central rod into lines of any feasible length, from a small 8-core unit up to 34 and 100 core banks. Adaptation to the particular circuit requirements thus has been anticipated, while ease of interconnection is provided by means of simple jumper connections between accessible solder terminals. The manufacturing design also incorporates the advantages of plug-in unit construction, by the addition of a 20-pin in base.

The authors wish to acknowledge the valuable help and co-operation given by Howard Aiken, Director of the Harvard Computation Laboratory, Harvard University, Cambridge, Mass.

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SYNCHRO DATA

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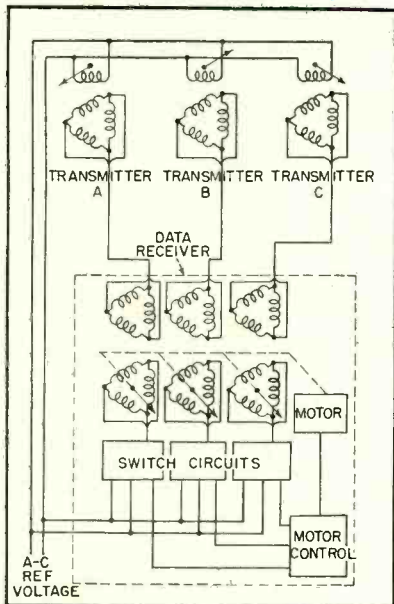


FIG. 1—Typical sampling layout for three synchro transmitters

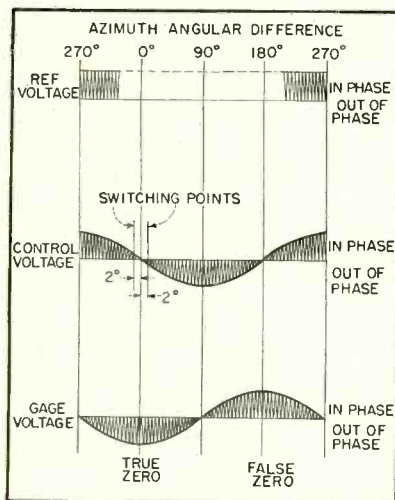


FIG. 2—Ninety-degree displacement eliminates 180-degree ambiguity

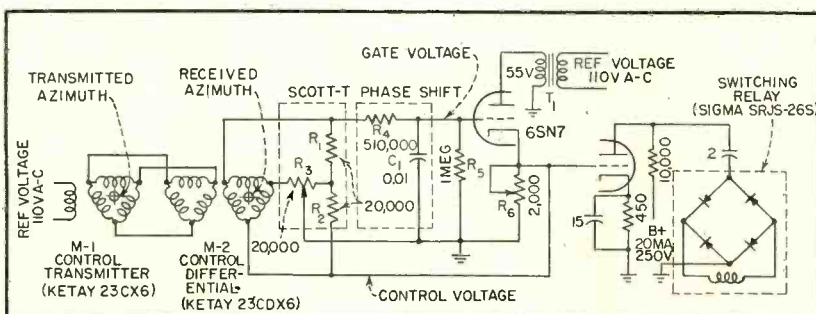


FIG. 3—Switching circuit serves a number of synchro combinations

ONE SERIOUS LIMITATION to the use of multi-synchro sampling systems for industry is the ambiguity introduced by the occurrence of null voltages at both zero and 180-degree displacements. The circuit described eliminates this 180-degree ambiguity factor, and enables a single receiving unit to sample the outputs of a number of synchro transmitters.

The receiving unit contains one synchro differential for each synchro transmitter. These synchro differentials are mechanically coupled to the shaft of a motor which rotates them from a fixed reference position in a predetermined direction and at a given speed. As each synchro differential comes within two degrees of the angular position of its corresponding synchro transmitter, to which it is coupled electrically, a single one-tube circuit operates a relay which causes the synchro data to be sampled at that point. The sampling process is repeated as each synchro differential reaches a position corresponding to its transmitter.

The circuit eliminates ambiguity by employing two synchro voltages whose amplitude envelopes are displaced 90 degrees. The amplitude of one of these voltages is used for switching when the angular difference is within two degrees of zero

or 180 degrees (which is approximately equivalent to two volts in synchro voltage); the phase of the other voltage is used to differentiate between the zero and 180-degree positions by having its phase compared to that of a reference voltage. The reference voltage is the synchro excitation voltage.

Figure 1 illustrates the switching arrangements for sampling three synchro transmitters. The motor control can be any one of a number of devices which will start and stop the motor or cause the motor to slave the synchro transmitter if an additional synchro control transformer and a servoamplifier are available. The synchro transformer is coupled and indexed in the same manner as are the synchro differentials; however, only one transformer is required for each data receiver unit.

Synchro Voltages

In order to explain how the two synchro voltages are obtained, the transfer of synchro voltage data from one synchro transmitter to the switching circuit is described. Synchro excitation is supplied to the transmitter whose output windings send data to the synchro differential. The output of the differential is connected to a Scott-T type resistor network¹ which supplies the two desired synchro voltages whose amplitude envelopes are displaced 90 degrees. It should be noted that these voltages are identical in amplitude and form, and that they reverse 180 electrical degrees in phase at each null-voltage point. If a special resolver synchro were available having a delta-wound stator and a dual-wound rotor with coils spaced 90 degrees apart, the Scott-T network would not be necessary.

The two synchro voltages have

SWITCHING CIRCUIT

One-tube circuit enables a single receiving unit to sample the outputs from a number of synchro transmitters automatically and without the ambiguity caused by the appearance of null voltages at both zero and 180-degree angular displacements

been designated as the gate voltage and control voltage and Fig. 2 illustrates the angular relationship between phase and amplitude for a revolution of the synchro transmitter with respect to its synchro differential. The choice as to which voltage is gate and which is control is completely arbitrary. It can be seen from these curves that at one null-voltage position of the control voltage, the gate voltage has maximum amplitude and is 180 electrical degrees out of phase with the reference voltage; while the other null-voltage position occurs when the gate again has maximum amplitude but is in phase with the reference voltage. Although the phase relationship illustrated is true theoretically, actually there is electrical phase shift of the excitation voltage caused by the synchros and the Scott-T network. A simple phase-shift network compensates for the shift and gives the desired phase relationship.

Switching Circuit

The switching circuit developed was designed around a single 6SN7 and a standard two-speed servo switching relay,² as shown in Fig. 3.

The first half of the tube is used to differentiate between the two null-voltage positions of the synchro transmitter. The gate voltage is fed to the grid, after the proper amount of electrical phase shift, and the reference voltage is fed to the plate through a 2-to-1 isolation transformer. When the gate voltage is in phase with the reference voltage the first half of the tube conducts, thus supplying bias to the grid of the second half of the tube by current flow through R_0 . This grid bias is sufficient to keep the second half of the tube conducting over the major portion of the time

during which the gate voltage is in phase with the reference voltage.

The control voltage is fed directly to the grid of the second half of the tube. Since only the amplitude of this voltage determines conduction, and since the gate voltage is available over a wide angle, no electrical phase shift is required on the control voltage. When the second half of the tube conducts, it energizes the relay which does the actual switching required for sampling. Switching occurs only when this relay is de-energized.

When the control voltage amplitude is less than two volts and the gate voltage is in phase with the reference voltage (this is equivalent to an angular difference of 180 ± 2 degrees), the cathode circuit of the first half of the tube supplies sufficient grid bias to keep the second half of the tube conducting. This is shown in Fig. 2 as false zero. The relay remains energized and no switching occurs.

The control voltage is again below two volts at an angular difference close to true-zero degrees. Here the gate voltage is 180 electrical degrees out of phase with the reference voltage, thus the first half of the tube cannot conduct and no bias is supplied to the second half of the tube. Since the control voltage is below two volts and no grid bias is available, the second half of the tube is cut off and the relay is de-energized. Switching occurs at this point which is the true zero.

Components

The detail component design of the circuit is based on the use of the simplest types available in order to keep the size and number of components to a minimum while obtaining reliable operation. Component values and descriptions are indicated on the circuit diagram. Re-

sistors R_1 , R_2 , and R_3 form the Scott-T resistor network for 90 degrees envelope shifting. Variable R_3 is adjusted for accurate 90-degree shift. Resistor R_4 and capacitor C_1 are used to make up for the electrical phase shift caused by the synchros and the Scott-T resistor network. A phase shift of approximately 45 degrees is required to bring the gate voltage in phase with the reference voltage.

Transformer T_1 is a standard 2-to-1 isolation transformer used to supply plate reference voltage to the first half of the 6SN7. Resistor R_5 sets the proper grid-bias voltage on the second half of the 6SN7 when the control voltage drops below two volts and the first half is conducting. The switching relay contains a full-wave dry disk rectifier and a d-c relay coil. A standard power supply capable of supplying 20 ma at 250 volts furnishes B+ voltages for each switching circuit.

Voltage and current measurements have indicated that all components are operated in their safe region. The switching circuit does not load the synchro data circuit, and the synchro wave shape has only a slight amount of distortion which will not affect the accuracy of the one-speed data used. The phase-shift network used to compensate for synchro electrical phase shift was satisfactory for the sampling method used; however, adjustment may be required if the transmission medium introduces a different amount of phase shift. The circuit is stable and not critical in adjustment or operation nor are any special components required.

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IMPROVED VERTICAL

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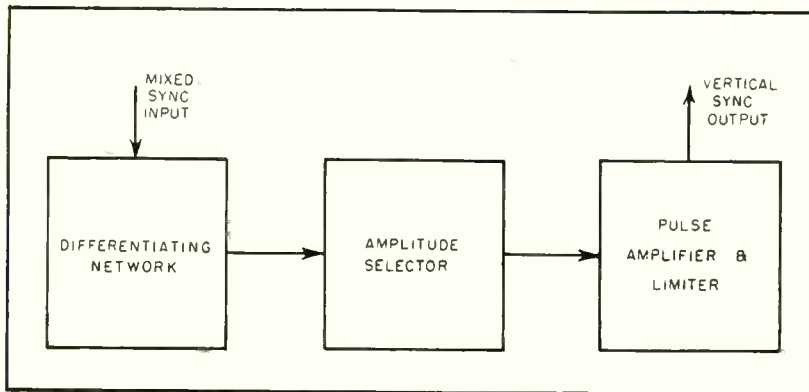


FIG. 1—Block diagram of system for producing steep-fronted pulses

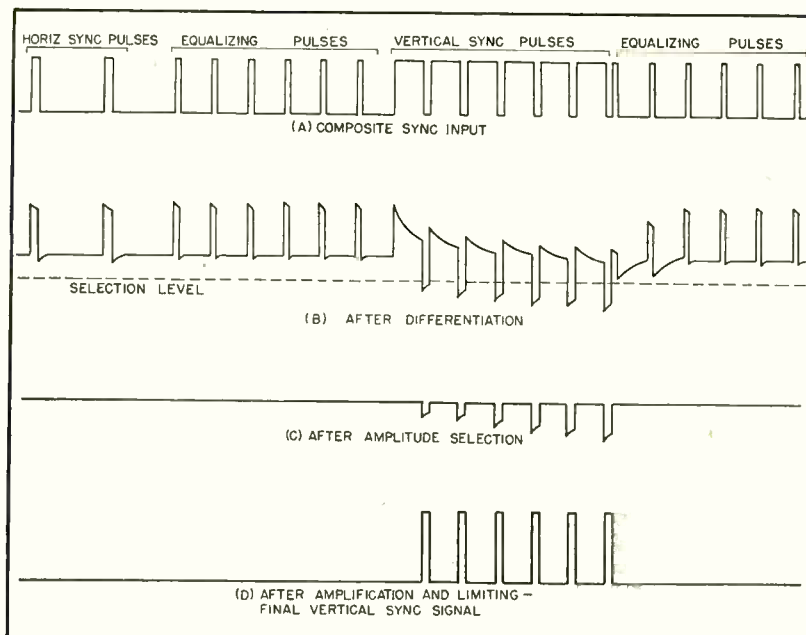


FIG. 2—Waveforms of composite sync input and changes produced by the system

Table I—Operating Characteristics

	<i>Input Pulses</i>	<i>Output Pulses</i>
Amplitude	40 v, peak	55 v, peak
Polarity	positive	positive
Rise time	0.8 μ sec	0.9 μ sec
Decay time	0.7 μ sec	1.1 μ sec
Pulse width	27 and 5 μ sec	4.8 μ sec
Pulse flatness	—	better than 2%
Keying frequency	60 cps	—
Repetition frequency	31,500 pps	31,500 pps
Number of pulses	—	6
Threshold level	—	17.5 peak sync input
Interference components on pulse baseline	—	1.5 v, p-p, approx

THE RELATIVELY POOR performance of vertical sync circuits is indicated by the difficulty often encountered in obtaining accurate and stable interlace free of drift, line pairing and the necessity for frequent and critical adjustment of television receivers.

With a few exceptions, present vertical sync circuits are essentially unchanged from those used in receivers of prewar vintage. Many of the shortcomings of these systems come about as a result of the method used for segregation of the vertical sync pulses from the composite sync signal. Almost without exception, this is performed by resistance-capacitance integration or equivalent means.

Integration with a resistance-capacitance network having a time constant suitable for complete elimination of the horizontal pulses produces a slowly rising serrated wavefront which reaches its maximum amplitude in approximately 190 microseconds. Because, with sync pulses of this shape, the triggering point of the vertical deflection oscillator is not positively determined with respect to time, stable and carefully controlled operating conditions of the latter are required if accurate interlacing is to be maintained.

Improved Rise Time

A material improvement in both vertical sync stability and interlace performance would result were the triggering pulses steep-fronted and of fairly large amplitude. Moreover, if a circuit responsive only to pulses of greater than a certain duration were placed between the sync clipper and the vertical deflection circuits, both horizontal pulses and short-duration noise pulses

SYNCHRONIZING SYSTEM

Positive interlace, freedom from line pairing and increased noise immunity without critical adjustments result from use of large-amplitude steep-fronted pulses for vertical synchronization. The pulses are derived from a simple circuit containing a germanium diode and a single triode

occurring during the field scanning interval would be rejected and the noise immunity of the entire system improved.

The circuit to be described performs the functions of pulse segregation, amplification, limiting, and sharpening, to yield a series of large-amplitude, steep-fronted pulses in rigidly controlled phase relationship to the transmitted vertical sync signal.

Theory of Operation

Figure 1 shows a block diagram of the improved sync system, while Fig. 2 indicates the significant waveforms drawn against a relative time scale.

Part A of Fig. 2 is a section of the standard sync signal at a time corresponding to the end of one interlaced field, and shows the last two horizontal sync pulses, twelve equalizing pulses and six vertical sync pulses. The approximate durations of these pulses are 5 μ sec, 2.5 μ sec and 27 μ sec respectively.

The mixed line, equalizing, and field sync pulses are applied in positive polarity to a resistance-capacitance differentiating network having a carefully chosen time constant. The network passes with negligible attenuation the leading and trailing edges of all pulses. Charge storage in the capacitor during the pulse interval, however, introduces an appreciable droop in the flat top of each pulse, and causes the trailing edge to undershoot the pulse base line. It can be shown that the amplitude of the undershoot is a function of both the width of the applied pulse and the time constant of the network.

For a single-stage resistance-capacitance network, the amplitude

of the undershoot may be expressed by:

$$E = V - \left[\frac{V}{\epsilon^{t/RC}} \right]$$

where E = amplitude of pulse undershoot, V = amplitude of applied pulse, t = width of applied pulse in μ sec, RC = time constant of network in ohms- μ f, and $\epsilon = 2.71828$, the base of natural logarithms.

For a cascaded network containing n identical stages,

$$E = V - \left[\frac{V}{(\epsilon^{t/RC})^{\frac{n(n+1)}{2}}} \right] \text{ to a close approximation}$$

The equations relate the amplitude of the pulse undershoot to that of the applied pulse, and are strictly valid only where the network is driven from a zero-impedance generator, and is terminated by an infinite impedance.

In a practical case, the source and terminating impedances may vary over wide limits. Use of a cascaded multistage network reduces the effect of variations in the former by making the output waveform less dependent upon the characteristics of the generator.

The composite sync signal is passed through a two-stage resistance-capacitance network, each stage of which, neglecting the terminating impedances, has a time constant equal to the width of one vertical sync pulse or 27 μ sec.

The effective constants of the network are then such that the undershoot amplitudes become

$$E_o = (V - 0.136V) = 0.864V \text{ for the } 27\text{-}\mu\text{sec vertical pulses, and}$$

$$E_o = (V - 0.705V) = 0.295V \text{ for the } 5\text{-}\mu\text{sec horizontal pulses}$$

where E_o is the amplitude of the undershoot developed across the

final resistive element. For convenience in terminology, these undershoots may be called inverse pulses.

The ratio of amplitudes of the inverse vertical to inverse horizontal pulses is approximately 2.9 to 1. For equalizing pulses and noise pulses of duration shorter than 5 μ sec, this amplitude ratio is increased.

Amplitude Selector

The output of the resistance-capacitance network consists of positive-going high-frequency components of the applied sync signal, together with the inverse vertical, inverse equalizing, and inverse horizontal pulses in the opposite polarity. This waveform, shown in Figure 2B, is applied to the cathode of a biased diode amplitude selector.

The cathode of the amplitude selector diode is maintained at a fixed positive potential with respect to its anode, and is nonconductive both for positive-going input signals and for negative signals of small amplitude. The positive cathode bias is adjusted to be somewhat greater than the peak amplitude of the inverse horizontal pulses. The latter, together with the inverse equalizing pulses and

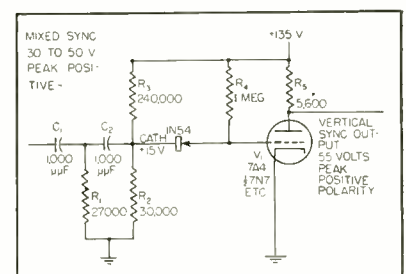


FIG. 3—Complete circuit contains a crystal diode and triode tube

any short-duration noise pulses, are therefore rejected by the diode.

During the vertical sync pulse interval, the higher amplitude inverse vertical pulses developed by the network drive the diode into conduction. As shown in Fig. 2C, a series of six steep-fronted negative pulses occurring in time coincidence with the trailing edges of the applied vertical sync pulses appear at the anode of the amplitude selector diode. These have durations approximately equal to the width of the serrations in the vertical sync block, $4.7 \mu\text{sec}$, and a recurrence rate of 31,500 pps, twice the line scanning frequency.

Pulse-Width Gate

From the above discussion, it is apparent that the combination of the R-C network and amplitude selector function as a pulse-width actuated gate, developing pulses at its output only when the input pulse duration exceeds a certain fixed value. Particularly effective pulse-width discrimination is obtained if the applied pulses are squared and amplitude stabilized, as is generally the case in a practical receiver application.

The negative-going inverse vertical pulses at the anode of the diode are applied to the input of a triode pulse amplifier, the operating conditions of which are such that pulse limiting and sharpening takes place. Because the grid is

returned through a high resistance to the plate supply, it assumes a very slightly positive potential with respect to the grounded cathode. This assures conduction of the tube in the absence of signal.

With the grid slightly above ground, a very effective clamping action takes place at the input of the pulse amplifier. The grid is prevented from being driven more positive, thus assisting materially in rejecting any positive-going high-frequency sync pulse components which may leak through the amplitude selector. At the same time, the d-c axis of the pulse is restored and held rigidly near ground potential.

Since the peak amplitude of the inverse vertical pulses applied to the pulse amplifier is more than sufficient to drive the grid to cutoff, the final inverted output pulses at the plate are squared and sharply clipped at the same level. The tube therefore acts as a limiter in both positive and negative directions.

The pulse train of Fig. 2D becomes the final vertical synchronizing signal, the amplitude of which may be made as large as desired, and the rise time of which is limited only by the bandwidth of the preceding video amplifiers and sync auxiliaries of the receiver.

Circuit Details

Figure 3 shows the complete schematic diagram of the system.

Capacitors C_1 and C_2 , together with resistors R_1 , R_2 and R_3 comprise the two-stage differentiating network. The values of these components are such that each stage of the network has the required $27\text{-}\mu\text{sec}$ time constant. Resistors R_2 and R_3 also serve as a voltage divider across the B supply, and maintain the cathode of the amplitude selector diode at a suitable positive potential.

The amplitude selector is a type 1N54 germanium diode. This type is characterized by high forward conductance together with unusually high resistance in the reverse direction, that is, with the cathode positive. Materially improved operation of the circuit is obtained with a germanium diode in this position, since the extremely low interelectrode capacitance of $1\text{-}\mu\text{f}$ greatly reduces feed-through of undesired high-frequency components existing at the output of the differentiator. In addition, the increased conductance afforded by the germanium diode provides a substantially higher pulse amplitude across the relatively low grid-cathode impedance of the pulse amplifier. This improves the limiting action of the latter at low signal levels.

The circuit constants have been selected for a supply voltage of +135 volts, and an input pulse peak amplitude of 40 volts. Inasmuch as resistors R_2 and R_3 provide a positive bias of 15 volts at the cathode of the amplitude selector diode, the circuit as a whole has a threshold of operation somewhat above this level of input sync pulse. Since upward of 30 volts are generally available at the output of the final sync amplifier, this threshold lies considerably below the video level at which a picture having satisfactory contrast is obtained.

Triode V_1 operates as a pulse limiter and sharpener, with a voltage gain of slightly over five times. The relatively low plate load resistance, 5,600 ohms, affords adequate amplifier response to pulses having rise times as short as one microsecond.

Although a substantial improvement in pulse rise time could have been effected by inductive peaking in the plate circuit, this was not considered sufficiently advantage-

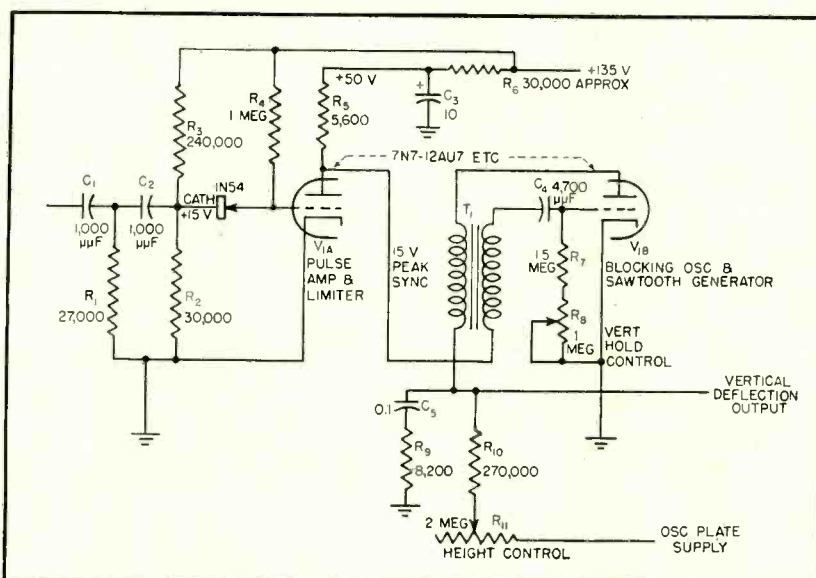


FIG. 4—Typical vertical blocking oscillator with addition of vertical sync pulse separator

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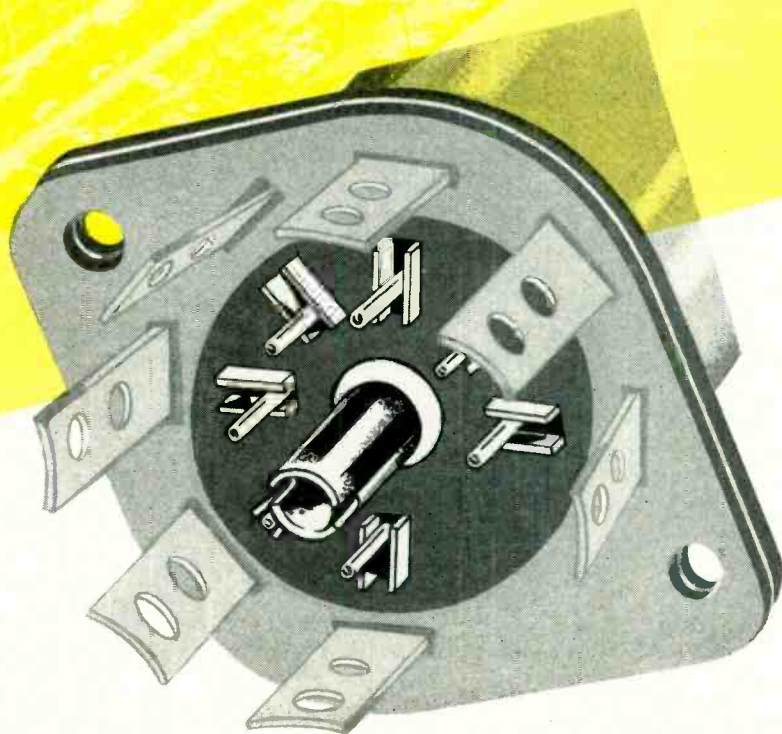
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ous to warrant the additional circuit complication.

Connection to Oscillator

Figure 4 is the schematic diagram of a typical vertical deflection circuit of the blocking-oscillator type, together with the vertical pulse separator system described. The preferred method of connection between the two is shown. The secondary of the blocking oscillator transformer T_1 is effectively a part of the plate load of V_1 , and acts to further shape the sync pulses as well as to retain their sharp leading edges.

Because the plate resistance of V_1 in parallel with its load resistance represents an effective impedance of only a few thousand ohms in series with the a-c grid return of the oscillator, including the pulse amplifier as a portion of the oscillator circuit in no way affects normal operation of the latter. Injection of sync in this manner offers the further advantage of extreme simplicity.

Sync Amplitude

The peak amplitude of vertical sync pulse developed at the plate of V_1 depends upon the effective supply voltage at the junction of R_5 and R_6 . Although a maximum of 55 volts of sync is available if R_6 were omitted, it may in some cases be found that more satisfactory operation of the blocking oscillator itself will be obtained with peak sync amplitudes of 10 or 15 volts.

The network consisting of C_3 and R_6 provides a means of adjusting the output pulse amplitude without affecting the pulse rise time; R_6 and C_3 also supply a measure of decoupling at the plate of the pulse amplifier. The time constant of this network should be long with respect to the field repetition period, and in general should be not less than 0.05 second.

With component values indicated in Fig. 4, the pulse amplifier operates at a quiescent plate voltage of 35 volts and a plate current of 2.9 ma. Under these conditions, the tube develops between 12 and 15 volts of sync pulse across the plate load, and requires but 4 volts of negative swing at the grid for complete limiting.

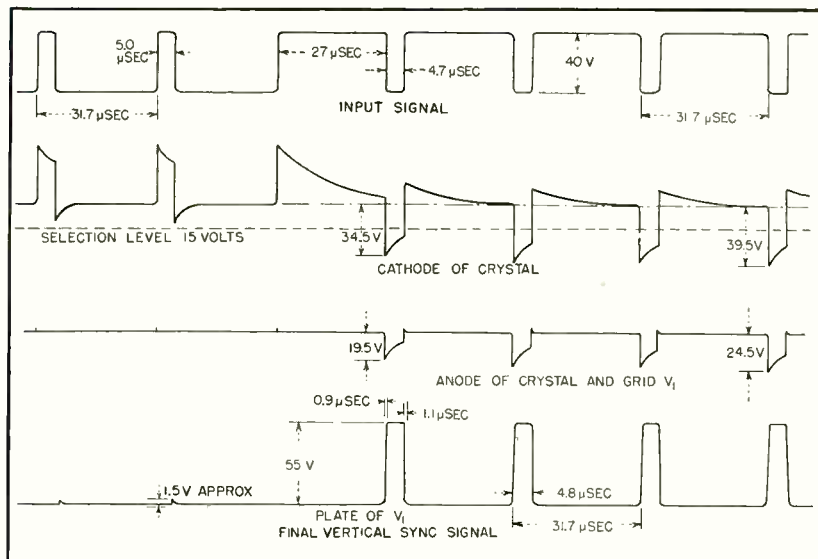


FIG. 5—Waveforms produced at designated points in the circuit

Pulse segregation with a system of this type has several additional advantages. Vertical synchronizing with pulses whose leading edges have a large time rate of change greatly minimizes interlace instability and eliminates the necessity for critical adjustment of the vertical oscillator frequency during and after warmup. The resulting accuracy of synchronizing is not nearly so dependent upon maintaining a constant amplitude of applied sync pulses as is that obtained with the usual R-C integrator system. This is because the shape of the final triggering pulse is completely independent of the input pulse amplitude over a very wide range. Rigid control of the latter is not so essential.

Integrator sync systems require that conditions before and after transmission of the broad-topped vertical sync pulses in the composite sync signal be identical for odd and even line fields. This necessitates the insertion of two groups of six equalizing pulses. Because the method of pulse segregation described does not depend upon integration, the equalizing pulses are unnecessary. This suggests that a degree of simplification could be effected in the composite sync signal.

An improvement in noise immunity in the vertical sync circuit may be realized, because short-duration noise pulses which occur during the

field scanning interval will affect the circuit in exactly the same manner as normal horizontal sync pulses and will be rejected by the amplitude selector. Such noise rejection increases the vertical sync stability of the receiver under adverse noise conditions, and virtually eliminates frame splitting and picture roll.

Operating Data

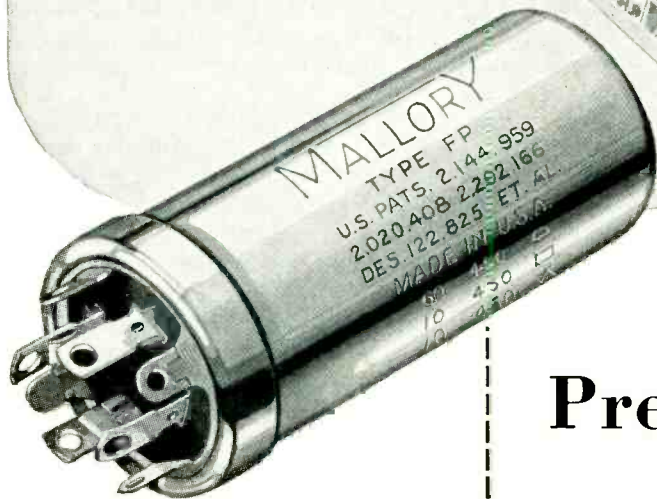
The major electrical operating characteristics of the circuit are shown in Table I. Figure 5 shows scale waveform tracings taken at significant points throughout the system. These were obtained directly from a Tektronix model 511-A wide-band oscilloscope. To permit more accurate measurements, resistor R_6 of Fig. 4 was temporarily shorted out, allowing maximum amplitude of output pulse to be developed.

All data are taken with a simulated sync signal consisting of keyed 27- μ sec and 5- μ sec pulse trains. The pulse repetition frequency and keying frequency are 31,500 pps and 60 cps respectively.

Measurements were made with a plate supply voltage of 135 volts and the total current was 10.7 ma with R_6 removed.

The author acknowledges with thanks the valuable assistance of M. C. Pease of Sylvania Electric Products Inc. in the preparation of this paper.

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Edited by VIN ZELUFF

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Stereo Television for Remote Control

BY H. R. JOHNSTON C. A. HERMANSON and H. L. HULL

*Remote Control Engineering Division
Argonne National Laboratory
Chicago, Illinois*

MANIPULATION of objects in three-dimensional space requires that depth perception be incorporated into any scheme used to view and control the means of manipulation. Ordinary two-dimensional television is not satisfactory for working with radioactive materials at a distance because the ability to judge depth is almost entirely lacking.

In the development of stereo television for the purpose a standard DuMont television pickup chain was employed. This equipment was modified so that two different lines of approach to the problem could be explored. One approach is the time-division method and the other the simultaneous method.

The time-division method used a mechanical rotating shutter and an optical system consisting of full and half-silvered mirrors. The left and right-eye images were sequentially projected onto the photo-cathode of the television camera tube. This system was abandoned because of image carryover and flicker.

In the simultaneous method finally adopted, the stereoscopic pair of images are transmitted simultaneously instead of sequentially.

This article is based on a paper presented at the 1950 National Electronics Conference. The Conference paper will appear in the Proc. NEC.

The two images are placed side by side in the same space normally occupied by a single image in standard two-dimensional television picture transmission.

Two variations of the simultaneous method have been tried. The first variation used a single lens and a beam splitter attachment at the camera. This scheme was dropped in favor of a two-lens ar-

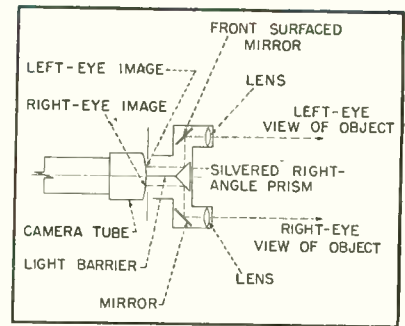


FIG. 1—Setup of the first version of the twin-lens system for the camera

angement illustrated herewith.

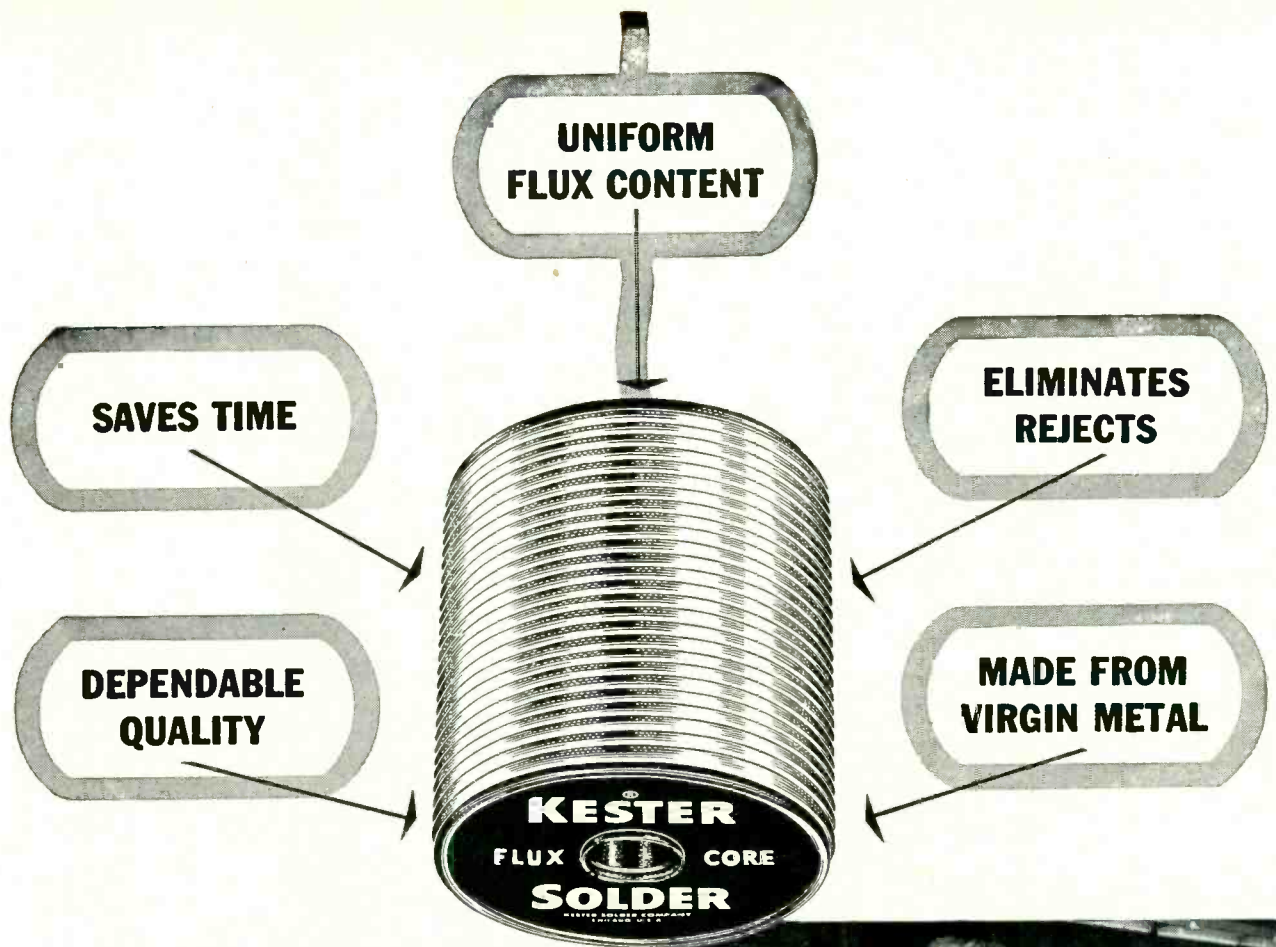
The twin-lens system was found to be superior to the beam splitter because the optical quality of the individual images was greatly improved and the image overlap in the center was reduced. Figure 1 shows a diagrammatic sketch of the twin lenses and mirrors that were used.

In the first version of the twin-lens system, two 105-mm lenses were mounted three inches between centers. The lenses were arranged so that they would be slightly rotated about a vertical axis and be converged on a nearby object.

At the receiving end of the system, the two images appear side by side on the face of a standard picture tube. The right-eye view is on the left side and the left-eye view on the right side as the observer views the face of the receiving tube. See Fig. 2. This transposition of



Single-tube stereo-television viewer monitoring the pouring of a liquid by a mechanical master-slave manipulator



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images is due to the geometry of the optics used.

Two polarizing filters whose axes of polarization are at right angles to each other are placed immediately in front of the images on the cathode-ray tube. An observer wears a pair of polarizing spectacles so oriented that the right eye is permitted to see only the right eye image and the left eye sees only the left eye image. In addition, a pair of 10-degree glass prisms are placed in front of the eyes to enable

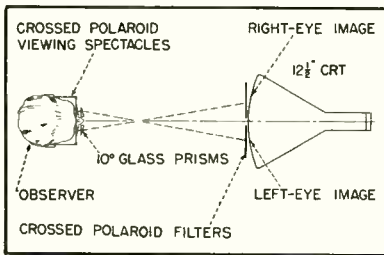


FIG. 2—Single-tube viewer for the first version of twin lens system

the observer to fuse the two pictures into a single three-dimensional image of the objects in front of the camera.

The use of glass prisms by the observer requires that his attention always be directed to the television screen since every other object in view appears double. Severe eye strain and mental discomfort result when the attention is directed to the hands in an attempt to operate switches or other devices.

A rotation of only 5 degrees of the observer's head about a horizontal axis perpendicular to the center of the viewing tube is sufficient to cause loss of stereo.

In the second twin-lens camera

arrangement, the effective distance between viewpoints is variable from five to seven inches. The mirrors were made adjustable for both distance between viewpoint and for convergence.

Another method used to view the three-dimensional television pictures makes use of two television picture tubes. These tubes are arranged at right angles to each other and a semi-transparent mirror is placed at 45 degrees to both tubes. See Fig. 3. Crossed polarizing filters are placed in front of each picture tube and the observer wears crossed polarizing spectacles. Both images of the stereo pair appear on the tubes but by means of positioning controls and masks, the right-eye picture is placed in the center of one tube and the left-eye picture in the center of the other tube. The observer is enabled to see the three-dimensional image by observing one image by transmission through the semi-transparent mirror and the second image by reflection.

The twin-tube stereo-viewer is by far the more desirable because the observer is required to use only a pair of polarizing spectacles. The super-position of the two images is accomplished by the use of the half-silvered mirror and the positioning controls of the television viewers.

Since no prisms are used, the observer may look from the viewing screen to other objects in the room such as controls and switches without danger of severe eye strain as in the first method. Also this method permits considerable translation and rotation of the head of the observer before the stereo illusion is lost. Several persons may

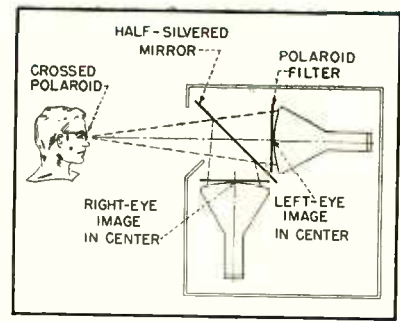


FIG. 3—Two-tube viewer has no prisms and provides best picture

easily observe the stereo image at the same time.

A considerable amount of non-linearity in the sweep circuits could be tolerated without serious impairment of the stereo-illusion. Slight differences in the sizes of the two images could be reconciled by the brain with some fatigue involved. It was found however, that appreciable vertical displacement of the images could not be tolerated.

Approximately 60 percent of the light of the image is lost in the first polarizing filters; 60 percent of the remaining light is then lost in the half-silvered mirror and another 10 percent of the light is lost in the polarizing spectacles. This results in a loss of approximately 85 percent of the total light available.

The picture tubes are 12½ inches in diameter and have aluminum-backed screens. To obtain the required increased brilliance, an accelerating voltage of 12,000 volts is applied. A well-regulated high-voltage supply is essential in the twin-tube viewer so that the size of the image does not change when brightness and contrast controls are adjusted.

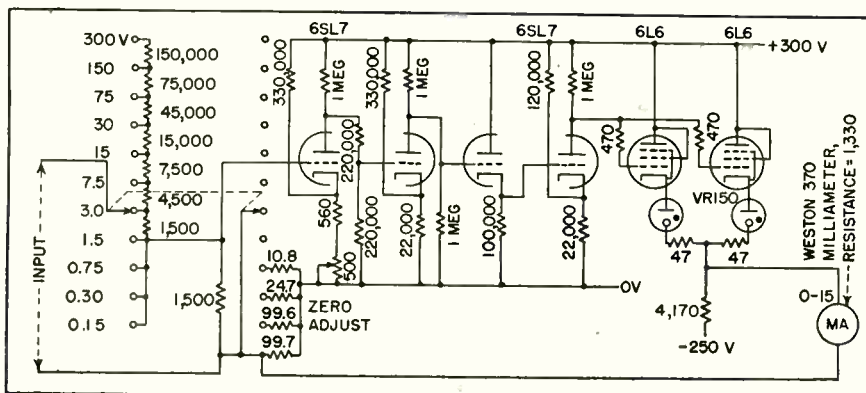
Operation of Electrodynamometer Instruments Through Amplifiers

By W. G. HOOVER

Associate Professor
Department of Electrical Engineering
Stanford University
Stanford, California

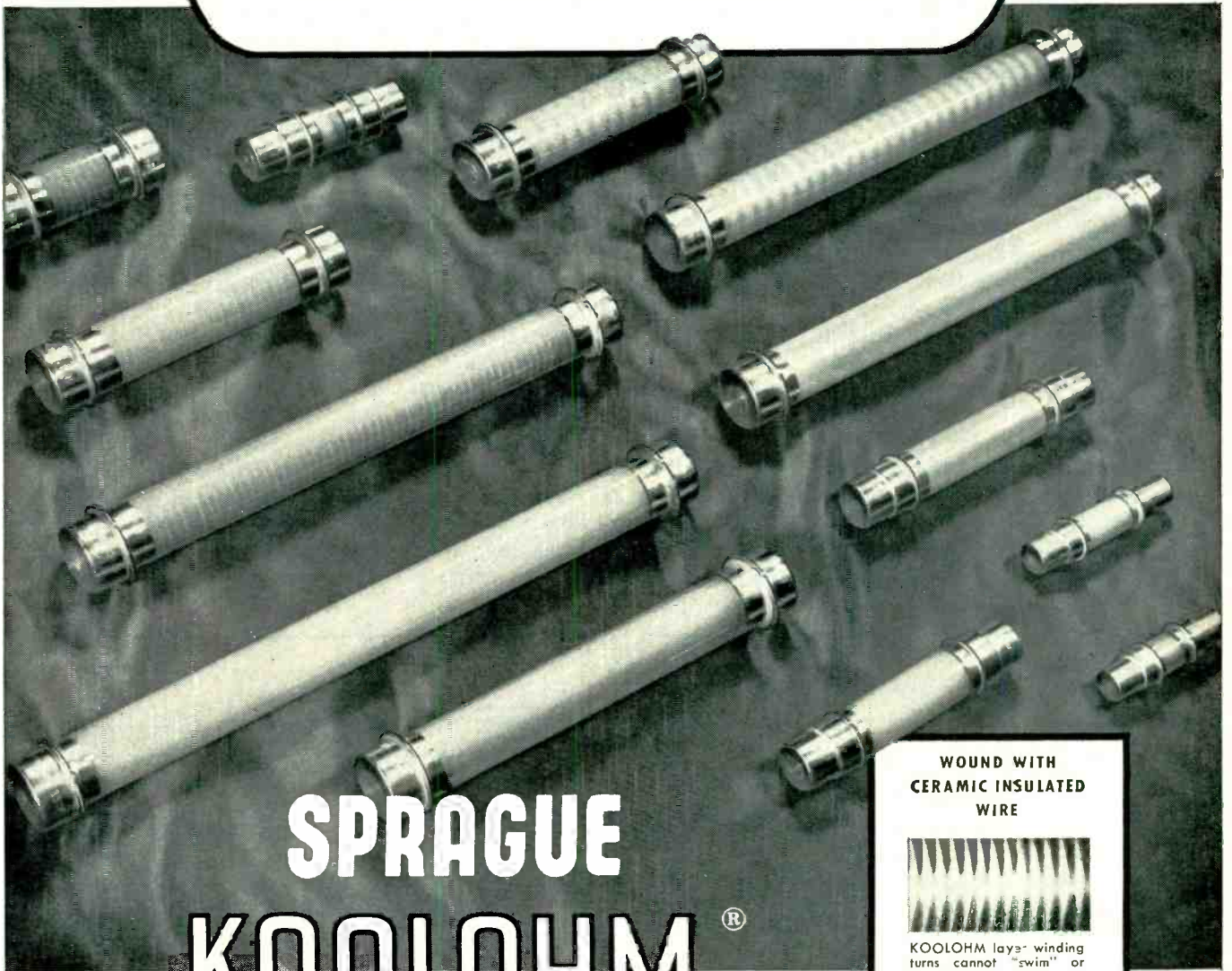
USE of direct-coupled vacuum-tube amplifiers to drive electro-dynamometer instruments is worth considering from the standpoint of sensitivity. Under proper conditions, amplifiers stabilized with large amounts of negative feedback can provide the required power with

(Continued on p 159)



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THE ELECTRON ART

Edited by JAMES D. FAHNESTOCK

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High-Definition Black-and-White Television System

A NEW high-definition system for black-and-white television has been suggested by R. B. Dome of the General Electric Company. Present monochrome receivers may receive high-definition transmissions with definition equal to that obtainable with present standards, but the addition of four tubes to the circuit will provide upward of 50 percent increase in horizontal detail. All precision equipment is located at the transmitter. The resultant pic-

ture is free from dot structure, since no sampling is employed.

The new system is based on the fact that the eye is not as susceptible to flicker in small areas as it is to flicker in large areas. The normal video band is divided into two approximately equal portions. The low-frequency portion is transmitted in regular 60-cps sequence, as in present-day monochrome transmissions, but the upper section of the video band is used only on

odd fields for the transmission of picture detail normally transmitted by present transmitters on both odd and even fields. The superhigh video band of frequencies added by the new system is transposed in frequency to fit the upper section which can be radiated and is transmitted on *even* fields. This represents an increase in horizontal resolution from the present 350 lines to 525 lines.

The block diagram of Fig. 1 shows the transmitter for generating the required signal. The camera output passes through three filters which divide the 0 to 5.3-mc signal into three sections, 0 to 1.6, 1.0 to 3.8 and 3.44 to 5.3 mc. The low portion is continuously amplified. The middle-band amplifier is keyed on alternate fields and its output is connected in parallel with the output of the low-frequency amplifier. The high range, carrying the super-fine detail, is fed to a suitable mixer-transposer to which is also fed a continuous wave of 15,750 cycles. The difference frequency of these signals is selected by a filter that passes 1.6 to 3.44 mc—the 1.6-mc comes from the 5.3-mc end,

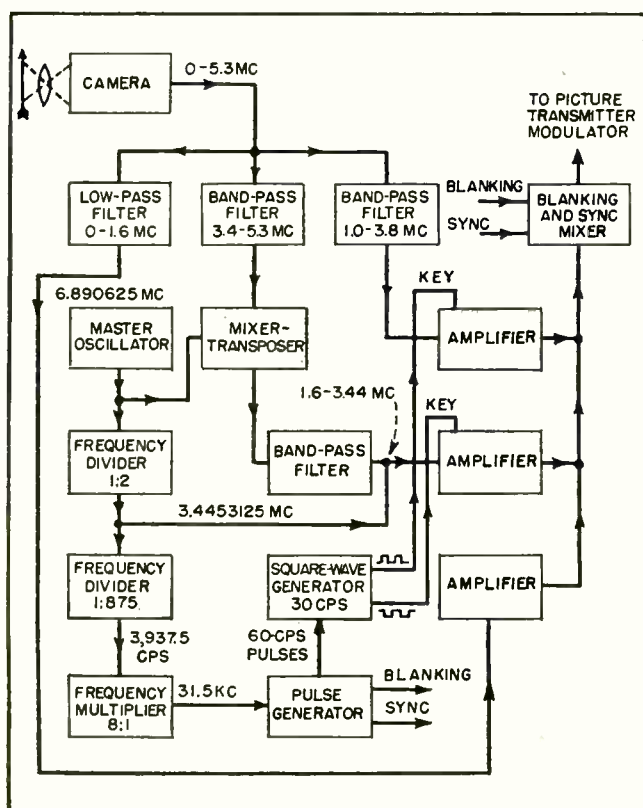


FIG. 1—Block diagram of circuits that are added to transmitter to utilize Dome system of high-definition black-and-white television

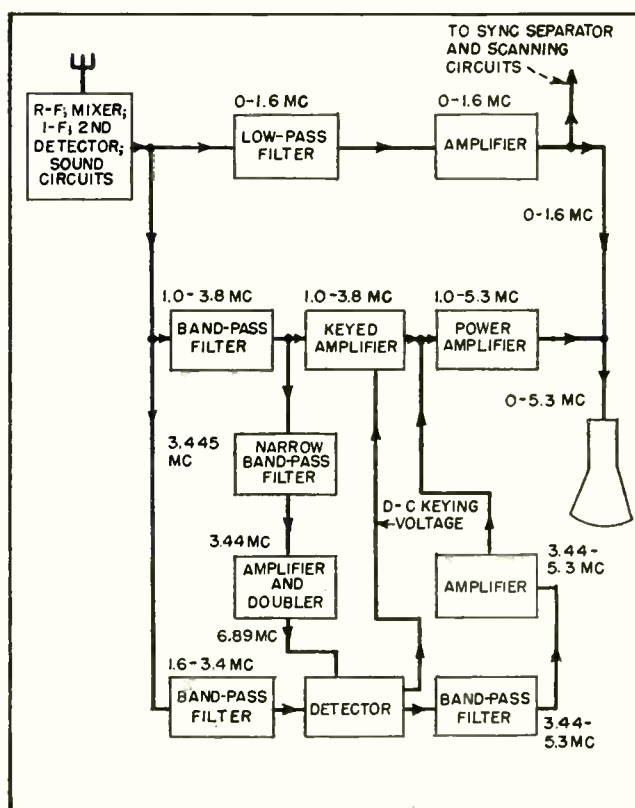
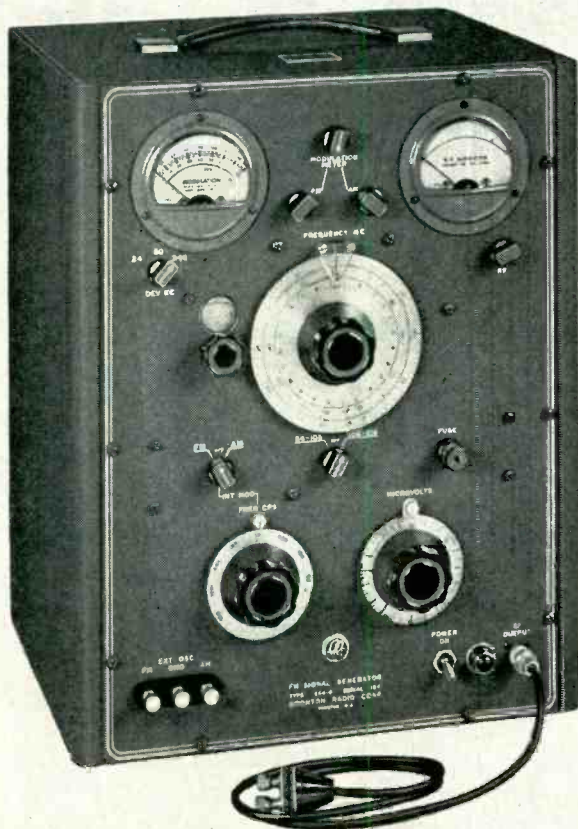


FIG. 2—Normal pictures are received by conventional receiver. Addition of four tubes increases horizontal detail by 50 percent

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while the 3.44 beat is derived from the 3.44 end beating with the 15,750 carrier. Thus inversion, as well as transposition of the super-highs has been accomplished.

At the output of the filter, a 3.4453125-mc wave is added for use at the receiver in retransposing. The 1.6 to 3.44-mc band is amplified by a third amplifier and combined by addition with the 0 to 1.6 and 1 to 3.8-mc bands. The 1.6 to 3.44-mc band is keyed on during alternate fields when the 1 to 3.8-mc amplifier is turned off. The combined signal is combined in a blanking and sync mixer to form a composite television signal which is then fed to the modulator of the conventional television transmitter.

The transmitted pulse generator chain includes a master oscillator at 6.890625 mc from which is derived the 3.4453125-mc signal and sync for a standard transmitter pulse generator. Transition keying is made during the vertical blanking period.

Receiver Circuit

The only receiver change appears in the video amplifier. A typical circuit block diagram is shown in Fig. 2. The video detector output is fed through three filters. The first passes the 0 to 1.6-mc band which is common to both odd and even fields. A second filter passes frequencies from 1 to 3.8 mc. These frequencies are keyed by an amplifier and combined with the low frequencies to feed the picture-tube gun.

A side circuit, connected at the output of the 1 to 3.8-mc filter, is tuned to the transposing frequency of 3.445 mc. This signal is amplified, doubled to 6.890625, and fed to a detector-modulator. The d-c output from this detector is fed to the keyed amplifier so that when 3.445 is present, the keyed amplifier is keyed off.

The third filter connected to the video detector passes 1.6 to 3.4 mc and this band is fed into the 6.89-mc detector-modulator. The output of this detector contains a difference band of 3.44 to 5.3 mc. This band is passed by a filter which rejects the 1.6 to 3.4-mc band and the 6.89-mc carrier and any traces of the 3.445-mc carrier which may

have passed the other filters. The output of the 3.44 to 5.3-mc filter is amplified by a video amplifier and applied in parallel to the 1 to 3.8-mc amplifier output.

The extra functions may be accomplished by the addition of four tubes, a 6AS6, 12AX7, 12AU7 and 6SF7.

The high-definition signal can be transmitted over any 4-mc channel.

Sb-Cs, Ag-Cs₂O-Cs Phototube Characteristics

SEVERAL MONTHS AGO, (August, 1950, p 132), there appeared in *Backtalk* a letter from a reader in Eastern Europe suggesting a design for a phototube containing a semitransparent Sb-Cs and a Ag-Cs₂O-Cs surface. Two engineers of the Rauland Corporation, S. Pakswar and W. O. Reed, undertook the investigation of the idea and built a model of the tube as suggested in the proposer's diagram which accompanied his letter. Their findings are presented in the curves and text which follows. We quote from their letter to the inventor whose name has been withheld at his own request.

"In the August issue of *ELECTRONICS* you published a letter concerning a phototube which contained a semitransparent Sb-Cs and a Ag-Cs₂O-Cs surface. We processed a tube constructed according to the drawing on page 132 (again reproduced in Fig. 1), and made measurements on it, some of which are presented in the enclosed graphs.

"In Fig. 2 are shown the current readings in the common anode lead and in the Ag-Cs₂O-Cs lead, the anode being held at + 300 volts

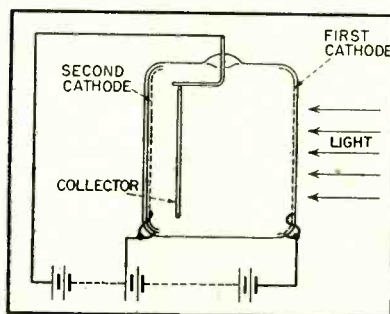


FIG. 1—Two-cathode phototube suggested by Eastern European reader in *Backtalk* letter

When used with a 2.7-mc channel, no improvement is possible under the system described, but it is possible to add some terminal equipment to transmit an apparent 3.84-mc signal over a 2.7-mc channel through the use of the system.

Tests have proved the feasibility of subdividing the video-frequency spectrum in the manner herein described.

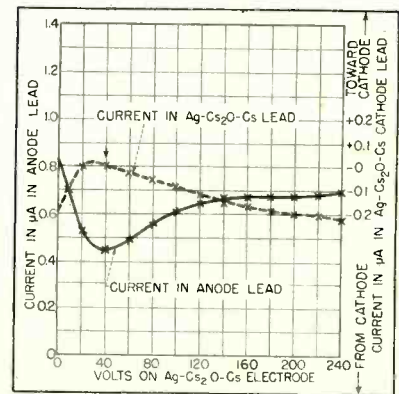
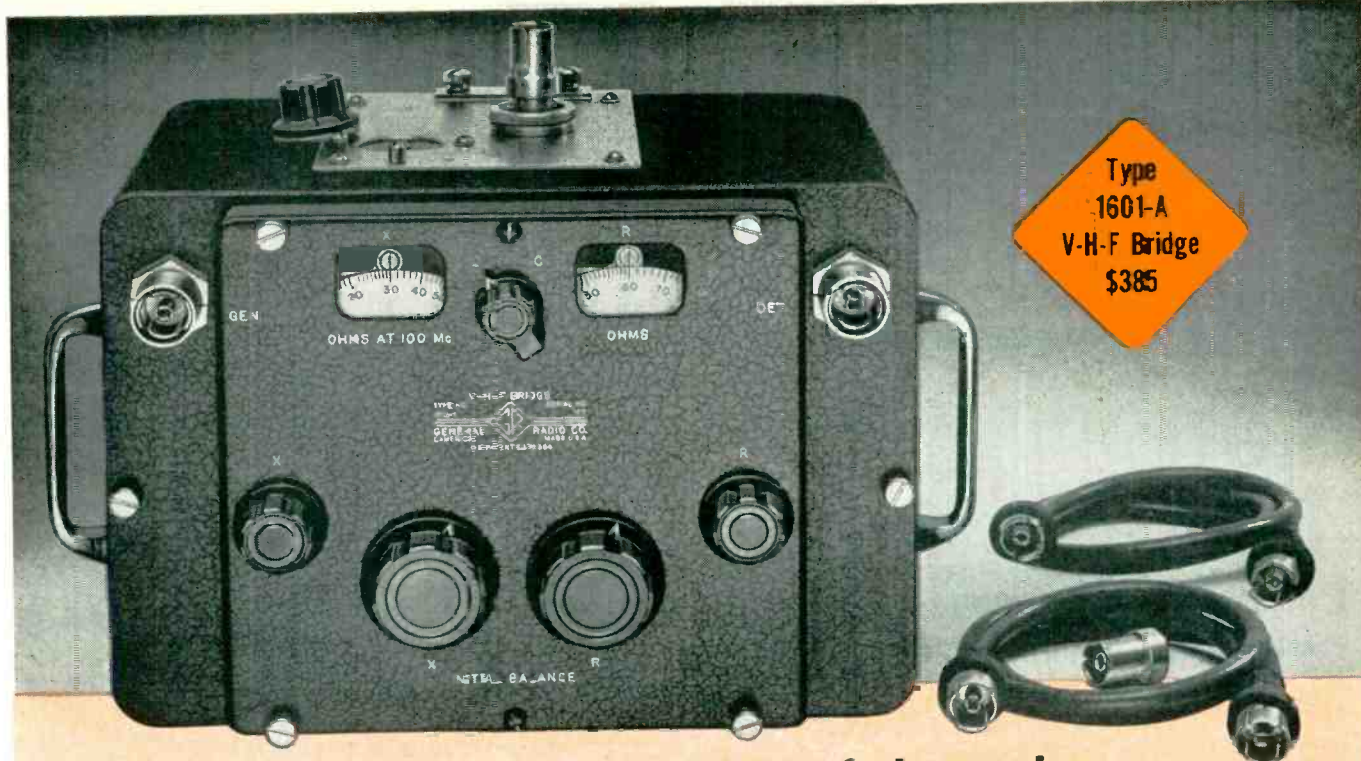


FIG. 2—Current readings in common anode lead and in Ag-Cs₂O-Cs lead of proposed combination phototube

and a variable positive potential being supplied to the second cathode. With both cathodes at the same potential the anode lead registers the combined photoemissive currents. Raising the potential at the second cathode, this cathode starts collecting some photoelectrons from the Sb-Cs surface; at still higher positive potentials the Ag-Cs₂O-Cs surface starts emitting secondary electrons and the current reverses itself. This consideration is substantiated by comparison of curves B and C in Fig. 3, which are drawn to the same scale (the other two curves being shown on other scales). Curve B had been taken with both cathodes at the same potential, curve C at a condition shown by the arrow in Fig. 2. It can be seen that the maximum in the blue green is less pronounced in curve C, corresponding to some loss of photoelectrons from the Sb-Cs surface.

"Curve D in Fig. 3 represents the response of the Sb-Cs surface alone

(Continued on page 190)



for Bridge Measurements of Impedance BETWEEN 10 AND 165 Mc

Direct-Reading Resistance Range 0 to 200 OHMS — independent of frequency except for small corrections.

Direct-Reading Reactance Range 0 to ± 230 OHMS at 100 Mc — inversely proportional to frequency.

Coaxial Adapter Supplied for Measurements on Coaxial Systems — eliminates errors from connecting leads and from residual terminal capacitance. Standing-wave ratio of unknown coaxial system unaffected by terminal capacitance of bridge.

THE new Type 1601-A V-H-F Bridge brings to the v-h-f frequencies a means for measurements of impedance of antennas, lines, networks and components, having the same accuracy and simplicity of measurement enjoyed by users of the popular G-R low-frequency Type 916-A R-F Bridge.

With this bridge the range of conventional bridge techniques is extended to 165 Mc. It is equally suited to measurements on coaxial-line systems as on lumped parameter circuits.

It is designed for direct-reading measurements of relatively low impedances, but measures high impedances indirectly and equally well.

For resistance measurements the accuracy is $\pm(2\% + 1 \Omega)$, subject to correction for inductance in the capacitor used to measure the resistance. A correction chart



The Type 1601-A V-F-H Bridge set up to measure the antenna of WCBS-TV on the Chrysler Building, New York City. The antenna consists of 16 radiating elements. Measurements of the impedance variation of an individual element over the operating frequency band as well as impedance measurements of the whole array were made easily and accurately.

is supplied with the instrument. The ohmic portion of the accuracy statement varies between 0.1 and 1.0 ohm. For reactance measurements the accuracy is $\pm(5\% + 2 \Omega)$. The ohmic uncertainty varies between 0.1 ohm at 100 Mc and 2 ohms.

This bridge is especially suited to measurements of resistors, capacitors, inductors, transmission-line networks and antennas.



GENERAL RADIO COMPANY

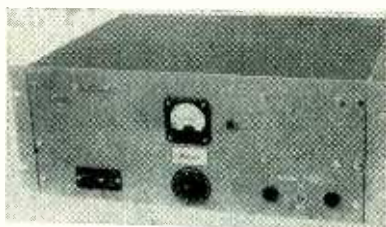
Cambridge 39,
Massachusetts

90 West St., New York 6 920 S. Michigan Ave., Chicago 5 1000 N. Seward St., Los Angeles 38

NEW PRODUCTS

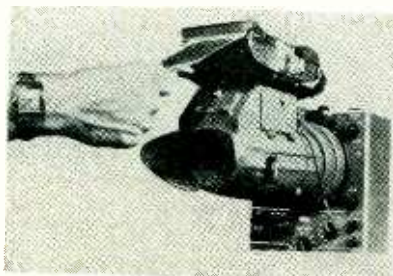
Edited by WILLIAM P. O'BRIEN

Industrial Lab Equipment Highlights New Devices . . . Wide Selection of Miniature and Weatherproof Components Will Aid Armed Forces Needs . . . Forty-Three Catalogs and Bulletins Are Offered for Engineers Mobilizing for Greater Production.



Multicoupler Amplifier

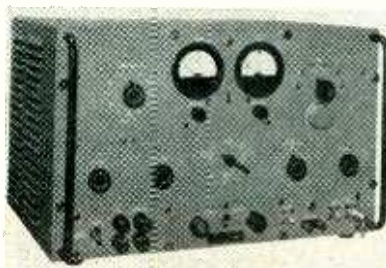
PLESSEY INTERNATIONAL LTD., Ilford, Essex, England. Type PV.14 antenna multicoupler wide-band amplifier permits the operation of up to 10 communication receivers within the 2 to 20-mc range from one common antenna system without loss of strength of individual signals or cross-modulation effects. It consists of an amplifier preceded by a high-pass filter attenuating incoming signals below 2 mc, which feeds ten cathode follower stages designed to work into 75-ohm unbalanced loads.



Oscillograph-Record Camera

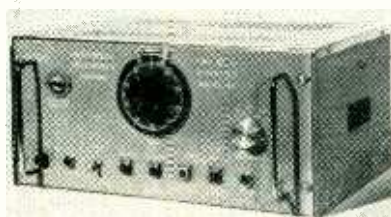
ALLEN B. DU MONT LABORATORIES, INC., 1000 Main Ave., Clifton, N. J. A new oscillograph-record camera provides, in one minute, a complete record of an oscillograph image. No darkroom facilities are required and waveform comparison is immediate. Designed specifically for application with any standard 5-in. c-r oscillograph, the camera employs the Polaroid-Land process for delivering a finished print at the termination of each completed exposure or set of exposures. Lens

aperture is f:2.8. Size of print is $2\frac{1}{4} \times 3\frac{1}{4}$ in.



Signal Generator

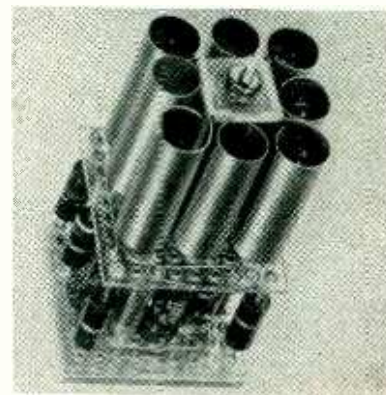
AIRCRAFT RADIO CORP., Boonton, N. J. Type H-14 signal generator was designed for complete testing of vhf airborne omnirange and localizer receivers in aircraft or on the bench. The unit has a frequency range of 108 to 118 mc. Its r-f output for ramp checks is 1 volt into a 52-ohm line and for bench checks, 0 to 10,000 μ v. Also available is an a-f output for bench maintenance and trouble shooting. Price is \$885.



Time Delay Generator

THE RUTHERFORD ELECTRONICS Co., 3724 $\frac{1}{2}$ So. Robertson Blvd., Culver City, Calif. Model A2 time delay generator will produce variable time delays ranging from 0.4 μ sec to 100,000 μ sec. Five delay ranges are provided, giving a full scale reading of 10 μ sec on the lowest range and progressing by decade steps to the highest range. The

blocking oscillator output pulse is 0.5 μ sec wide. The multivibrator output pulse width is designed to permit easy viewing on a synchroscope and is a function of the delay range in use.



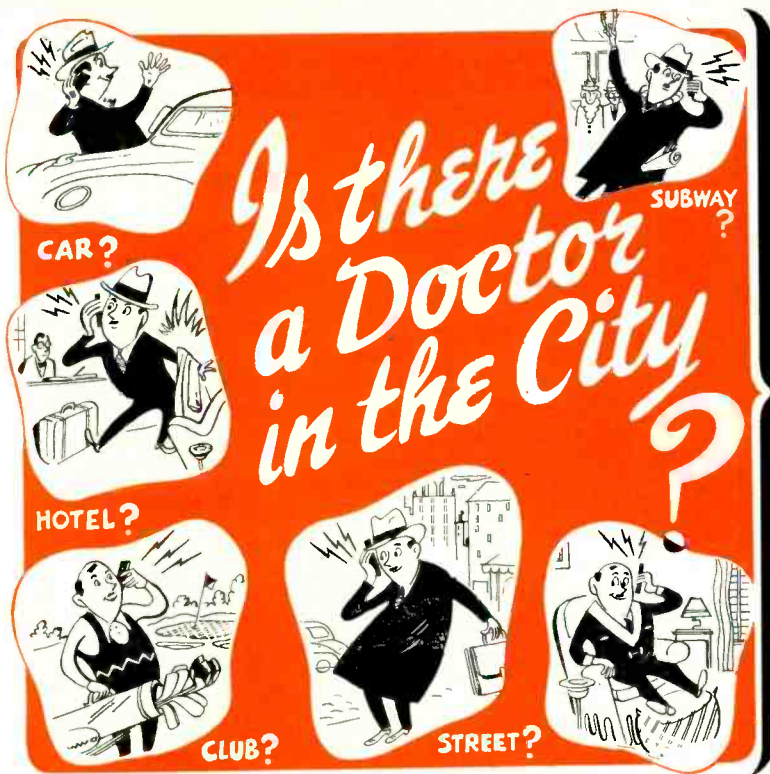
Universal Chassis

AVION INSTRUMENT CORP., 121 E. 24th St., New York 10, N. Y., has designed a universal electronic chassis for use in servomechanisms, pulse and flip-flop circuits, analog computers and similar devices. Up to eight subminiature tubes can be mounted and wired. The complete assembly mounts in a metal case filled with a special potting compound which provides mechanical support for the components, ample heat dissipation and protection from tropical or arctic conditions. The chassis is designed to operate in temperatures ranging from -50 C to $+80$ C. It meets specification An-E-19 with respect to condition of altitude, humidity and vibration.



Insulating Devices

TEFLON PRODUCTS DIVISION, UNITED STATES GASKET CO., P.O. Box 93,



TELANSERPHONE'S
 "AIRCALL" FINDS
 HIM QUICKLY, SURELY,
 DEPENDABLY
 THANKS TO THESE



SUBMINIATURE
 TUBES



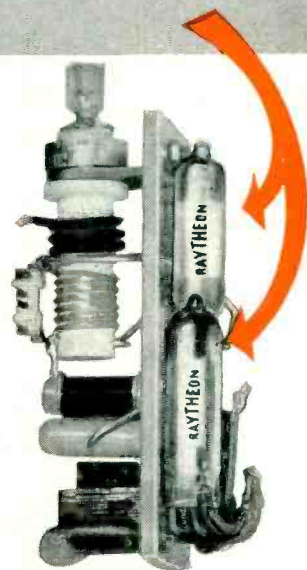
This ingenious little device puts the finger on the "doctor, lawyer or merchant chief" wherever he may be, indoors or out, within a twenty-five mile radius. He simply presses the button, holds the "Aircall" to his ear for a moment while it gives off broadcast call numbers, headed and terminated by call letters in a different voice. If his number comes up he simply calls the Telanserphone office from the nearest phone and is given the message. In this way he is never missing—never out of touch with his office, hospital, home or what not. Will electronic wonders never cease!

Raytheon
 Subminiature
 Tubes

have exactly what it takes for applications such as this. They're rugged, long lasting, generally more dependable and efficient than their large tube counterparts.

Raytheon Subminiatures fit standard sockets or can be soldered or welded into the circuit.

Raytheon Subminiatures are standard the world over—more in use than all other makes combined.



Excellence in Electronics

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SUBMINIATURE TUBES
 GERMANIUM DIODES
 and TRIODES
 RUGGED COUNTER TUBES
 RUGGED, LONG LIFE TUBES

This chart gives you at a glance the characteristics of representative Raytheon Subminiature Tubes

Type No.	Remarks	Maximum Diameter	Maximum Length	Filament Or Heater		Mutual Conductance umhos	Power Output MW	TYPICAL OPERATING CONDITIONS				
				Volts	Ma.			Plate	Screen	Grid	Control	
HEATER CATHODE TYPES												
CK5702/CK605CX	Characteristics of 6AK5	0.400	1.5	6.3	200	5000		120	7.5	120	2.5	Rk = 200
CK5703/CK608CX	Triode, UHF Oscillator, 1/2 watt at 500 Mc	0.400	1.5	6.3	200	5000		120	9.0			Rk = 220
CK5704/CK608X	Diode, equivalent to one-half 6AL5	0.315	1.5	6.3	150			130ac	9.0			
CK5744/CK619CX	Triode, High mu.	0.400	1.5	6.3	200	4000		250	4.0			Rk = 500
CK5784	Characteristics of 6A56	0.400	1.5	6.3	200	3200		120	5.2	120	3.5	-2.0
CK5829	Similar to 6AL5	0.300x0.400	1.5	6.3	150			117ac	5.0 per section			
FILAMENT TYPES												
IAD4	Shielded RF Pentode — High Gm	0.300x0.400	1.5	1.25	100	2000		45.0	3.0	45.0	0.8	0
CK571AX	10 ma. Filament electrometer tube, I _g = 2x10 ⁻¹¹ amps.	0.285x0.400	1.5	1.25	10	1.6†		10.5	0.20			-3.0
CK573AX	Triode, high frequency output	0.300x0.400	1.5	1.25	200	2000		90.0	11.0			-4.0
CK574AX	Shielded Pentode RF Amplifier	0.290x0.390	1.25	0.625	20	37†		22.5	0.125	22.5	0.04	-0.625
CK5672	Output Pentode	0.285x0.385	1.5	1.25	50	625	60.0	67.5	2.75	67.5	1.1	-6.25
CK5676/CK556AX	Triode, UHF Oscillator for radio use	0.300x0.400	1.5	1.25	120	1600		135.0	4.0			-5.0
CK5677/CK568AX	Triode, UHF Oscillator for radio use	0.300x0.400	1.5	1.25	60	650		135.0	1.9			-6.0
CK5678/CK569AX	RF Pentode	0.300x0.400	1.5	1.25	50	1100		67.5	1.8	67.5	0.48	0
CK5697/CK570AX	Electrometer Triode Max. grid current 5x10 ⁻¹¹ amps.	0.285x0.400	1.25	0.625	20	1.5†		12	0.22			-3.0
CK5785	High voltage rectifier	0.285x0.400	1.5	1.25	15				0.1			Inverse peak 3500 volts
VOLTAGE REGULATORS												
CK5783	Voltage reference tube — like 3651	0.400	1.63			Operating voltage 85. Operating current range 1.5 to 3.5 ma.						
CK5787	Voltage regulator	0.400	2.06			Operating voltage 100. Operating current range 5 to 25 ma.						

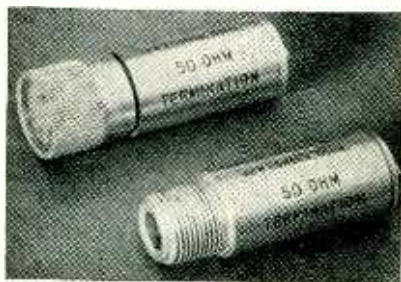
†Voltage Gain Ratio.

Camden, N. J., is now fabricating all types of Teflon insulators (spacers for coax cables, inserts for coax connectors, beads, and so on) for high-voltage, high-temperature, high or ultrahigh-frequency service in tv transmitters, radio, radar and other electrical equipment. These tetrafluoroethylene resin insulators have a power factor less than 0.0005, and a dielectric constant of 2.0 over the frequency range measured to date. Teflon is serviceable throughout a temperature range of from below -90 F to +500 F.



Magnetron

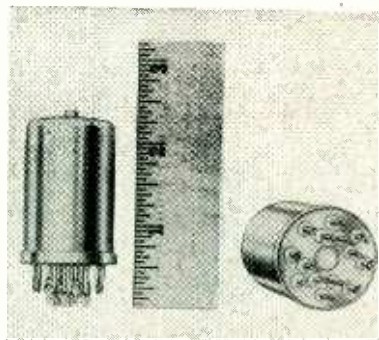
RADIO CORP. OF AMERICA, Harrison, N. J. Model 2J50 magnetron is of the internal-resonant circuit type intended for pulsed oscillator service, such as radar, at a fixed frequency of 8,825 mc. It has a maximum peak power input rating of 260 kw. When operated with a peak anode voltage of 12,000 volts, the 2J50 is capable of giving a peak power output of 45 kw at a duty factor of 0.001.



Coax Line Terminations

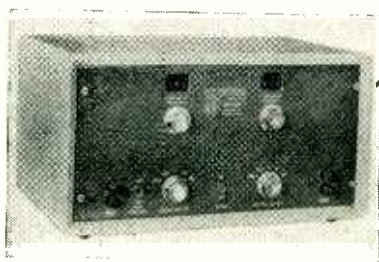
NEW LONDON INSTRUMENT CO., P.O. Box 189, New London, Conn. Illustrated above are 50-ohm termi-

nations for coaxial transmission lines featuring low standing-wave ratios from d-c to over 3,000 mc. Fittings are type N, especially designed for minimum reflections. The units are useful for testing cables, slotted lines, r-f bridges, sweep generators and random noise sources. Price is \$11.30.



Miniature Relay

THE HART MFG. CO., Hartford, Conn., has developed a new aircraft type, hermetically sealed, miniature 4-pole double-throw relay. It is built to withstand shocks up to 50 G and to operate in temperatures ranging from -65 C to +200 C. Displacing only 1.5 cu. in. and weighing but 3.5 oz sealed with a dry, inert gas, pressure filled, the new relay has variable mounting arrangements. Contact ratings are 2 amperes, 28 volts, d-c; 2 amperes, 115 volts, a-c, 400 cycles. Overload rating is 12 amperes, 28 volts, 20 seconds.



ULF Rejection Filter

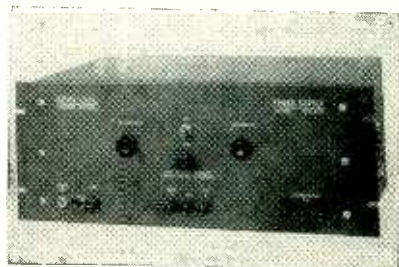
KROHN-HITE INSTRUMENT Co., 580 Massachusetts Ave., Cambridge, Mass., announces model 350-A variable ultra-low frequency rejection filter that provides either a rejection band in which the gain falls at a rate of 24 db per octave or a sharp single frequency null. High and low cutoff frequencies of the

rejection band are independently and continuously adjustable over the frequency range from 0.02 to 2,000 cps. A sharp null may be obtained at any frequency between 0.1 and 500 cps. Gain is within 3 db of unity at one octave above or below the null frequency. The unit is especially useful for vibration studies and electromedical research, for geophysical and seismological instrumentation, and in conjunction with any i-f phenomenon involving selective amplification.



Beam-Power Amplifier Tube

GENERAL ELECTRIC Co., Syracuse, N. Y. Type 6W6-GT beam-power amplifier tube is designed for use in the audio output stage of tv and radio receivers. Maximum ratings of the tube include: peak positive pulse plate voltage, 1,000 volts; peak negative pulse grid No. 1 voltage, 200 volts; plate dissipation, 10 watts. Heater voltage, a-c or d-c, is 6.3 volts; heater current, 1.2 amperes.



Voltage-Regulated Power Supply

KEPCO LABORATORIES, INC., 149-14 41st Ave., Flushing, N. Y. Model 131 power supply features a high-

(Continued on p 212)

NEWS OF THE INDUSTRY

Latest Color TV Receiver

Edited by WILLIAM P. O'BRIEN

Navy Needs Technicians

CURRENT military action in Korea has resulted in a large increase in over-all activity at the Naval Air Development Center (NADC), Johnsville, Pa. The NADC is now accepting applications for engineering and other technical positions from high-grade engineering, scientific, and mechanical personnel with education, training or experience in the fields of aeronautical, mechanical, electrical or electronics engineering, physics, mathematics, biology and clinical psychology. It is also seeking engineering draftsmen and laboratory mechanics who have considerable experience in aeronautical, electrical, electronic or mechanical drafting or shop work.

Under the management control of the Bureau of Aeronautics, the NADC performs development functions in the fields of aircraft elec-

tronics, pilotless aircraft, aviation armament and research and development in aviation medicine pertaining to the centrifuge.

Positions currently available, salaries offered and experience required are as follows:

Electronics engineer, GS-13 (\$7,600-\$8,600). Development, operation and maintenance of analog computer.

Physicist, GS-13 (\$7,600-\$8,600). Magnetic detection.

Electronics engineer, GS-12 (\$6,400-\$7,400). Sonar development.

Electrical engineer, GS-12 (\$6,400-\$7,400). Design and administrative experience as applied to aircraft systems.

Physicist, GS-12 (\$6,400-\$7,400). Sonar development.

Physicist (Electronics), GS-12 (\$6,400-\$7,400). Design experience in adopting electronic methods



One of three experimental color TV receivers demonstrated by RCA in December is shown above. It contains 43 tubes, uses the latest tricolor picture tube containing about 600,000 phosphor dots for higher definition and has new red and blue phosphors for better brightness. Also demonstrated was a standard 16-inch black-and-white receiver, converted for color by inserting a tri-color picture tube, a new deflection yoke and other circuits containing 13 additional tubes. Since the RCA system is compatible, the received color pictures were shown side by side with standard black and white receivers

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PRODUCED FOR YOUR REQUIREMENTS
- by the top specialists in the ceramic field

Hi-Q

CERAMIC PLATE CAPACITORS

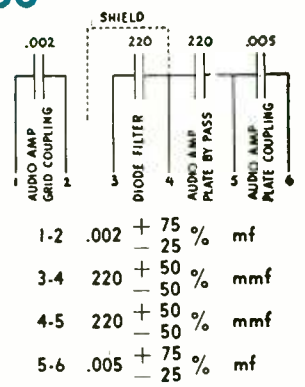
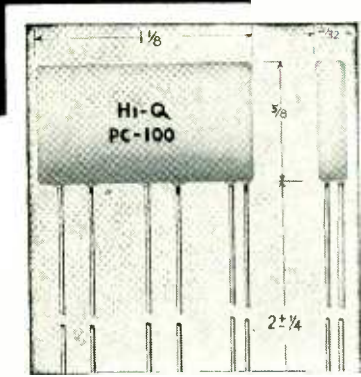
Essentially similar, except in shape, to Hi-Q Disk Capacitors except that in the multiple units they do NOT have to have a common ground as is the case with disks. These Hi-Q Plates can be produced in an unlimited range of capacities, the number on a plate being limited only by the K of the material and the physical size of the unit. They offer the greatest available capacity per unit volume of any type condenser on the market.

Guaranteed minimum values of capacity up to 33,000 mmf per sq. in. are available. This is based on the use of Body 41 ceramic having 3000 as a dielectric constant "K" and .020 in. thickness and the formula:

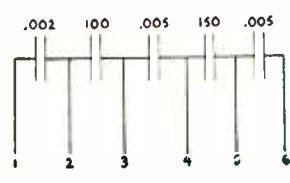
$$C \text{ (mmf)} = \frac{.224 \text{ K A (Sq. in.)}}{D \text{ in.}}$$

If temperature compensating ceramics are used, the capacity will be considerably lower. Typical circuits are shown here, but almost any combination can be produced for your specific needs. Consult our engineers for complete details. Write for new Hi-Q datalog.

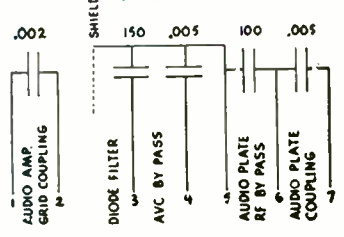
PC-100



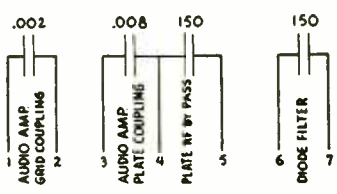
PC-101



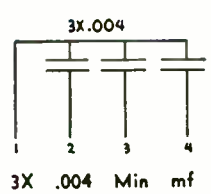
PC-102



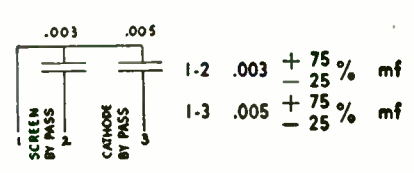
PC-103



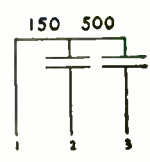
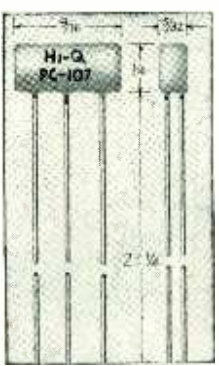
PC-104



PC-105



PC-107



Hi-Q COMPONENTS

Capacitors
 Trimmers • Choke Coils
 Wire Wound Resistors

BETTER 4 WAYS

- ✓ PRECISION
- ✓ UNIFORMITY
- ✓ DEPENDABILITY
- ✓ MINIATURIZATION

JOBBERS—ADDRESS: 740 Belleville Ave., New Bedford, Mass.



Electrical Reactance Corp.

OLEAN, N. Y.

SALES OFFICES: New York, Philadelphia
 Detroit, Chicago, Los Angeles

PLANTS: Olean, N. Y., Franklinville, N. Y.
 Jessup, Pa., Myrtle Beach, S. C.

to solving physical problems.

Physicist (Light), GS-12 (\$6,400-\$7,400). Design and development in field of light.

Electronics engineer, GS-11 (\$5,400-\$6,400). Flight control systems, antenna and specialized systems for radio-controlled aircraft and associated equipment; test and evaluation of electronic components and test equipment; radar development; aircraft or similar control devices; test and evaluation of developmental airborne search and attack equipment.

Physicist, GS-11 (\$5,400-\$6,400). Sonar development; radar development; electronic option in test and evaluation of developmental airborne search and attack equipment.

Electronics engineer, GS-9 (\$4,600-\$5,350). Installation of radio telemetering gear in pilotless aircraft, design or selection of special components and establishment of data-reduction calibrations; countermeasures equipment; radar development; missile guidance control.

Physicist, GS-9 (\$4,600-\$5,350). Optics.

Inquiry regarding the above positions should be made by letter addressed to the Industrial Relations Officer, U. S. Naval Air Development Center, Johnsville, Pa., or by personal visit to the NADC.

First TV in Canada

THE LATE John D. Woodlock, VE2HE, former assistant director of O'Sullivan College in Montreal,

JAN. 10-12: Second High Frequency Measurements Conference, sponsored by AIEE, IRE and NBS, Hotel Statler and Dept. of Interior Auditorium, Washington, D. C.

JAN. 22-26: AIEE Winter General Meeting, Hotel Statler, New York, N. Y.

MARCH 5-9: ASTM Spring Meeting and Committee Week, Cincinnati, Ohio.

MAR. 19-22: IRE Annual Convention, Hotel Waldorf Astoria and Grand Central Palace, New York City.

APR. 30-MAY 4: SMPTE Spring

MEETINGS

Convention, Hotel Statler, New York.

MAY 23-24: Fifth National Convention, American Society for Quality Control, Hotel Cleveland, Cleveland, Ohio.

JUNE 18-22: ASTM Annual Meeting, Atlantic City, New Jersey.

JUNE 25-29: AIEE Summer General Meeting, Royal York Hotel, Toronto, Ontario, Canada.

AUG. 28-SEPT. 8: Eighteenth British National Radio Show, Earls Court, London, England.

transmitted television signals recently from his home in Iberville, Quebec, Canada, using equipment designed by J. R. Popkin-Clurman, reported in August 1950 *ELECTRONICS*. Iberville is located about 28 miles north of the American border and 32 miles from the city of Montreal.

The transmitting equipment was on the air continuously from Sept. 1 to 5 using a carrier frequency of 53.51 mc (6-meter amateur band). Standard tv receivers modified by shifting the local oscillators down from channel 2 were used for field tests.

The transmitter radiated 25 watts peak and was fed into a VEE-DX type RD-13-A rotatable array mounted 90 feet high. Effective radiated power was estimated at

250 watts. Later, propagation tests were made with an erp of 5 kw.

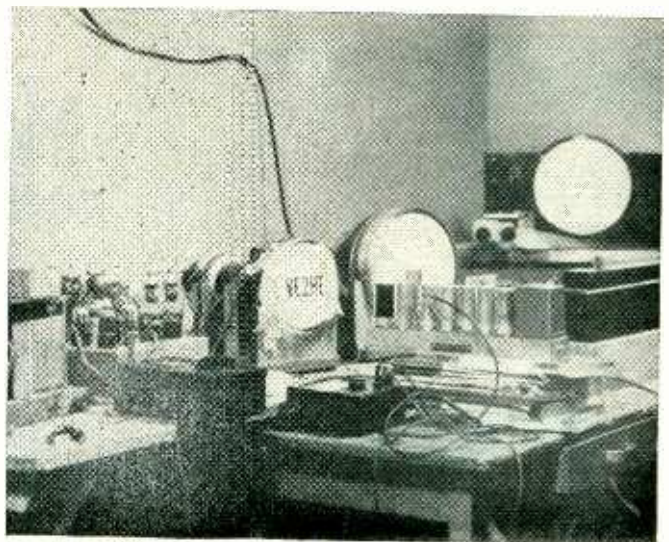
Strong signals were received at Laclede, Quebec, by VE2AMO, 21 air miles distant and at several places in the city of Montreal. The blanking bars were received at Lavaltrie, Quebec, by VE2SV, approximately 51 miles distant, with a faint picture visible.

The effective resolution of the pictures up to eight miles was better than 325 lines.

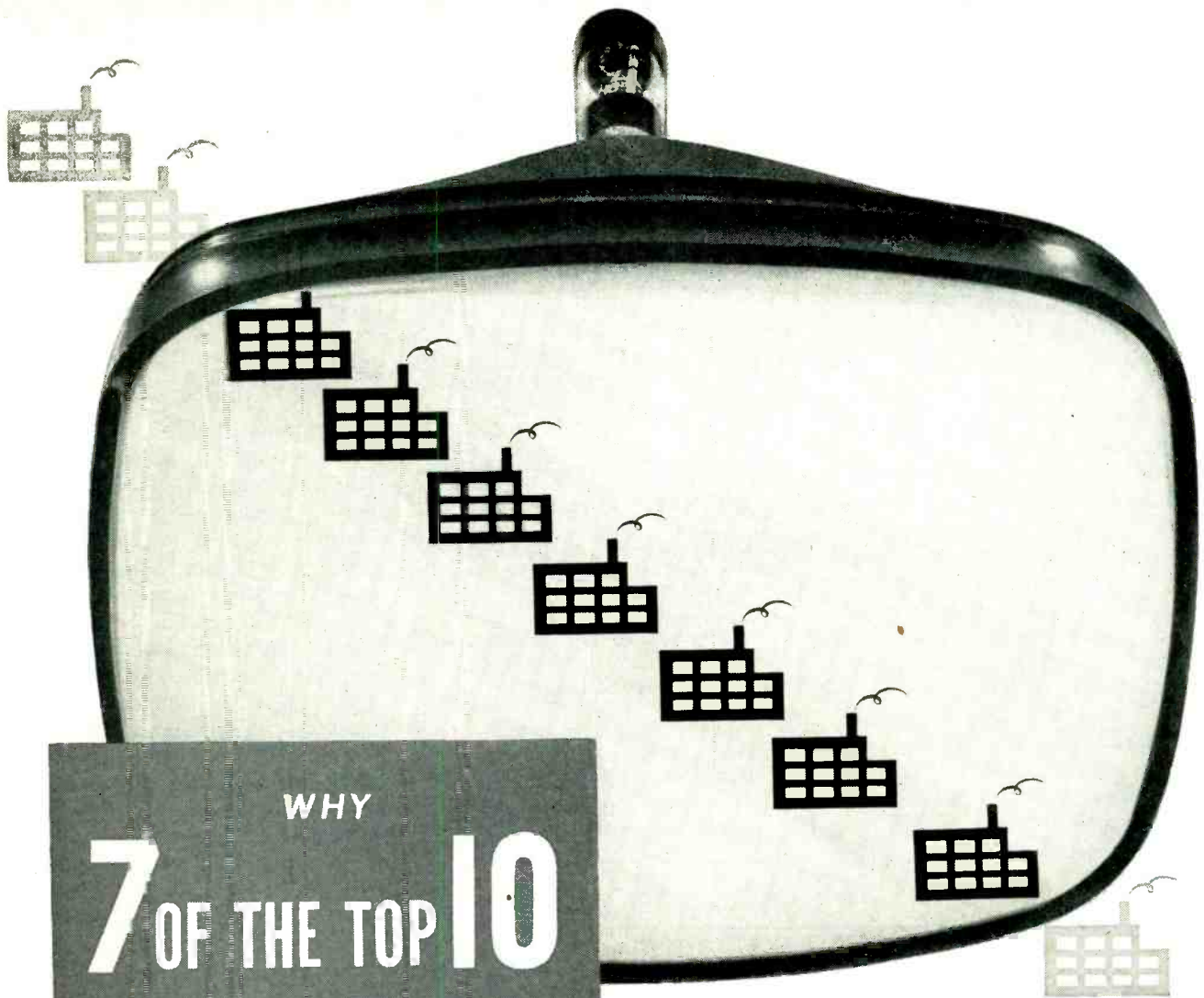
Signal Corps News

THE SIGNAL CENTER at Fort Monmouth, N. J., has over 700 vacancies for civilians who can qualify

(Continued on p 246)



Equipment used in recent amateur tv transmissions showing the r-f portion of the transmitter, monitoring set, and phototube and video amplifier chassis facing test transparency on face of the transmitting crt



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RADIO TUBES; TELEVISION PICTURE TUBES; ELECTRONIC PRODUCTS; ELECTRONIC TEST EQUIPMENT; FLUORESCENT TUBES, FIXTURES, SIGN TUBING, WIRING DEVICES; LIGHT BULBS; PHOTOLAMPS; TELEVISION SETS

NEW BOOKS

The Theory and Practice of Industrial Research

BY DAVID BENDEL HERTZ. *McGraw-Hill Engineering Management Series, McGraw-Hill Book Co., New York, 1950, 354 pages, \$5.50.*

THIS BOOK deals with the "application of the methodologies of scientific disciplines in industry" and the necessity for efficient use of the limited reservoir of creative ability. It defines research as the "application of human intelligence in a systematic manner to a problem whose solution is not immediately available". The author recommends that a research director be given the prime responsibility to attempt to solve all the problems turned over to him. He recommends a tight organization, with specific problems planned in detail in advance and preliminary estimates on what is to be done.

It is unfortunate that the author

did not use the word "development" instead of "research" because his suggestions would have been at least somewhat more applicable. However, no attempt to distinguish between basic or applied research or development is carried through the discussions. The policies which he recommends are not in accord-

RELEASED THIS MONTH

Electrons and Holes in Semiconductors; William Shockley; Van Nostrand; \$9.75.

Fundamentals of Acoustics; L. E. Kinsler and A. R. Frey; Wiley; \$6.00.

Micro-Wave Measurements; H. M. Barlow and A. L. Cullen; Macmillan; \$6.00.

Traveling Wave Tubes; J. R. Pierce; Van Nostrand; \$4.50.

TV and Other Receiving Antennas; A. B. Bailey; Rider; \$6.00.

ance with those practiced in productive research organizations where creative work is done.—
WALDO H. KLIEVER, *Director of Research, Minneapolis-Honeywell Regulator Co.*

Principles and Applications of Waveguide Transmissions

BY G. C. SOUTHWORTH, *Bell Telephone Laboratories. D. Van Nostrand Co., Inc., New York, 1950, 689 pages, \$9.50.*

THE AUTHOR of this book is internationally known as one of the pioneers in waveguide work and one of the outstanding authorities in this field. A book written by him should be expected to be, and is in fact, outstanding in many respects.

As the title of this book states, both principles and applications of waveguide transmission are discussed. Most of the emphasis is placed on the applications and this book will be invaluable to all development engineers employing or developing microwave components. Seldom in the experience of this re-

(Continued on p 140)

BACKTALK

This Department is Operated as an Open Forum Where Readers May Discuss Problems of the Electronics Industry or Comment Upon Articles that ELECTRONICS has Published

Video on Tape

DEAR SIR:

I'M AFRAID I can't quite agree with John Boyers' conclusions (see *Backtalk*, and the Editorial page of ELECTRONICS, June, 1950) that anything so plebeian as a direct approach to the problem of recording video frequencies on magnetic tape is obviously impractical. To be sure, the application of new principles to the problem is most desirable and logical, but the cost of doing the job by the "brute-force" method is not as fantastic as it may seem.

The calculation presented by Mr. Boyers is the first one everyone

makes, of course. However, the cost given (\$1,275.00 for a fifteen-minute recording) is somewhat high since, in the quantities that any large user buys tape, the net price for the material would come to about \$760.00. If the tape were used only 100 times (and re-use of the tape is one of the objectives in developing a new system), the cost per use would be only \$7.60.

At the present time, television recordings are made on 16-mm and 35-mm film. The cost of a fifteen-minute print (neglecting entirely the negative costs) is about \$15.00 and \$50.00 respectively. These films are reproduced once in the city to which they are sent and then de-

stroyed. So, even using an elementary approach to the recording problem, magnetic recording of television programs would result in a 2 to 1 saving over 16-mm costs and better than a 6 to 1 saving in 35-mm costs. When it is considered that well in excess of 200 hours (or 800 quarter-hours) of release points are used every week by each network, the potential savings are seen to be substantial. I don't think that the approach is as "obviously" impractical as Mr. Boyers concludes!

HOWARD A. CHINN
Columbia Broadcasting System, Inc.
New York, N. Y.

It Is to Laugh

DEAR SIR:

YOUR "*Cross Talk*" column in the June 1950 issue under the heading, "Landlord" illustrates perfectly the comic aspect of what passes for engineering these days. The reference to Alpine, however, while quite

(Continued on p 262)



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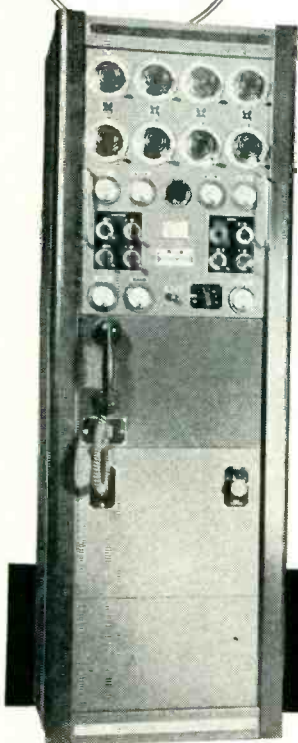
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Vol. 10. Edited by N. MARCUVITZ, Polytechnic Institute of Brooklyn. 428 pages, \$7.50

Presents in compact form all currently available theoretical data and some experimental data on the properties of microwave transmission lines, microwave circuit elements (obstacles, windows, discontinuities, bends, junctions and couplings) and of some structures, such as cavities, which may be considered as composites of these.

2. PROPAGATION OF SHORT RADIO WAVES

Vol. 13. Edited by DONALD E. KERR. Johns Hopkins University. 729 pages, \$10.00

This volume treats the phenomena associated with the propagation of short radio waves between terminal points, whether they be the radar antenna serving a dual purpose or the antennas of a communications system. Emphasizes methods of planning experiments and of analyzing results.

3. THEORY OF SERVOMECHANISMS

Vol. 25. Edited by H. M. JAMES, Purdue Univ.; N. B. NICHOLS, Taylor Instrument Co.; and R. S. PHILLIPS, Univ. of Southern Calif. 375 pages, \$5.00

4. PULSE GENERATORS

Vol. 5. G. N. GLASOE, Rensselaer Polytechnic Institute; and J. V. LEVACQZ, Johns Hopkins Univ. 737 pages, \$9.00

5. MICROWAVE RECEIVERS

Vol. 23. Edited by S. N. VAN VOORHIS, Assoc. Professor of Physics, Univ. of Rochester. 611 pages, \$8.50

6. TECHNIQUE OF MICROWAVE MEASUREMENTS

Vol. 11. Edited by C. G. Montgomery, Associate Professor of Physics, Yale University. 937 pages, \$10.00

7. VACUUM TUBE AMPLIFIERS

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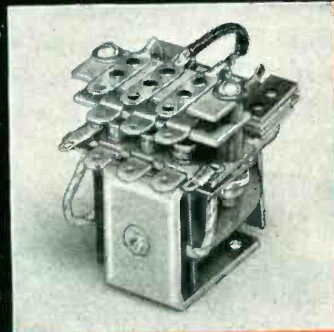
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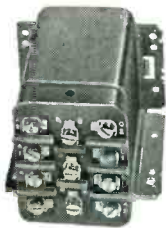
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viewer has such a coordinated picture been assembled of up-to-date developments in a particular field as this book does with regard to the work of the Bell Telephone Laboratories. In this respect this book could be compared to Volume 9 of the Radiation Laboratory Series. The fact that substantially more weight is given and space devoted to the work done within the Bell Telephone Laboratories than to the work of others was to be expected and detracts only very slightly from the value of the book.

Introductory Theory

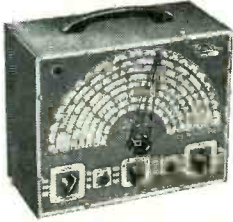
After a very interesting historical introduction, basic concepts are given on networks, transmission lines, electromagnetic waves and waveguide theory. The discussion of these principles is given in the first seven chapters, which are necessary for an integrated presentation but will not be found as useful and satisfactory as the following ones. Some readers may object for instance to seeing critical coupling and maximally flat coupling confused in Section 2.5, or not completely agree with statements like the following: "according to one view of electricity the individual charges to which lines of force attach themselves are unable to flow through the conductor with the velocity of light. If this is true, lines of force snap along from one charge to the next in a rather mysterious fashion".

The eighth chapter deals with impedances in waveguides, junctions, irises, tuners and cavities.

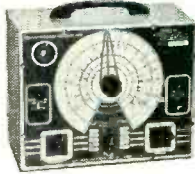
The ninth chapter considers waveguide components in general, transformers and filters. Here the quality of the book and the wealth of material made available become outstanding. New information previously unpublished is given; the problem of branching filters is extensively dealt with together with that of more conventional filters, phase shifters, hybrid junctions, directional couplers, mode converters, rotary joints and attenuators.

The next chapter covers antennas, with a particularly excellent and complete treatment of horn antennas. Leaky waveguide antennas and dielectric antennas are dealt

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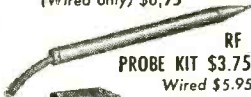
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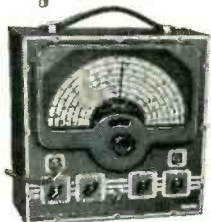
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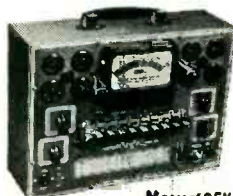
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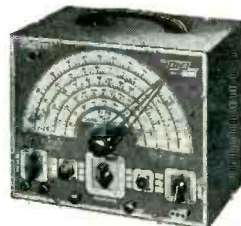
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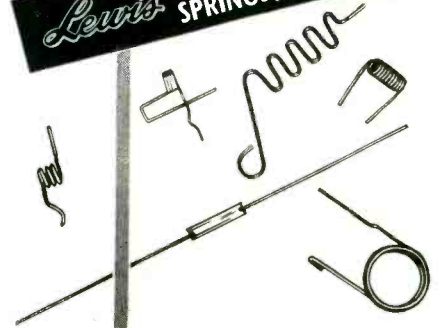
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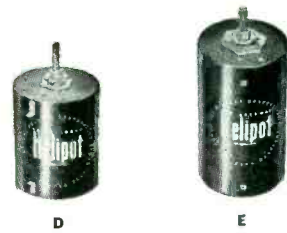
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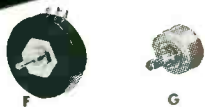
In this panel are illustrated standard models of HELIPOT multi-turn and single-turn precision potentiometers—available in a wide range of resistances and accuracies to fulfill the needs of nearly any potentiometer application. The Beckman DUODIAL is furnished in two designs and four turns-ratios, to add to the usefulness of the HELIPOT by permitting easy and rapid reading or adjustment.



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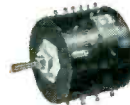
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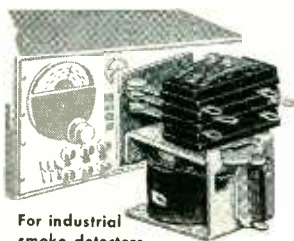
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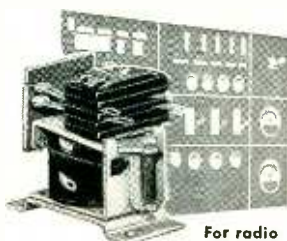
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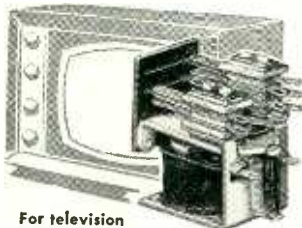
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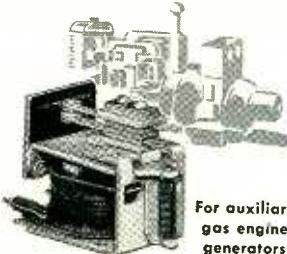
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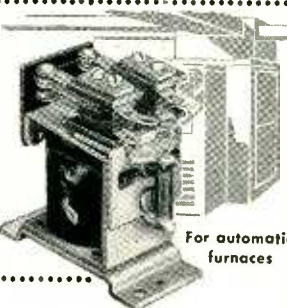
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MANUAL AND MAGNETIC ELECTRIC CONTROLS — FOR AUTOMOTIVE, INDUSTRIAL, COMMUNICATION AND ELECTRONIC USE

with in detail. Here again, material previously unpublished or available only through patent literature is supplied. Parabolic antennas and lens antennas are also dealt with, in somewhat less detail. In this chapter particular mention should be made of not only the section on horns but also that on corner reflectors, an important subject not usually covered in textbooks.

The eleventh chapter deals with tubes capable of operating at microwave wavelengths. The section on microwave amplifiers is particularly interesting. Information not previously available on circuits using the microwave Western Electric tube type 416A is also given. Descriptions of the multigap velocity variation tubes (which used to be known during the war as Samuel tubes) are given. Magnetron oscillators are also dealt with in reasonable detail; some basic information is given on traveling-wave tube amplifiers and TR and ATR tubes.

The twelfth chapter, on modulation and demodulation, contains, besides some other very useful information on converters, a summary of a theory on frequency conversion by crystals which is published here for the first time and which is attributed to A. B. Crawford.

In conclusion, this book contains a very complete summary of applications of waveguide components, suggests new ideas and points the way to future progress in the microwave field.—E. G. FUBINI, *Super-vising Engineer, Airborne Instruments Laboratory, Mineola, N. Y.*

Survey of Modern Electronics

By PAUL G. ANDRES. *John Wiley & Sons, Inc., New York, 1950, 522 pages, \$5.75.*

IN THE PREFACE to this book on electronics the author states that it is intended for use in a survey course in electronics for electrical engineering students who have not yet begun to specialize in power, communication or any other field. The emphasis throughout the book is very frankly on the description of electronic devices by words and pictures rather than by mathematics. The many applications of



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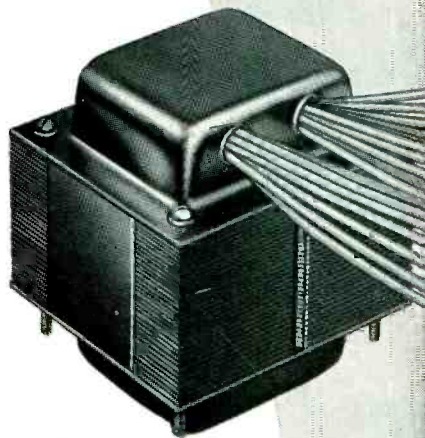
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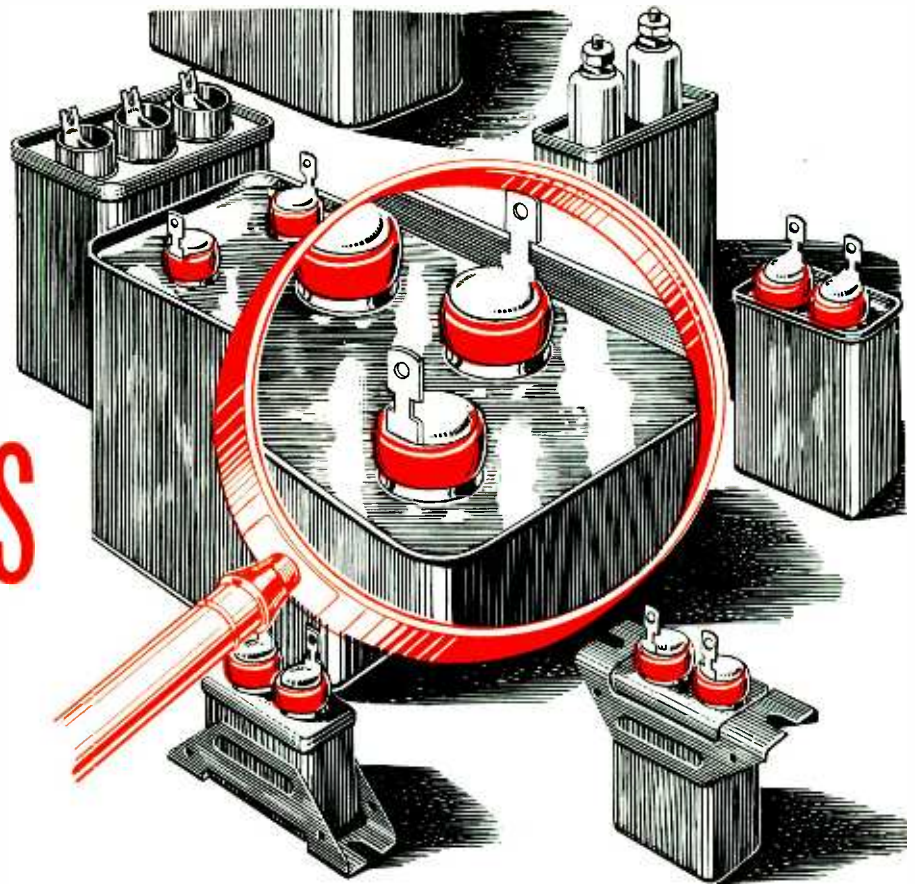
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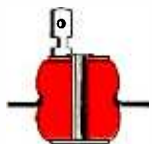


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electronics treated include a number which are not to be found in other texts of this general level—some interesting examples are the sections on Electrical Detearing and Precipitation, The Mass Spectrometer, Metal Detectors and The Electroencephalograph.

This broad treatment would certainly serve to arouse an interest in the field of electronics in the minds of electrical and other engineering students who have not begun to specialize. Although there is some gap between the elementary treatment of such subjects as the triode amplifier and the associated application example—an automatic pilot in this case—the excellent problems at the end of each chapter would serve to fill in if they were properly used.

Electrical engineering students are often plunged into the detailed study of the elements of electronic circuits in their junior or senior year without being provided with reasons for the importance of these elements. A survey course based on a book such as this would help to explain why the more detailed and more mathematical studies which follow are necessary.

A goodly number of references are given at the end of each chapter, and the index appears to be quite complete.—VINCENT C. RIDEOUT, *Assoc. Prof. of Electrical Engineering, Univ. of Wisc.*

Father of Radio

The Autobiography of Lee de Forest. Wilcox & Follett, Chicago, 1950, 500 pages, \$5.00.

ANY DISBELIEVERS of the idea that the way to succeed is to try, try again had better read this story of "old Doc" and become converted. For this is an incredible story of success and failure, one following the other, time after time throughout the first fifty years of a man's life and of the life of wireless and radio. Success in invention; failure in exploitation. It is the story of the unfinanced inventor, one gifted not only with technical ability but with great dreams; a story of the troubles such inventors have. All sorts of troubles; finances and the lack of them; unscrupulous associates; lawyers; stock salesmen; great companies with great funds;

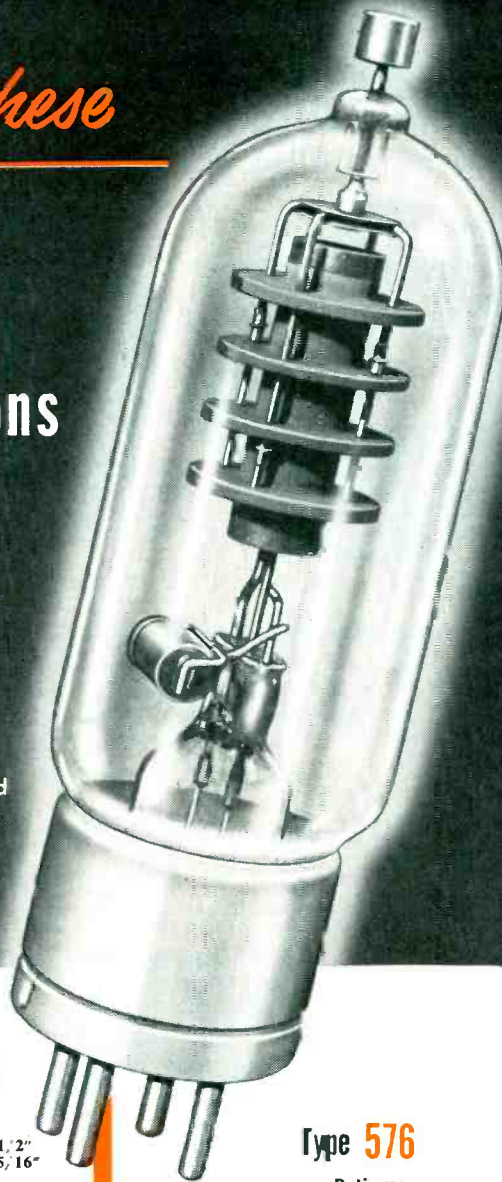
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Ib 2.5 amps.



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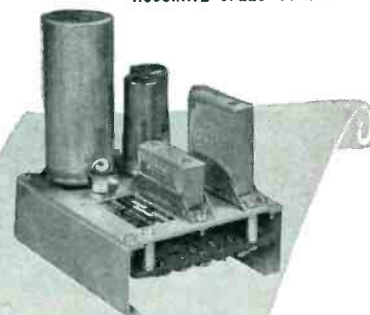
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In the first half-century of any art or science as big as electronics there is bound to be much that is exciting, tawdry, good, bad, sad, joyous. Of all these, Doc had his share. But he always had hope. There is scarcely any technical phase of electronics in which de Forest did not make an important mark; and of the major aspects of electronics as we now know it, he was way out a head of the procession. His efforts to establish and maintain wireless telegraph systems here and abroad, his first use of the electric knife in surgery, his broadcasting of voice and music before the present brood of crooners began drooling, his early work with sound-on-film, the story of the telephone repeater, of electronic musical instruments and of much more—all this is in Doc's book in his own words.

From the nontechnical standpoint, de Forest's love of music, of poetry and of the classics or his prowess as a mountain climber may be news to those who know so well his technical deeds; but there is no doubt about the value of these extra-curricular activities to him.

To the end the "father of radio" believes that better service could have been made of at least one part of his contributions—broadcasting—and there are millions of former avid listeners who will agree with him.

This is an interesting and often inspiring story.—K.H.

High-Speed Computing Devices

BY THE STAFF OF ENGINEERING RESEARCH ASSOCIATES, INC., including C. B. TOMPKINS, J. H. WAKELIN AND W. W. STIFLER, JR. McGraw-Hill Book Company, New York, 1950, 451 pages, \$6.50.

THIS BOOK is quite well written and should be of great interest to anyone concerned with computing machinery, particularly digital type computers. The material is presented in such a fashion that it could be successfully used as a first-course textbook for graduate students interested in digital computers. The basic fundamental concepts of machine computation are



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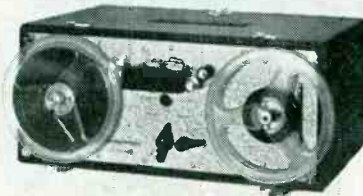


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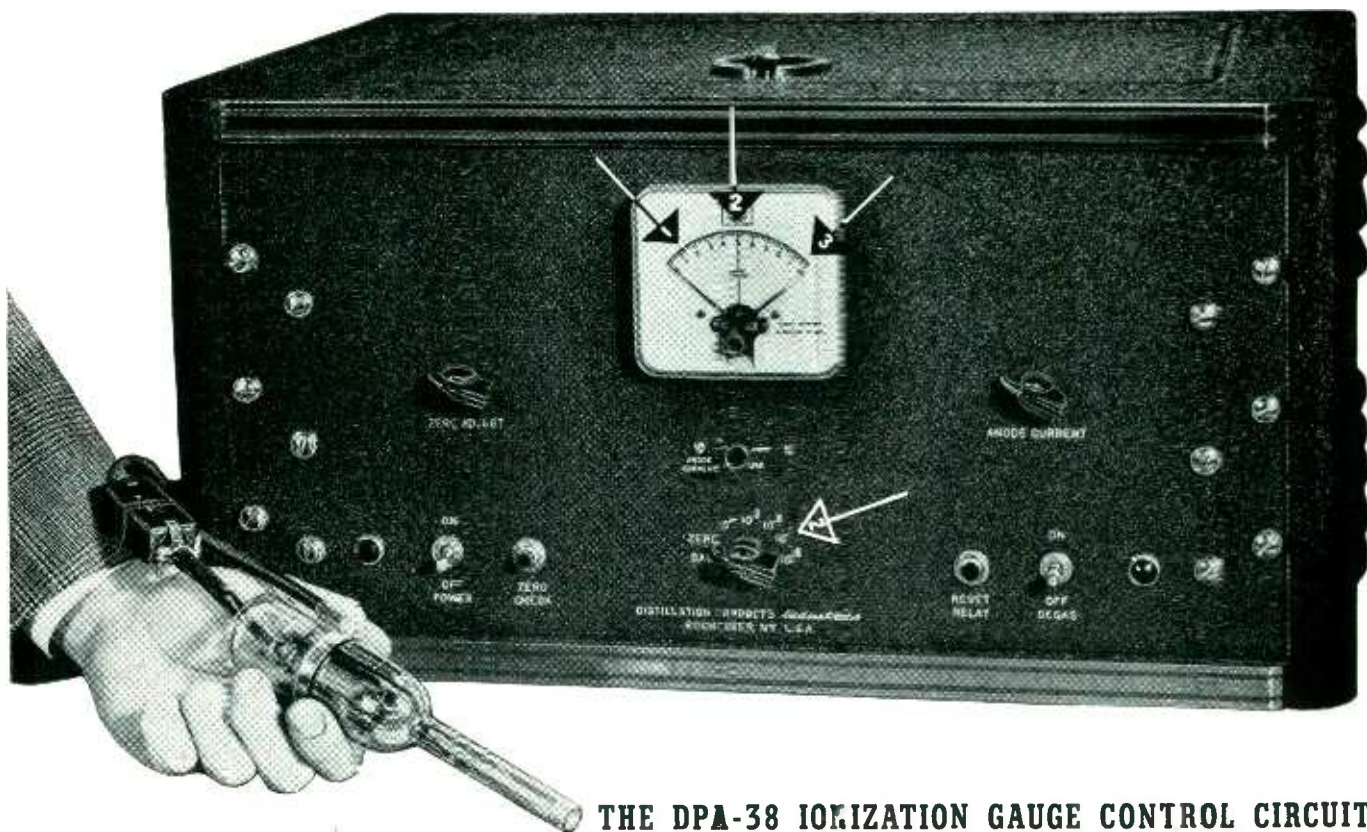
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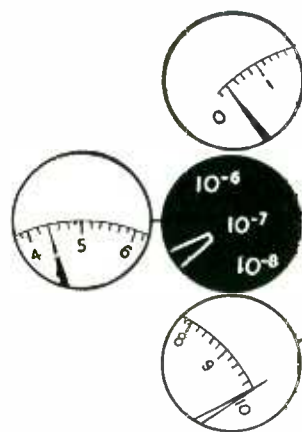
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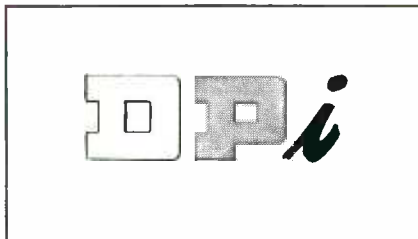


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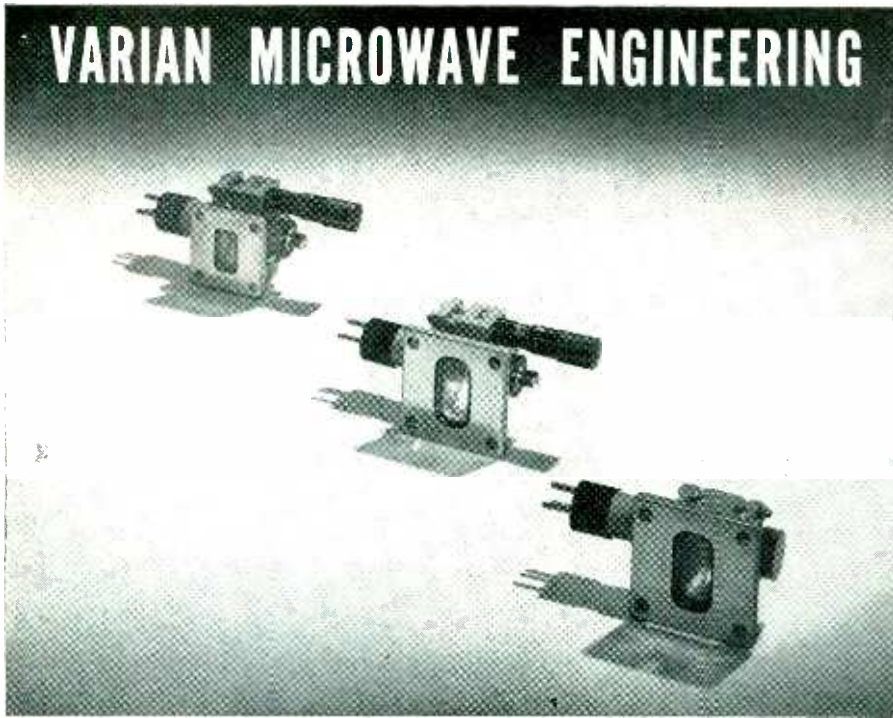
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.. adds a new broadband waveguide-output klystron

Designed for high-power laboratory and antenna measurements as well as for use as a stable transmitter tube in fixed and mobile service, the new Varian X-21 Klystron covers the frequency range 9100 to 11,000 mc. It is illustrated at right above. The two resonant cavities are integral and have self-contained feedback. Output mates with standard UG/39U flange for 1/2-by-1-by-0.050-in. waveguide. Low microphonic construction. Weight, 4 1/2 oz.

Typical Operation: Frequency, 10,000 mc; beam voltage, 1270 v; beam current, 98 ma; power output, 5.9 w; load VSWR, less than 1.1.

Two tunable waveguide-output reflex klystrons for the frequency range 8100 to 17,500 mc, the Varian X-12 and X-13, left and center in the illustration. Widely used for transmitter service and as local and bench oscillators as measurement power sources. Single screw tuners cover entire frequency ranges.

Typical Operation:	X-12	X-13
Frequency, mc	16,000	10,000
Beam Voltage	600	400
Beam Current, ma	50	48
Reflector Voltage	280	575
Power Output, mw	25	230
Load VSWR, max	1.1	1.1
Modulation Bandwidth, mc	50	30
Temperature Coefficient, mc per deg C, max	0.25	0.25

Now in production, two new klystrons for television service. Varian X-17 covers the range from 1990 to 2100 mc with 5 watts minimum power output. Varian X-26 Klystron group covers 5850 to 8200 mc with 0.5 watts minimum power output.

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NEW BOOKS

(continued)

quite clearly presented. The authors have done a particularly good job in breaking down a complex subject into simple terms such that one with only a reasonable technical background will have no difficulty in following the material.

It is somewhat disappointing, however, that the authors did not include more information on analog-type computers. The book consists of seventeen chapters and only one is devoted to analog computers. Furthermore, most of this chapter deals with analog computers in the most general terms only. Some details of the differential analyzer are given but less than one page is devoted to the large, modern general-purpose analog computer such as the Anacom at Westinghouse and Northwestern University and the California Institute of Technology. There is no discussion of modern analog techniques nor of the basic procedures used to derive analogies. The bibliography on analog computers is incomplete. A number of the classic analog papers presented during the past 10 years are not mentioned.

For those interested in digital type computers only, the book presents much valuable and interesting material.—D. L. WHITEHEAD, *Engineer in Charge, Analog Computing Laboratory, Westinghouse Electric Corp.*

Industrial Instrumentation

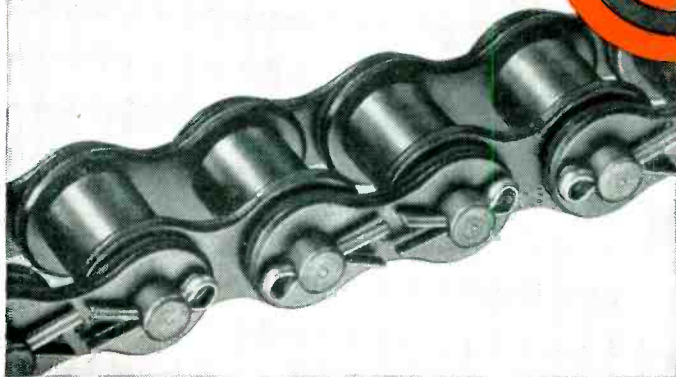
By DONALD P. ECKMAN. *John Wiley & Sons, Inc., New York, 1950, 396 pages, \$5.00.*

AS AN introduction to the science of measurement for engineering undergraduates, this book reviews one by one the principles of various methods of measuring and sensing employed in industrial processing and manufacturing. Though emphasis is on the method rather than the mechanism, important practical details are stressed wherever possible.

Although electronic equipment is not specifically covered, practically all of the information in this book is essential for intelligent application of electronic controls in industry, since each control system must start with measurement of a variable. An appendix of tables,

Truarc E-Rings Improve Performance of Detachable Chain...5 ways!

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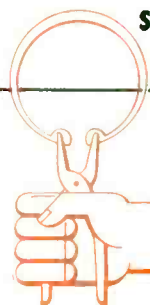
2. GREATER SHOCK RESISTANCE. Higher *shock strength ratios* than cotter pins, due to greater contact surface plus spring reaction for damping moment of shock. Circular movement of ring in groove relieves *shock surface loadings*—instead of resisting rigidly as with cotter pins in fixed holes.

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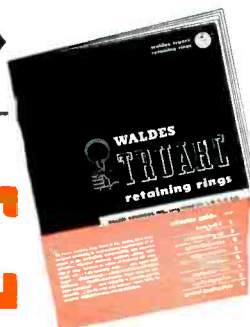


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FREQUENCY RESPONSE: 50 to 15,000 c.p.s. flat within $\pm 2\frac{1}{2}$ db.
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Microphones **BY TURNER**

NEW BOOKS

(continued)

dealing mostly with temperature measurement since this is the commonest type of instrumentation, adds to the reference value of the book for all engineers. Questions and problems after each chapter add to the value as a text both for colleges and for home study.—J. M.

THUMBNAIL REVIEW

MAGNETIC RECORDING — 1900-1949. Bibliography Series No. 1, John Cretar Library, 86 E. Randolph, Chicago, 60 pages mimeographed, \$2.00. Compiled by Carmen Wilson, chief, Technology Department, to meet requests for material on magnetic recording. References have been supplemented by descriptive annotation or abstract wherever titles were not self-explanatory. References to outstanding patents are included. Arranged chronologically and cross-indexed by authors and by subjects.

RCA RECEIVING TUBE MANUAL RC-16. RCA Tube Department, Harrison, N. J., 320 pages, \$.50. New edition covers over 460 receiving and picture tubes, brought up to date by revisions and expansions. Technical data sections include new material on calculation of power output, load resistance and distortion, cathode-follower data, and high-voltage and safety considerations for kinescopes. Many new audio amplifier and receiver circuit designs have been added.

NOMOGRAMS OF COMPLEX HYPERBOLIC FUNCTIONS. By Jorgen Rybner, Professor at Royal Technical University of Denmark. Available from Scandinavian Book Service, 620 W. 158th St., New York (in English), 1947, 35 pages plus charts and diagrams, \$4.80. Large, accurately printed nomograms give accuracy comparable to 5-place tables and a computing machine. The charts present the sinh and cosh functions as rectangular functions of a rectangular variable, and the tanh function as a polar function of a rectangular variable. Additional material in the text makes it in some respects a compendium of transmission line and filter theory.

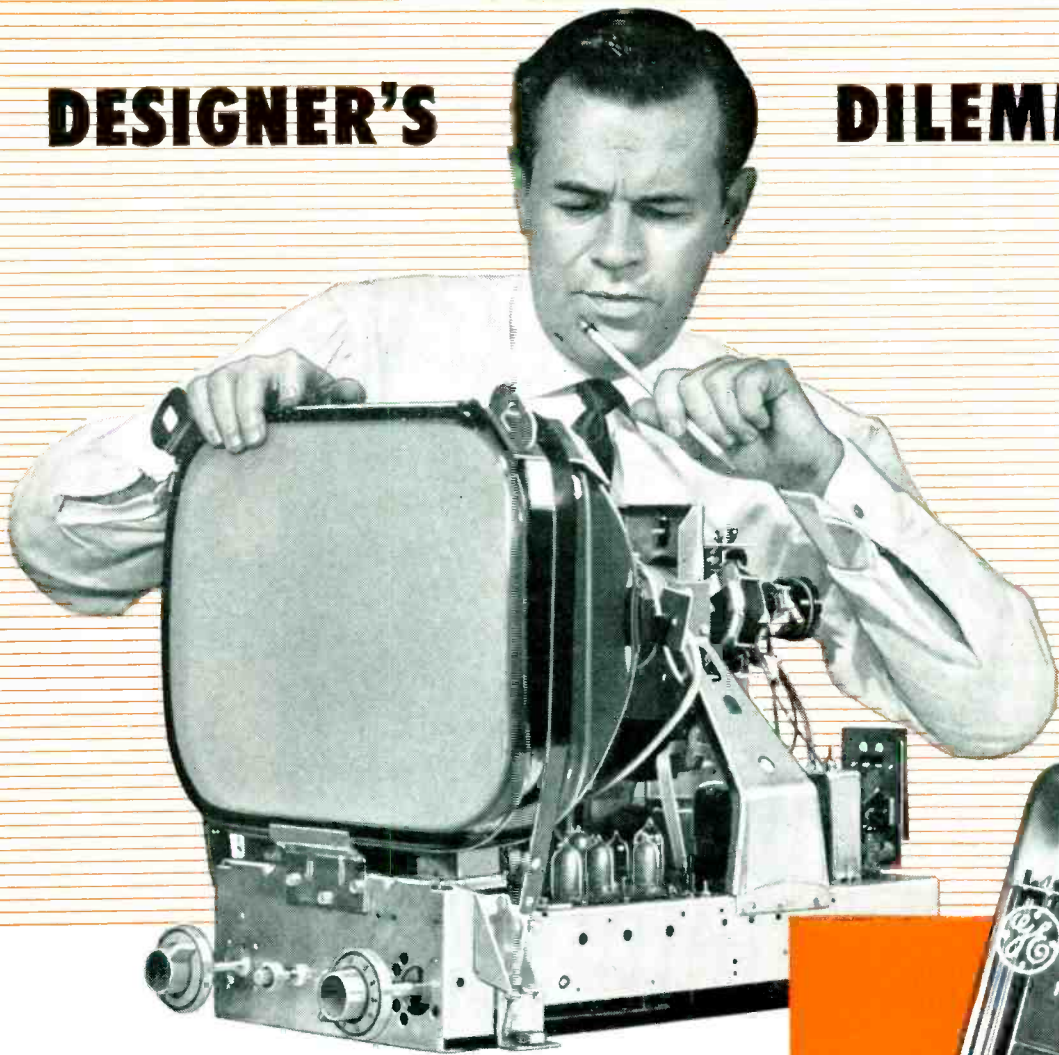
TABLE FOR USE IN THE ADDITION OF COMPLEX NUMBERS. By Jorgen Rybner and K. Steenberg Sorensen. Available from Scandinavian Book Service, 620 W. 158th St., New York (in English), 1948, 95 pages, \$4.00. Facilitates calculations with complex numbers by making possible their addition or subtraction in polar form.

TELEVISION SERVICING. By W. H. Buchsbaum. Prentice-Hall, Inc., New York, 1950, 340 pages, \$5.35. Written to aid in training technicians in television. Part I covers receiver theory; Part II deals with installation and alignment; Part III serves as a troubleshooting guide.

STRUCTURAL PLASTICS. By H. C. Engel, C. B. Hemming and H. R. Merriam. McGraw-Hill Book Co., New York, 1950, 301 pages, \$4.50. First seven chapters deal largely with properties of plastics, molding procedures, sandwich constructions and structural adhesives, but the last chapter—Radomes and Microwave Windows—is definitely of interest to electronic engineers. This analyzes the broad problem of providing antenna covers, also called radomes and microwave windows, that are as transparent as possible to the radio waves they are designed to pass. Four basic radome solutions are presented—the thin wall, thick wall, double thin wall and sandwich, and a design procedure is given.

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6BN6

GATED-BEAM MINIATURE

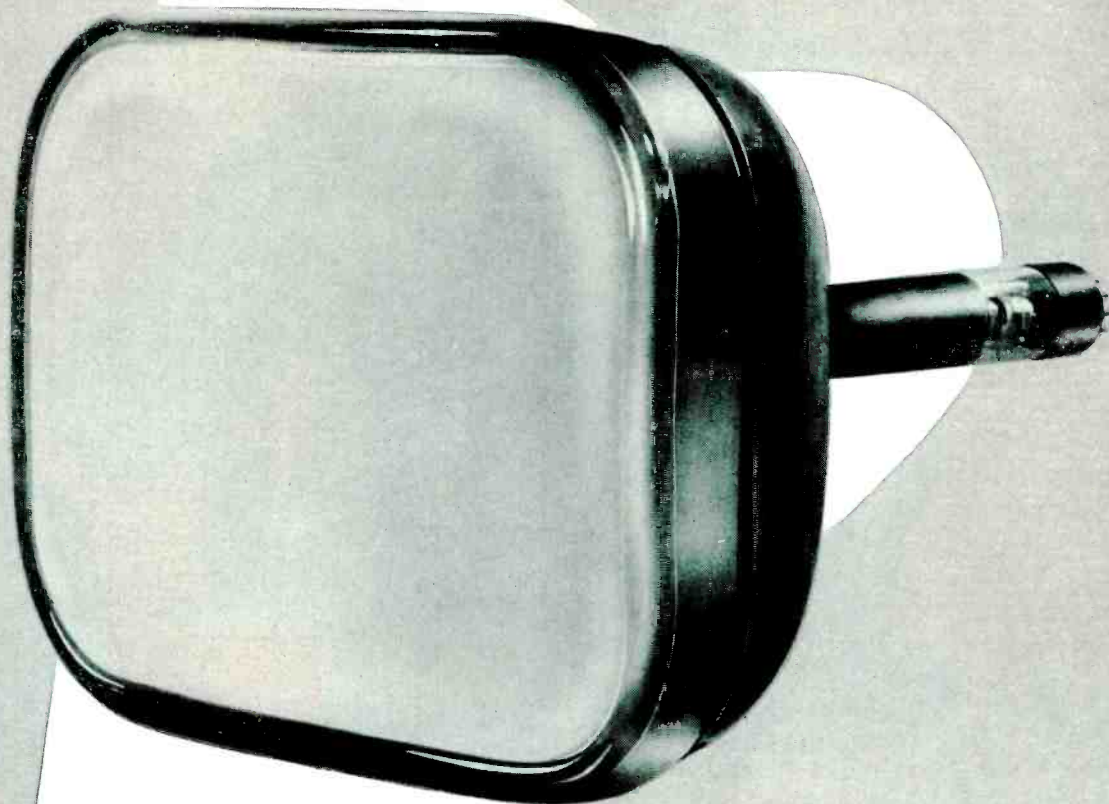
Typical Operating Conditions,
TV Application, 4.5 mc

Plate supply voltage	270 v
Plate load resistance	.33 megohms
Accelerator voltage	100 v
Cathode resistance	200 to 400 ohms
Min signal voltage for limiting action	1.25 v RMS
Audio output voltage	12.5 v RMS
AM rejection, with 2-v input signal	25 db

GENERAL ELECTRIC

181-K1

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THE STORY OF AMERICAN TELEVISION IS THE HISTORY OF TELEVISION

TUBES AT WORK

(continued from p 122)

sufficient sensitivity and accuracy.

An amplifier was constructed using the circuit shown. The amplifier is designed for operation of a Weston model 370 a-c and d-c milliammeter, an instrument of the electro-dynamometer type with a stated accuracy of $\frac{1}{4}$ percent of full scale.

The amplifier is direct coupled throughout and makes operation possible on d-c as well as a-c. It maintains the combination useful as a transfer means between alternating and direct voltages.

The input voltage range of 1.5 to 300 v full scale is covered with a voltage divider made up of wire-wound precision resistors of 0.1 percent accuracy. The input resistance is 1,000 ohms per volt. For the ranges of 0.75 down to 0.15 volt full scale, reduced amounts of feedback are used with a fixed input resistance of 1,500 ohms.

The input voltage between grid and cathode of the first stage of amplification was measured as approximately 0.0039 v for full scale deflection of the milliammeter. For input voltage ranges of 1.5 to 300 v, the output of the voltage divider is 1.5 v. The feedback voltage is correspondingly about 1.496 v. The required feedback resistor is then $1.496/15 \times 10^{-3}$ or approximately 99.7 ohms. Accuracy of scale calibration thus depends mainly on the accuracy of adjustment of the feedback resistor. For a 0.15-v input, the feedback voltage is 38 times the net grid-cathode input voltage.

Advantages of D-C Coupling

The use of d-c coupling in a high-gain amplifier brings with it problems of drift and zero adjustment but much higher values of negative feedback are allowable. Elimination of coupling capacitors or transformers between stages prevents phase shifts giving sufficient positive feedback at certain frequencies to cause oscillation. The use of a large amount of negative feedback reduces drift and sensitivity to power supply variations to nearly a negligible amount. Some drift has been noticed during warmup on the lowest voltage ranges (where the feedback is reduced) but is easily compensated

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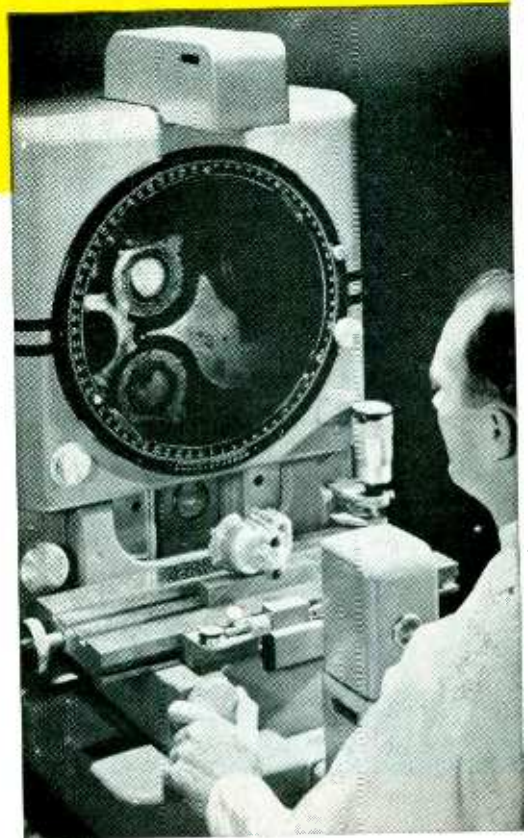
DEEP RECESSES ▶



SURFACE DETAILS



CONTOURS



Few objects are too small or complicated for *complete* inspection under magnification with the Kodak Contour Projector. Deep recesses and surface details, *illuminated from the projection system itself*, stand out sharply and in natural color.

With unmatched versatility, it can be switched instantly from surface illumination to silhouette projection, or a combination of both. Any of six magnifications from 10X to 100X is available at the turn of a dial *without refocusing*. Your operator can work rapidly and efficiently, unhampered by the usual hoods or curtains.

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Multipole Types, Too!

In addition to the single-pole units illustrated, Struthers-Dunn produces these hermetically-sealed aviation relays in types up to 6 poles and having the same exacting characteristics.

These little hermetically-sealed d-c relays are specifically designed for aviation conditions involving high shock and vibration, elevated temperatures and high altitudes. A completely new magnet structure permits greatly reduced size with improved dependability. Three available types are for operation up to +85°C., +160°C. and +200°C. respectively, thus matching specific aviation service requirements. Write for S-D Data Bulletin 2410.

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ST. LOUIS • SAN FRANCISCO • SEATTLE • SYRACUSE • TORONTO



Amplifier and electro-dynamometer-type milliammeter set up for operation

by the zero adjustment shown.

Regulated power supplies were found advantageous for stabilizing the low input voltage ranges and for maintaining high accuracy for either polarity of d-c input voltage. A high degree of regulation is not required, but an improvement over the natural power supply regulation (for d-c input voltages and corresponding plate current changes) and changes due to a-c line voltage variations is desirable.

A troublesome problem in the initial development of the amplifier was the effect of conductive grid current in the first stage. With low plate and grid bias voltages, a small but significant grid current may flow because of ionized gas in the tube or the initial velocity of electrons emitted from the cathode. This effect varies with electrode voltages, heater temperature, and the particular tube of a given type.

A current of 1 μ a flowing through the 1,500-ohm grid to cathode voltage-divider resistance would cause an error in the input voltage of 0.1 percent. It is important to keep the plate potential of the first stage high enough to maintain the grid current at a low value, even at the expense of loss of gain in a voltage divider to supply the grid of the next stage.

The inherent gain of the amplifier is so great that it is difficult to adjust without feedback. However, by adjusting one or two stages independently, finding proper input and output d-c potentials, and then connecting all stages together along with the feedback loop, correct operation may be obtained.

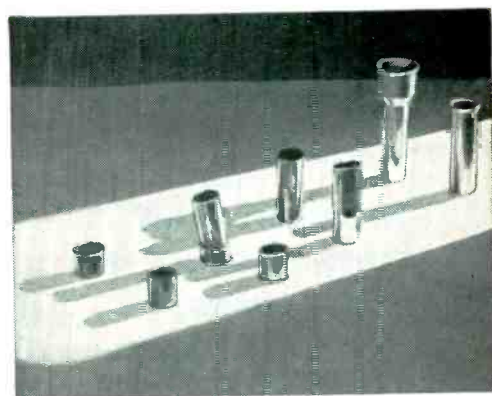
Performance and Applications

The combination described may be used also to measure current in

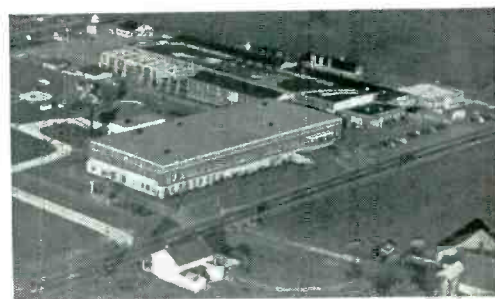
Through this portal pass the nation's top stars



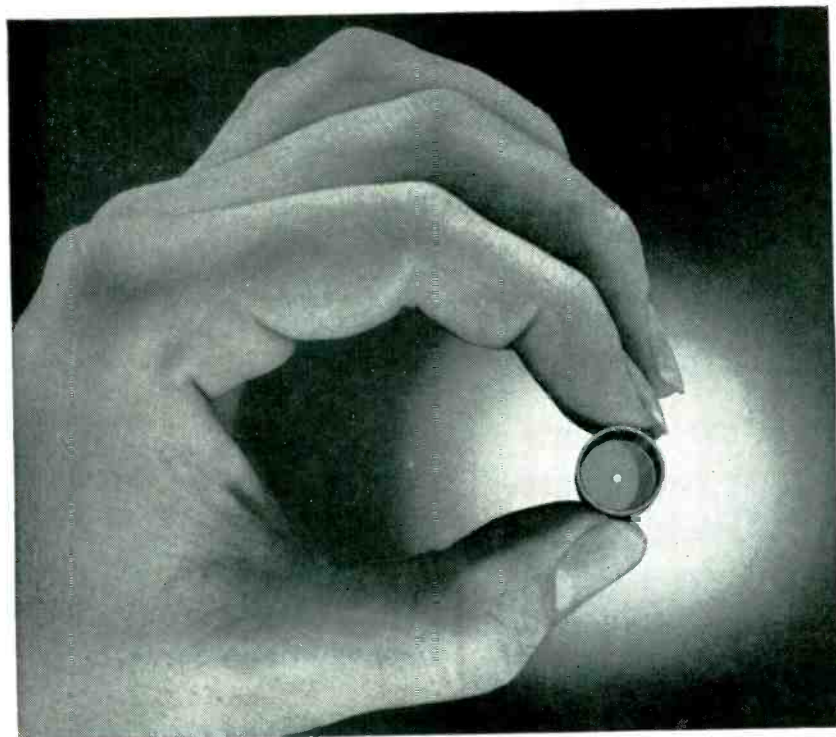
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● You may not recognize the object pictured above. It is the first grid cylinder for a cathode ray tube gun structure, photographed from an unusual angle. The hole is only .040" in diameter—and the grid itself is deep drawn in one piece to save unnecessary welding and assembly operations by TV tube manufacturers.

This is tubing technology in operation. It is an example of Superior's superiority in electronic research, production know-how

and facilities, and metallurgy. It is one product of hundreds pioneered for the electronic industry by Superior.

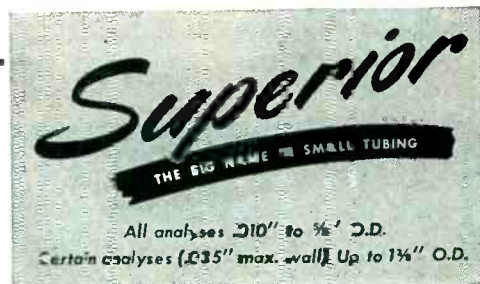
You may already be one of our valued customers and friends—nearly all electronic manufacturers are. If small Seamless or †WELDRAWN tubing can help anywhere in your product Superior can help you. To find out how, write Superior Tube Company, 2500 Germantown Avenue, Norristown, Pennsylvania.

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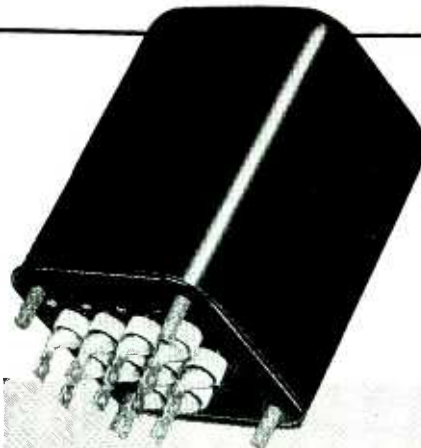
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TANT NEED. CHICAGO Hermetically Sealed Transformers meet all requirements of Grade I, JAN-T-27 specifications for Class A operation. Designed expressly to fill transformer requirements for military airborne, marine, and ground communication equipment, as well as for use in tropical and sub-zero climates. Ideal for a wide range of application, particularly in research and development work, prototype equipment and pilot runs. The complete range of CHICAGO JAN-T-27 units is available for quick shipment from stock.



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2. Immersed in hot and cold brine at temperatures of 75°C to 0°C.
3. Subjected to severe vibration on shake table for 20 periods of 15 minutes each.
4. Given a pull test on all terminals, from all directions, of 5 lbs. or more for 30-second intervals.
5. Tested on each winding at twice rated a-c voltage and frequency.
6. Tested for insulation resistance in excess of 500 megohms throughout heat-and-cold cycles.
7. Tested for corona discharge at voltages 1 1/4 times operating voltage of transformers.
8. Capable of operation in 65°C ambient temperature with temperature rise not exceeding 40°C.
9. Operated 48 hours with 12% overload at rated ambient temperature.

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a shunt. The 0.15-v range is particularly useful in this case.

Another possible application is in the measurement of low values of power. Provided a non-inductive resistor is used for feedback, the large amount of feedback employed insures a very accurate phase relation between input voltage and output current. Amplifiers of this type might be used to drive potential, current, or both circuits of electro-dynamometer voltmeters to measure accurately very small amounts of power.

Amplifiers of this type may be used to drive thermal instruments. The attendant advantages may be increased sensitivity and a much wider input current or voltage range than generally available in a single instrument.

Several particularly useful applications of this type of amplifier to the measurement of slowly varying or sub-power-frequency quantities have come to the author's attention. Since the amplifier is d-c coupled, it has no low frequency limit.

Wien Bridge as Frequency-Shift Servo

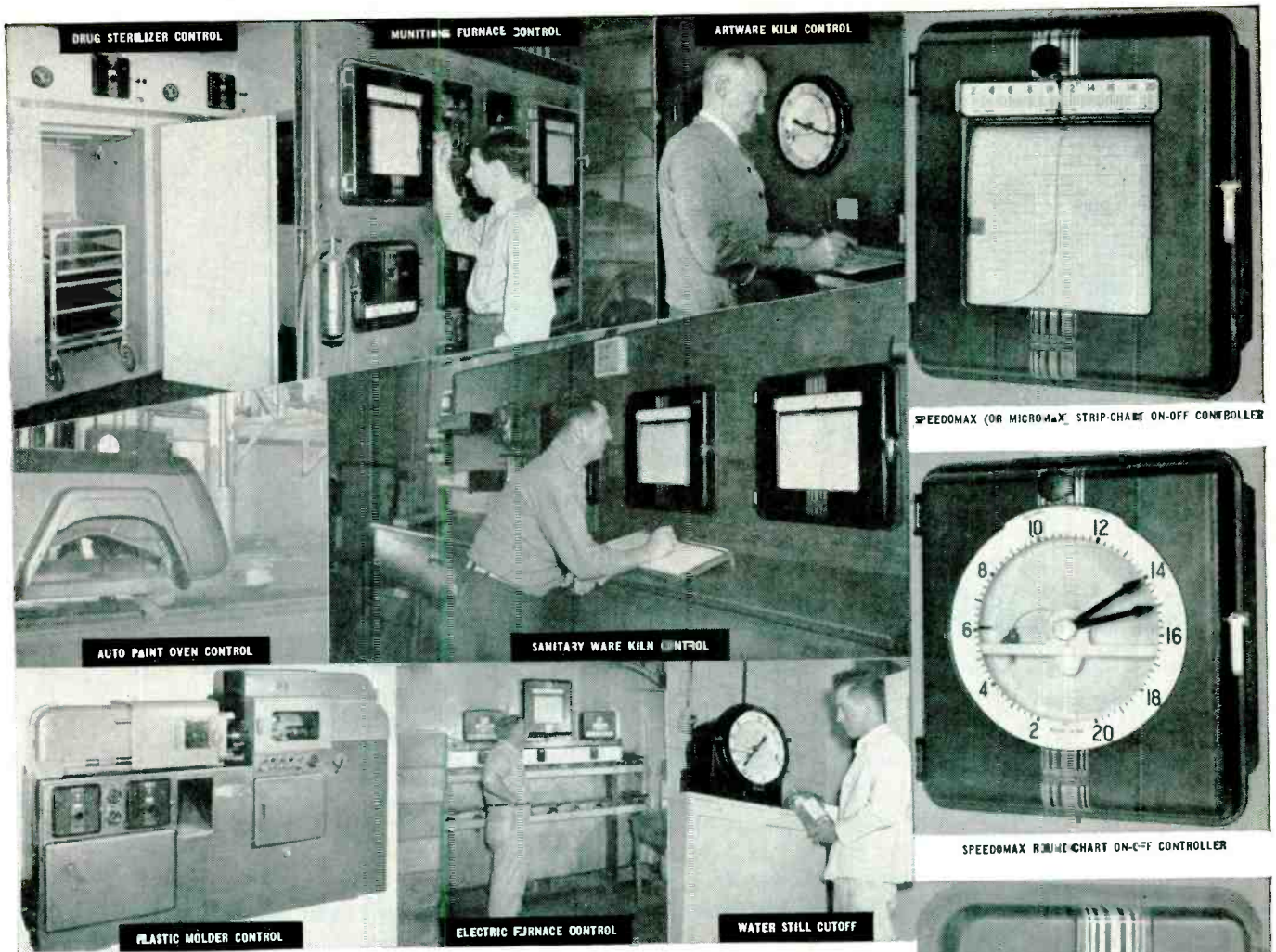
BY JACK YEISER

Field Engineer
Philco Corporation
Philadelphia, Pa.

USE of a Wien bridge as a frequency discriminator in servo applications makes it possible to employ a standard two-gang variable capacitor as the rebalance element. The low inertia of the capacitor as compared to moving-iron or slide-wire elements results in rapid response of the system.

The instrument was constructed as a recording frequency meter for the purpose of recording tele-metered information appearing as an audio tone with frequency varying between 45 and 150 cycles. Sensing is provided by taking advantage of the 180-degree phase shift which occurs as the bridge passes through a null.

A breadboard assembly was used with two standard 12-watt public-address amplifiers corrected for



Dependable "ON-OFF" Controllers for Industry

THE kind of control instrument which industry calls on-off or 2-position is not only the oldest form of automatic regulator, but is one which many manufacturers still use instead of more advanced types, for simple requirements. Usually, the instrument merely closes the valve when temperature reaches the control point, and opens valve again when temperature falls below point. The question of whether such on-off action is best for the given case can of course be settled by using the instrument with the best, most useful features. Here are some which L&N On-Off Controllers offer:

1. Instruments may be Recording Controllers with either strip-chart or round-chart, or Controllers with no charts at all.
2. Instruments can operate at high or moderate speed; can be located regardless of machine vibration, building tremors or distance from process.
3. Controls are outstandingly dependable because they "balance" temperature against a standard. Intermediate bearings and springs cannot increase, decrease or otherwise influence accuracy or sensitivity.
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5. More than 1000 standard ranges. Specials are available, but seldom needed.

Tell us your problem and we will send further information. Write either to our nearest office or to 4979 Stenton Avenue, Philadelphia 44, Pa.

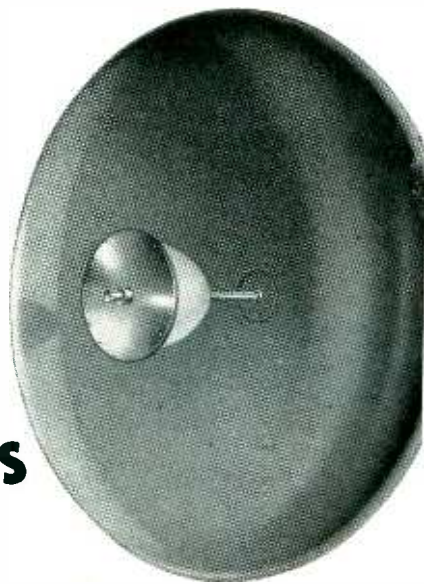
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ELECTRONICS — January, 1951

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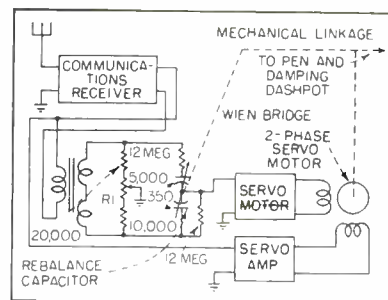
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TUBES AT WORK

(continued)



Breadboard assembly for Wien bridge used as a frequency discriminator in a servo system

zero phase shift employed as servo amplifiers. The input grid resistor of the bridge amplifier is disconnected to prevent bridge unbalance. Transformer T_1 is a balanced shielded type with a one-to-one ratio and zero phase shift over the range of frequencies employed. Balance resistor R_1 is adjusted for best null.

Oil dashpot damping is used and overshoot is negligible for full pen deflection on a 3-inch strip chart with 5-cps excursions.

The Wien bridge follow-up circuit could also prove useful as the receiving servo in radio control systems. The accuracy and stability of the bridge make its use as an accurate frequency meter promising.

TV Receiving Antenna Measurements

By KENDRICK H. LIPPITT

*Chief Engineer
Technical Appliance Corp.
Sherburne, N. Y.*

TECHNICAL information regarding antenna arrays is needlessly confused by the maze of conflicting performance figures published by some manufacturers.

Measurements made on television receiving antennas using the system of the Technical Appliance Corp. result in a gain figure which takes into consideration not only the true gain of the antenna but also the mismatch loss which occurs into a 300-ohm load.

In this system, the voltage developed across the terminals of a folded dipole terminated in a 300-ohm load is compared with the voltage developed across the terminals



OTHER WORKSHOP ANTENNAS

Aeronautical Ground Station
For aircraft communications — omnidirectional.

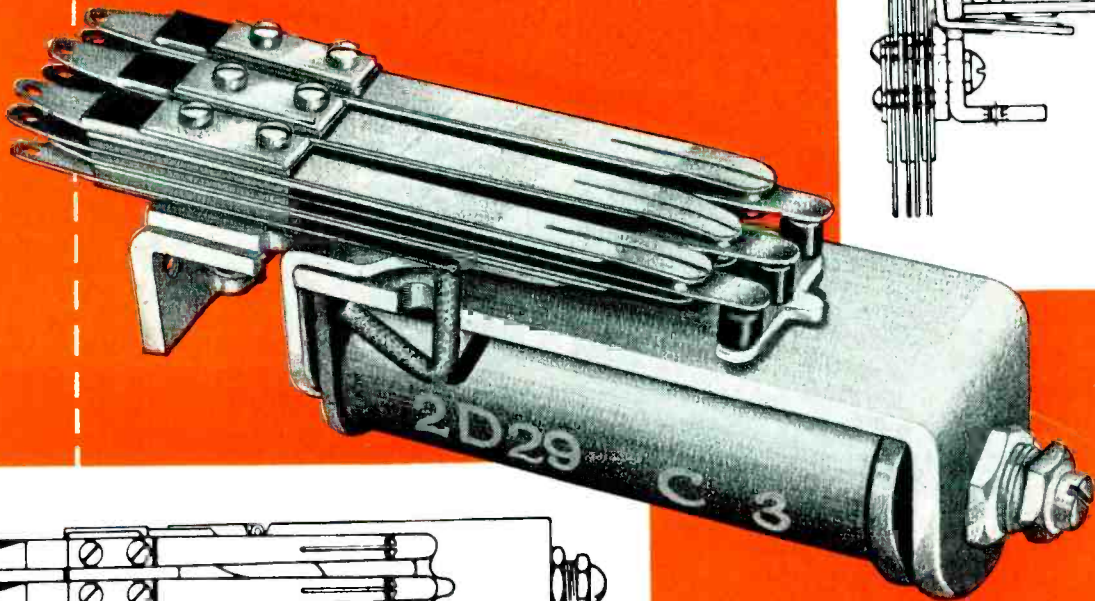
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simple · sturdy



reliable · efficient

BECAUSE their basic principle is so simple, it's easy to believe that anyone can make relays: But, where dependability, reliability and efficiency are specified, such belief leads to certain disappointment.

If you are designing circuits requiring absolute quality, with zero failure, you must have relays backed by years of experience and a very special know-how. North Relays have

just such backing. We've been in the business since 1884, engineering and producing millions of relays, from multiples to midgets, from simple single-makes to intricate pileups with any combination of makes and breaks.

BUY NORTH for insurance on critical relay circuits.



SPECIAL RELAYS? Let North Engineer Them For You
THE NORTH ELECTRIC MANUFACTURING COMPANY
1438 South Market Street, Gallon, Ohio, U. S. A.

— Originators of ALL RELAY Systems of Automatic Switching —

Look to *Permoflux* for the **NEWEST...FINEST...MOST SENSATIONAL** **AUDIO COMPONENTS**

Newest!

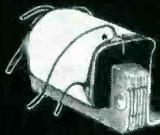
MINIATURES AND SUBMINIATURES

The MRB-3 miniature dynamic receiver and microphone has excellent wide-range frequency response characteristics, maintained flat by the Patented Permoflux acoustical damping method. Utilizes a self-formed voice coil. Sensitivity—115 db in 6 μ c coupler with 1 m. w. input. Overall diameter 1" — height $1\frac{1}{16}$ ". Can be supplied with miniature input or output transformers in any impedance.

T1 and T2 Transformers — and Chokes — These sub-miniature units provide power efficiency from 80-90% with high voltage breakdown characteristics and extremely low susceptibility to electrolytic deterioration. Frequency response is ± 2 db from 100 to 8000 \sim . Impedances up to 200,000 ohms and windings with inductive reactances up to one megohm. Ideal for use with Permoflux microphone-receiver units and headsets.



Model MRB-3



Model T1



Model T2

Finest!

STANDARD HIGH FIDELITY SUPER HIGH FIDELITY DYNAMIC HEADPHONES

are world famous and quality-recognized products of Permoflux Corp. Sturdy and comfortable, they are built to withstand excessive shock, high humidities and a wide range of temperatures without impairing their high efficiency and dependable performance. Patented acoustical damping provides a flat frequency response to 4500 \sim in standard models and through 10,000 \sim in Super High Fidelity models. Unparalleled in performance for broadcast studio, aviation, laboratory, and audiometer work.



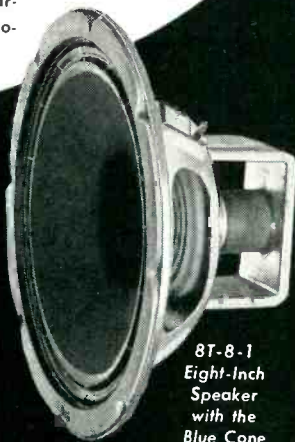
DHS-17
CAA Approved

*MOST
Sensational!*

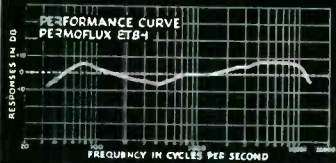
ROYAL EIGHT"

Compares
with any
12" speaker

This average laboratory response curve of the Permoflux 8T-8-1 proves that it compares with the finest speakers regardless of size or price.

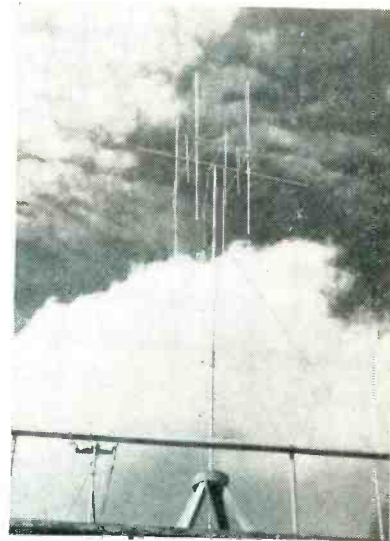


8T-8-1
Eight-Inch
Speaker
with the
Blue Cone



PERMOFLUX
"SOUND IN DESIGN"

PERMOFLUX CORPORATION
4900 W. GRAND AVE., CHICAGO 39, ILL. • 236 S. VERDUGO RD., GLENDALE 5, CALIF.



All-channel type transmitting antenna
in test position

of the antenna array being tested, also terminated in a 300-ohm load.

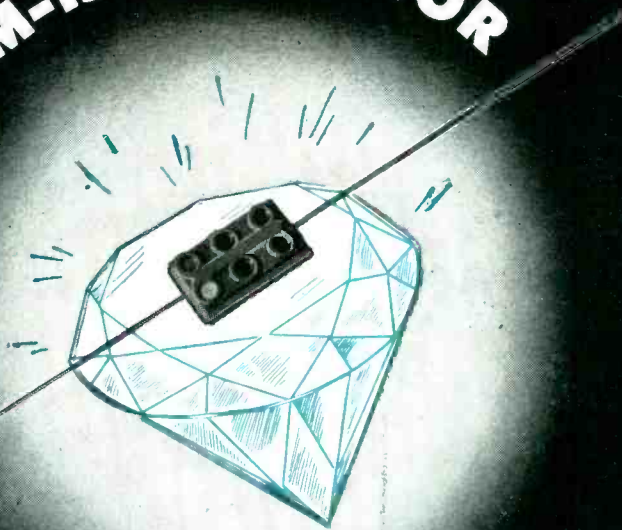
Thirty feet of standard 300-ohm twin-lead line connect the standard folded dipole and the array under test to the measuring voltmeter. A plug arrangement is used at the input to the voltmeter so that neither of the two transmission lines can be connected.

The voltmeter used is an RCA type 301B, a high-frequency field-intensity meter. It has a linear measuring system and is sufficiently stable for gain measurements. The input circuit of the meter was designed to have an impedance of 300 ohms by means of a General Radio bridge, type 916A, and a standing-wave line. For channels 7 to 13 special equipment was built with linear scales.

The zone in which the array is placed for measurement and the half-wave dipole used for reference are not subject to exactly the same signal intensity. Therefore, a television program can not be used to measure the gain of an antenna array because the 6-mc signal level changes as picture detail varies.

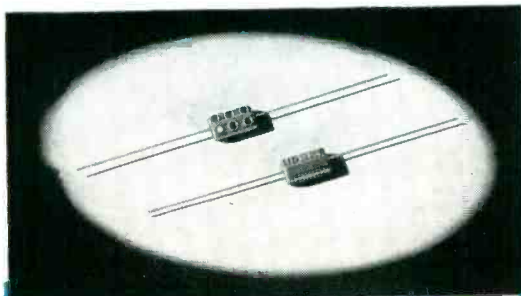
A signal generator with stable output connected to an all-channel-type transmitting antenna is the best source of signal for this type of measurement. It is tunable to any frequency within its range and sends out a signal with a narrow bandwidth. In this way the performance of the antenna over the 6-mc band or over a series of bands

EL-MENCO CM-15 CAPACITOR



THIS GEM-SIZED UNIT DOES A

GIGANTIC JOB



CM-15 MINIATURE CAPACITOR

Actual Size $9/32'' \times 1/2'' \times 3/16''$
 For Television, Radio and other Electronic Applications.
 2 to 420 mmf. cap. at 500v DCw.
 2 to 525 mmf. cap. at 300v DCw.
 Temp. Co-efficient ± 50 parts per million per degree C for most capacity values.
 6-dot color coded.

Each tiny El-Menco CM-15 capacitor performs at maximum efficiency regardless of climate or critical operating conditions. Before leaving the factory, it is tested for dielectric strength at *double* working voltage—for insulation resistance and capacity value. Every gem-sized El-Menco capacitor meets and beats the strictest Army-Navy standards. That's why *you* can always depend on this tiny condenser to give gigantic performance in your product.

A COMPLETE LINE OF CAPACITORS TO MEET EVERY REQUIREMENT

THE ELECTRO MOTIVE MFG. CO., Inc.
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Write on your firm letterhead for
 Catalog and Samples.



MOLDED MICA **El-Menco** MICA TRIMMER CAPACITORS

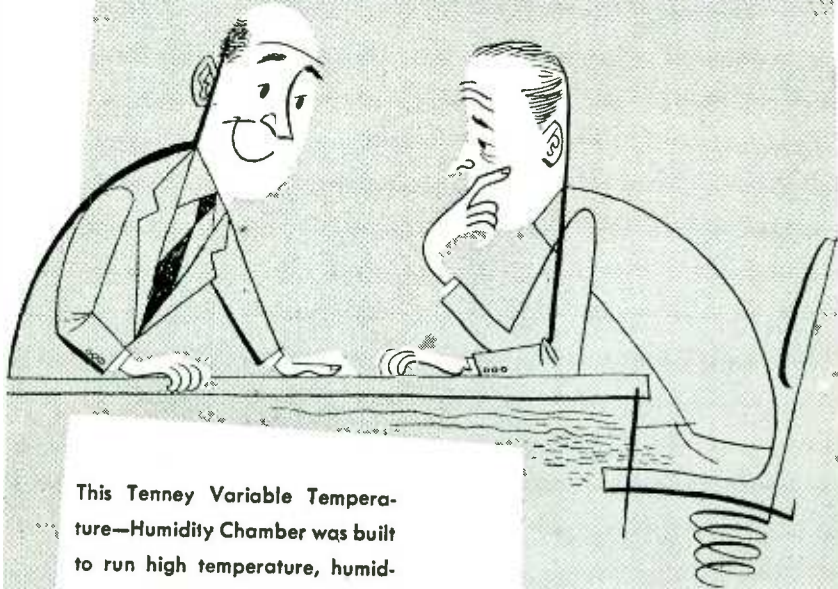
FOREIGN RADIO AND ELECTRONIC MANUFACTURERS COMMUNICATE DIRECT WITH OUR EXPORT DEPT. AT WILLIMANTIC, CONN. FOR INFORMATION.

ARCO ELECTRONICS, INC. 103 Lafayette St., New York, N. Y.—Sole Agent for Jobbers and Distributors in U. S. and Canada

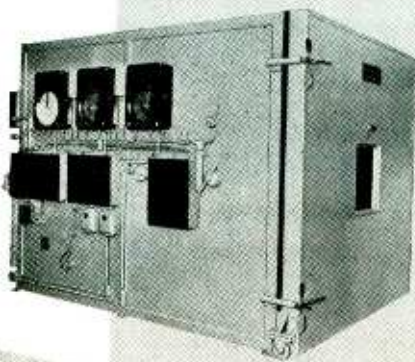
DON'T LET U.S.A.F.

No. 41065-B

GET YOU DOWN, BILL... TAKE IT TO TENNEY



This Tenney Variable Temperature—Humidity Chamber was built to run high temperature, humidity, and mildew-resistance tests (Groups 10, 30 & 70) on aircraft electronic equipment and components under 41065-B. Specified range from 60° F. to 200° F. Relative humidity 20% to 95%. Sizes from 3 cu. ft. to walk-in rooms.



"Take it to Tenney" is sound advice when you're faced with a testing problem. For years Tenney has specialized in designing and building testing equipment to meet the strictest specifications for sand and dust, low temperature, high altitude, liquid immersion, salt spray and many other conditions. Absolutely accurate simulation of changing conditions can be obtained through the use of Tenney program control apparatus. Tenney engineers are always available for consultation and help. You need only ask for their assistance. For literature and further information write Tenney Engineering, Inc., Dept. A, 26 Avenue B, Newark 5, New Jersey.



Tenney

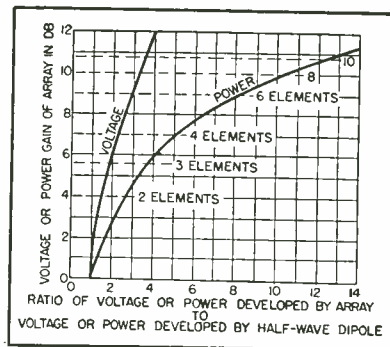
Engineers and Manufacturers of Automatic Temperature, Humidity and Pressure Control Equipment

7183

170

TUBES AT WORK

(continued)



Maximum gain obtainable from antenna arrays with various numbers of half-wave elements. For example, a four-element array is capable of producing a maximum power gain of 5 or a voltage gain of 2.3 which is 7-db gain over a half-wave dipole

swung into the position previously occupied by the antenna array and the meter reading recorded.

With single-channel type antennas, such as Yagi antennas, it is possible to estimate the maximum gain obtainable from any type array made up of half-wave elements. The chart shown gives the maximum gain available from antenna arrays with various numbers of half-wave elements.

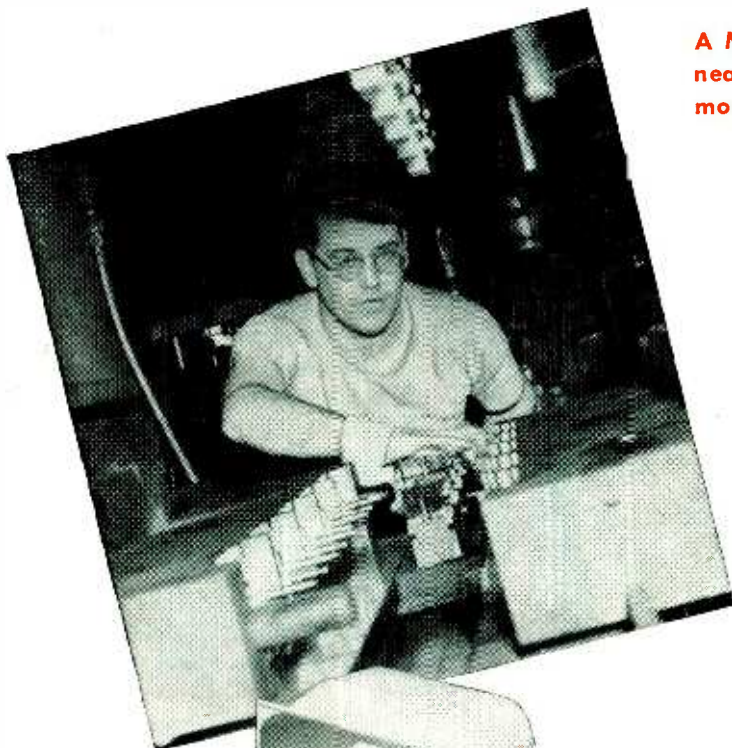
For the same total transmitting power, the power in a single half-wave dipole antenna is twice that in each dipole of an antenna made up of two half-wave dipoles. If the power is cut in half the field produced by the antenna is reduced to 0.707 times its previous value. Therefore, if the voltage from the two half-wave dipoles adds up in phase, 1.4, a 3-db gain is obtained over a single dipole antenna.

In the chart the gain of two elements over one is given as four rather than three db. This improvement is produced by a change in the current distribution on the antenna elements. When elements are spaced close together, as in the conventional Yagi, the current distribution is not sinusoidal. For this same reason, top loading of transmitting antennas is justified where the current distribution is changed to increase the transmitted signal.

The justification for the remainder of the chart follows from the previous reasoning. When the power is divided into two similar antennas, the gain is increased

**TREMENDOUS PLASTICS
MOLDING CAPACITY—**

to serve your needs!



Multicavity molds increase production.

A MILLION-DOLLAR expansion program is now nearing completion at General Electric's modern plastics molding plant at Taunton, Mass.

With expanded plant facilities to serve you in the Midwest and in the East, General Electric now provides a plastics molding service that offers you many important advantages.

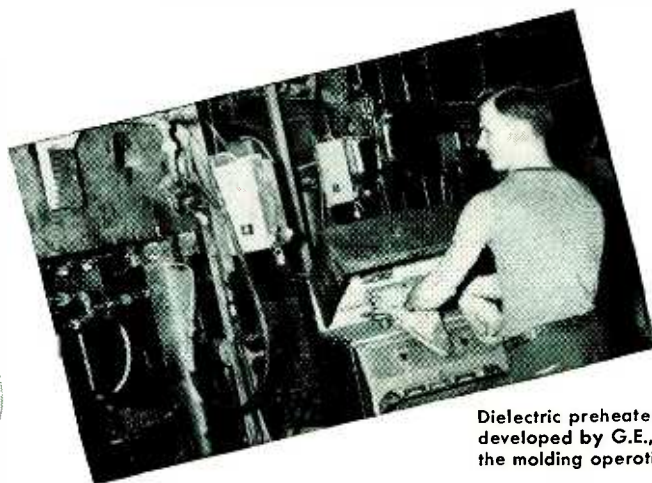
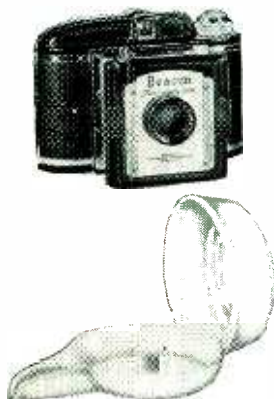
Quick Delivery! New automatic presses and equipment capable of handling the biggest jobs combine to give you *fast delivery*.

Economical Production! Modern plant layout and the latest equipment can cut costs on large-volume runs.

General Electric's 56 years of experience as one of the world's largest plastics molders means you get the benefit of sound and tested designing, engineering, and molding "know-how." You can depend on G.E. for a plastics service that may substantially reduce your costs or improve your product. Write us for further details.

Write on your company letterhead for the interesting booklet, "**Your Plastics Dollars Worth.**" Address: Section Y4, General Electric Company, 1 Plastics Avenue, Pittsfield, Mass.

**ECONOMICAL
BIG-VOLUME
JOBS**—like the refrigerator snack box, camera case, and juicer bowl pictured here—are the specialty of General Electric's molding service.



Dielectric preheaters, developed by G.E., speed the molding operation.

You can put your confidence in

GENERAL  ELECTRIC

three db over one single antenna.

Over a period of two and one-half years more than 1,000 different antenna arrays have been measured using this technique, from single half-wave dipoles to arrays of sixteen elements. During this period the chart has been accurate and satisfactory.

Radioactivity in Textile Production

A COTTON mill in Lancashire, England, is testing the use of radioactivity to measure the uniformity of slivers (pronounced slyvers in the cotton industry). Slivers are strands or slender rolls of cotton in an untwisted state produced by a carding machine and used to produce cotton yarns.

In the manufacture of yarns, the textile spinner has to pass the constituent threads through a series of doubling operations in order to even out any irregularities. This is a costly process and involves much work and handling of materials. If the uniformity of the sliver could be measured quickly and continuously in a uniform condition the doubling process could be eliminated.

The first step towards uniformity is an accurate means of measuring the sliver. This is difficult because sliver is of a loose and spongy nature which makes mechanical means impractical. By employing a beta-ray thickness gage, in which sliver is interposed between a radioactive isotope source and an ionization chamber, a means for obtaining an accurate measurement is available.

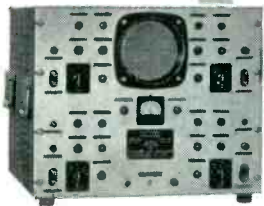
The sliver passing through the path of the rays absorbs some of them and the amount reaching the ionization chamber can be measured in terms of the sliver thickness. The ionization current developed is extremely small but can be amplified and used to operate an indicating instrument or recorder scaled in degrees of thickness or weight per unit length. If necessary, the current can be further amplified and used to operate a

THE OSCILLOSCOPE CAN Fool YOU!

It's no mean trick to keep an eye on 2, 4 or more oscilloscopes for simultaneous comparison. Worse yet may be the successive use of a single 'scope for the one-at-a-time study of different transients that should be compared simultaneously under identical conditions.

ETC Multi-Channel Oscilloscopes reduce these problems to their simplest form—by combining a number of wave forms on a single tube. Whether in equipment or material testing; in electroencephalography, neurophysiology or other medical research; in the field of explosives; in seismography or geology or in other critical applications it is thus entirely practical, infinitely more convenient and often far more accurate to observe different transients under exactly the same conditions or stimulus.

In addition to standard 2-, 4-, 5- and 8-channel 'scopes, ETC produces many special adaptations for specific uses.



4-CHANNEL OSCILLOSCOPE, TYPE H-43. For recording through continuous strip cameras.



UNIVERSAL DUAL CHANNEL OSCILLOSCOPE, TYPE H-22. Plug-in a-c or d-c amplifiers. Registers from DC to 1 megacycle.

ETC

electronic tube corporation

PHILADELPHIA 18, PENNSYLVANIA

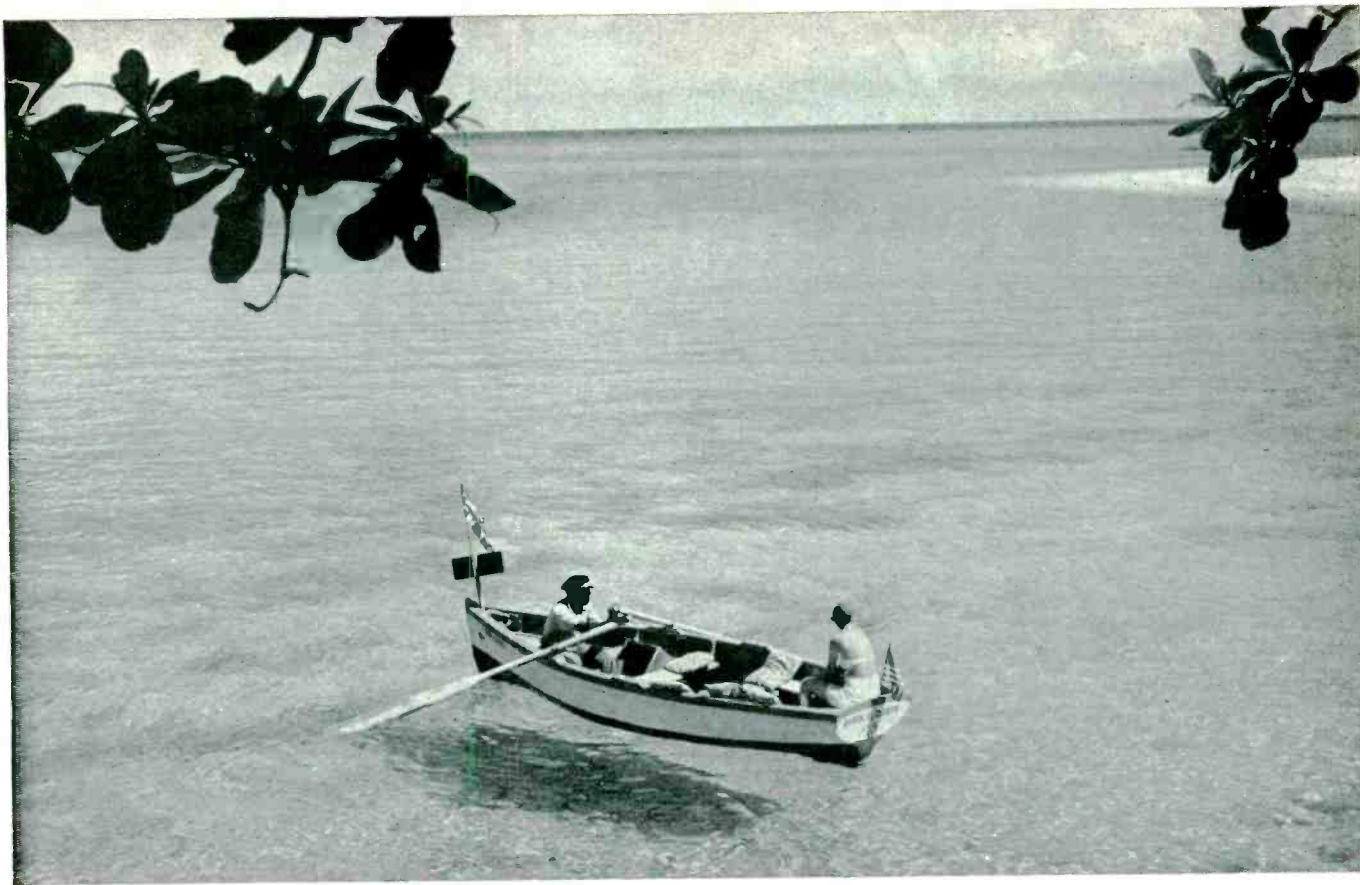


Photo by Earl Leaf from *Guillumette*

out deep... *it's different*

Too bad all the ocean isn't this clear. There'd be no need for complicated under-water detection equipment, no need for constant research and development of depth-finding instruments and sonar equipment such as Edo engineers are working on now.

But as long as the ocean depths can hide their secrets, we'll need better and better eyes and ears with which to see and hear — electronically — what's below. Much is being pioneered along these lines at Edo.

Already Edo equipment, designed and manufactured for the U.S. Navy, makes possible new accuracy in under-water detection techniques.

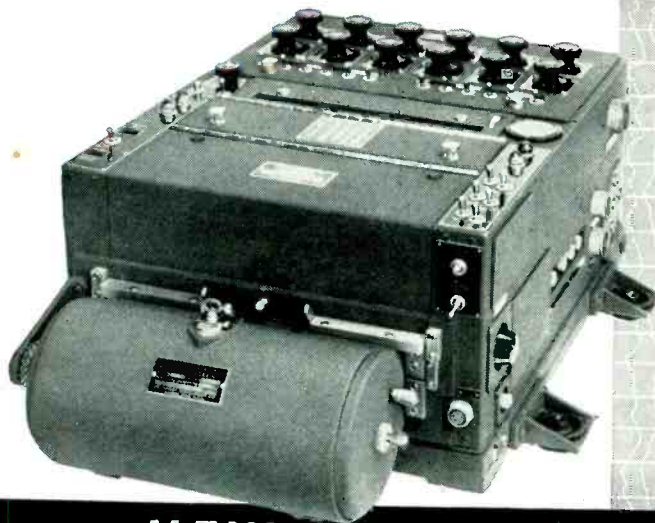
WHO IS EDO?

Twenty five years of research, development and manufacturing experience are behind Edo's work in the electronic field. Founded in 1925, the company first built seaplane floats, later expanded to the design and manufacture of marine aircraft, and built various aircraft components in great quantity during the war. Now to this intimate knowledge of aviation, has been combined top engineering and manufacturing talent in the field of electronics for the design and production of various types of under-water detection equipment.

For a complete picture of Edo's first quarter of a century send for your copy of "Edo's 25th Anniversary" brochure by writing to the Edo Corporation, Dept. M-1, College Point, N. Y.



EDO CORPORATION • COLLEGE POINT, N. Y.



the NEW S-8 Oscilloscope

Here, in a versatile instrument of advanced design, are all the things you need for complete oscillographic recording. The Hathaway Type S-8 Oscilloscope, which has long been the standard of oscillographic recording, has been improved to meet the rapidly expanding demands of modern research. Whether your measurement problems are simple or complex, the NEW Type S-8 Oscilloscope has the inherent capabilities necessary to measure vibration, pressure, acceleration, and strain with new ease and accuracy.

The newest features include:

QUICK-CHANGE TRANSMISSION fully enclosed with gears running in oil to provide instantaneous selection of 16 record speeds over the range of 120:1

CHART TRAVEL INDICATOR provides continuous indication of chart motion. Operator knows instantly by flashing lamp if anything should happen to interfere with chart motion

FULL-RESILIENT MOUNTING FOR MOTOR AND TRANSMISSION isolates all possible vibration and makes possible the use of modern super-sensitive galvanometers

NEW GALVANOMETER STAGE accommodates all Hathaway galvanometer for recording milliamperes, microamperes, or watts

NEW RECORD-LENGTH CONTROL AND NUMBERING SYSTEM designed for long, trouble-free service under all kinds of ambient conditions

All the other valuable features are retained, such as **PRECISION TUNING-FORK-CONTROLLED TIMING SYSTEM** produces either 1/10-second or 1/100-second time lines across sheet

WIDE RANGE OF GALVANOMETER TYPES AND CHARACTERISTICS provide for almost any recording requirements. Natural frequencies to 10,000 cps. Sensitivities to 50,000 mm per ma, single and polyphase watts

DAYLIGHT LOADING AND UNLOADING RECORDS TO 200 FT. IN LENGTH, width to 10 inches

SIMULTANEOUS VIEWING AND RECORDING

AUTOMATIC BRILLIANCY CONTROL

12 TO 92 ELEMENTS

Whatever your needs may be, investigate the NEW Type S-8 Oscilloscope and its 170 types of galvanometers—the most versatile equipment in existence for general-purpose applications.

WRITE FOR BULLETIN 281-A-G

Hathaway
INSTRUMENT COMPANY
 1315 SO. CLARKSON STREET • DENVER 10, COLORADO

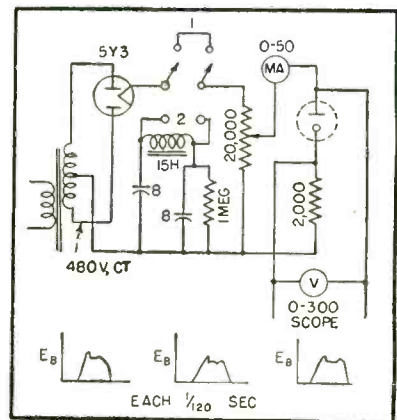
servo which will correct any deviation from the desired value.

The advantage of this new method of measuring sliver uniformity is that it enables accurate measurement to be made without physical contact with the material under examination.

Precision VR Tube Tester

WHEN an unusually constant voltage is desired, careful selection of VR tubes is necessary as these tubes vary noticeably in their operating characteristics. A simple circuit for predetermining the reliability of VR tube performance is shown in the diagram.

Ideally, the voltage drop across the VR tube is constant throughout its rated current range; however, many tubes do not give a uniform



Circuit for testing VR tube over its operating current range

regulating characteristic. Small transients caused by line variations or other reasons result in changes in voltage drop across the tube with consequent changes in regulated output. These results are virtually independent of tube age, and new tubes are sometimes among the worst offenders.

Thus to test VR tubes properly, it is necessary to examine each tube over its entire operating current range, while employing a sensitive detecting device to indicate voltage variations.

The tube selector circuit has been developed by O. B. Rudolph and described in *Rev. Sci. Inst.*, May, 1950. By throwing the switch to position 2, a well-filtered d-c output

they

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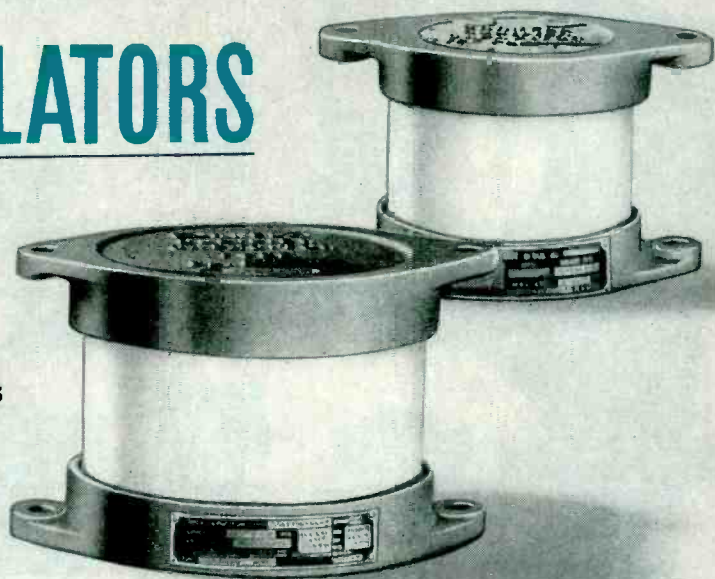
is

only

one

C-D

THE STANDARD IN THE FIELD OF HIGH POWER OSCILLATORS



type 50 series

C-D HIGH POWER MICA TRANSMITTER CAPACITORS

Typical of the many C-D firsts are the type 50 mica capacitors. Only C-D micas can point to a record of dependable service of over forty years. Here's why:

Series mica stack—C-D first to use and patent this construction. Affords uniform voltage gradient!

India-ruby mica—Sheets individually tested for uniform thickness and dielectric strength!

Special exclusive high melting point low loss filler—Reduces stray field losses; protects against humidity!

Vacuum impregnated assembly—Assures high insulation resistance; low losses; eliminates air voids!

High pressure maintained on stacks—Results in high Q; good capacity stability.

Cast-aluminum end caps—Low-resistance, wide-

path, positive-contact terminals for series, parallel or series-parallel connection. Speedy, space-conserving installations!

Every unit tested under long, continuous overload—Assures maximum reliable service.

Type 50 capacitors are available in all commercial capacity and voltage ratings. For complete description of these and Faradon type transmitter capacitors, write for catalog. CORNELL-DUBILIER ELECTRIC CORPORATION, Dept. K-11 South Plainfield, New Jersey. Other plants in New Bedford, Brookline and Worcester, Mass.; Providence, R. I.; Indianapolis, Ind., and subsidiary, The Radiart Corp., Cleveland, Ohio.

C-D Best by Field Test!



CONSISTENTLY DEPENDABLE

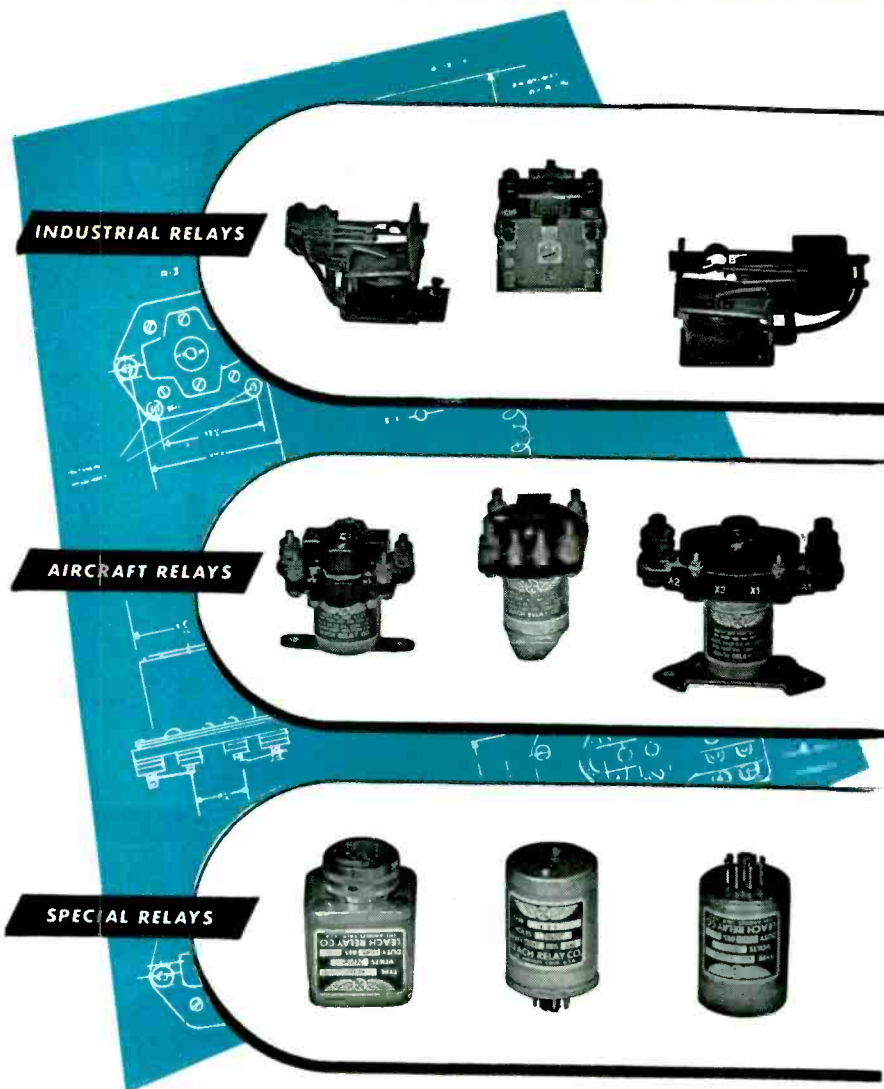
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Leach RELAYS

ARE PERFORMANCE PROVED!



You get better service from LEACH RELAYS because thousands of types of relays for thousands of applications have been proved-in-use for over 30 years.

LEACH RELAYS are designed with an exceptionally high factor of safety for *extra* dependability. Simplicity of designs makes installation quick, easy and inexpensive. Get *all* the facts and make your own comparisons. LEACH RELAYS' outstanding performance, reliability, sturdiness and economy have been *proved-in-use*.

Highest standards of engineering, materials and workmanship assure long, safe, efficient, trouble-free service.

FOR BETTER CONTROLS THROUGH BETTER RELAYS—CONTACT LEACH

LEACH RELAY CO.

8815 AVALON BOULEVARD, * LOS ANGELES 3, CALIF.

Representatives In Principal Cities of U. S. and Canada

TUBES AT WORK

(continued)

will be obtained which can be used for preheating the tube undergoing test if desired and also for checking firing voltage which will be indicated on the voltmeter. With the switch in position 1, pulsating d-c voltage will be applied to the tube for precision checking of the overall voltage-current characteristic. The milliammeter indicates rms current and care should be exercised to prevent the peak value of the current from exceeding 40 ma.

Shown in the illustration are three of the various types of oscilloscope traces which have been obtained from different tubes. The trace at left is ideal and the only one acceptable for many applications.

Television Electronic Pointer

A METHOD for pointing out a person or item in a television picture by means of an electronic pointer has been developed by the General Electric Company.

The new device enables a narrator or commentator to insert a black or white pointer about thirty lines high and seven lines wide at any point in the tv picture.

The equipment consists of a rack-mounted chassis and a simple control unit, a device similar to the control stick of an airplane. A toggle switch selects either a black or white pointer.

The signal input is a noncom-



Operator shown positioning a white pointer by means of the control lever

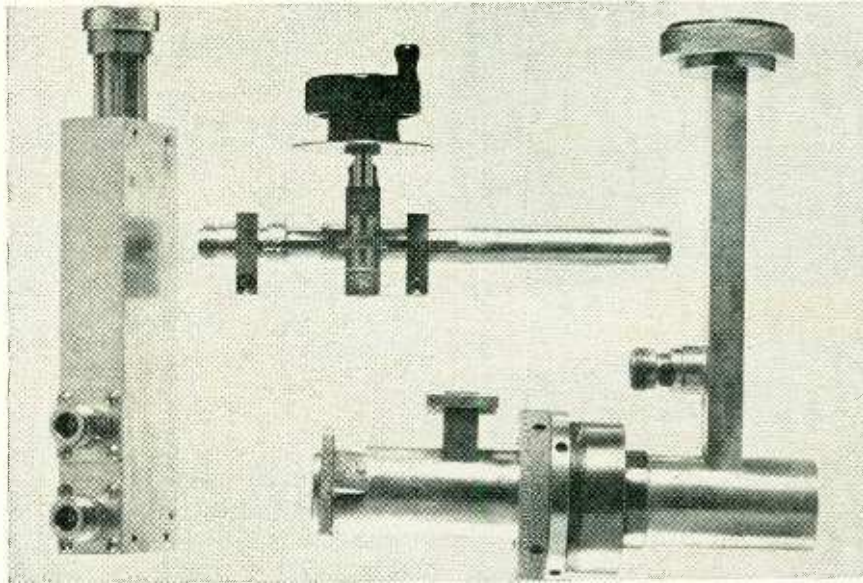


BRIDGEPORT BRASS COMPANY

COPPER ALLOY BULLETIN



MILLS IN BRIDGEPORT, CONN. AND INDIANAPOLIS, IND.—IN CANADA: NORANDA COPPER AND BRASS LIMITED, MONTREAL



Various types of electronic components manufactured from brass: left, line stretcher; center, piston-type, cutoff attenuator; right, rotating joint. Diamond Manufacturing Co., Wakefield, Mass.

Accuracy of Electronic Components Increased by Brass and Bronze

Copper-base alloys in rod, strip, sheet, wire and tube form are the backbone of the manufacture of electronic components such as crystal mixers, attenuators, rotating joints, line stretchers, antennas, R. F. coaxial connectors and numerous other items.

Accurate dimensions and highly polished surfaces are essential for microwave test equipment and plumbing components. Copper alloys can be both machined or drawn to these exacting demands.

Plating Essential

All parts are either silver or gold plated for electrical conductivity and protection from corrosion. The majority of the copper alloys can be plated cleanly and with a minimum of work. They hold their plate for long periods of time without scaling.

All types of machining operations are necessary in producing this precision equipment. For example, the illustrated line stretcher is made up of a number of screw machine parts from free turning brass rod. The body is also rectangular rod of the same alloy. Drill-

ing, tapping, milling, polishing, plating, silver soldering are involved in producing this component.

Any type of corrosion changes the electrical characteristics of these units. Brass and bronze are both resistant to atmospheric corrosion. Some of these units are used in the open, especially those linking up antennas and in radar and other communication equipment.

Close Fits Needed

On sliding parts and mating surfaces used as bearings, the parts must be fitted closely enough to eliminate any play which would affect the characteristics of the unit. This is also true of mating threads.

Spring contact units are made from phosphor bronze, grade A, to reduce wear and fatigue dangers.

Since plating is essential for protection purposes, mating parts in tubular construction are sometimes plated with nickel and chrome to obtain a better bearing with the silver plated part through the difference in the coefficient of friction.

Brass Smooths Action of Resistor

Smooth action, ability to withstand wear and corrosion in all types of weather conditions, are essential in variable resistance units used in television, radio and other electronic work.

Copper-base alloys answer these demands. Through the excellent machinability of free cutting brass rod, the threaded guide bushing can be held accurately to take the shaft with a minimum of play. At the same time the leaded brass makes a good bearing surface for smooth action.

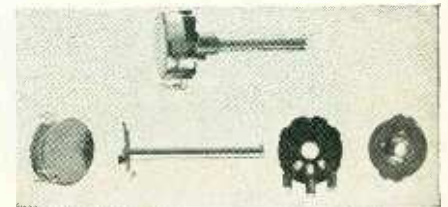
The bushing plate is leaded clock brass (62.25% copper, 2% lead and the remainder zinc). Clean blanking and piercing are possible with this alloy and in hard temper it has a tensile strength better than 70,000 psi.

Copper soldering terminal lugs are used both for conductivity and ease of tinning, and they are held into the body with hollow rivets made from cartridge brass, which has high ductility.

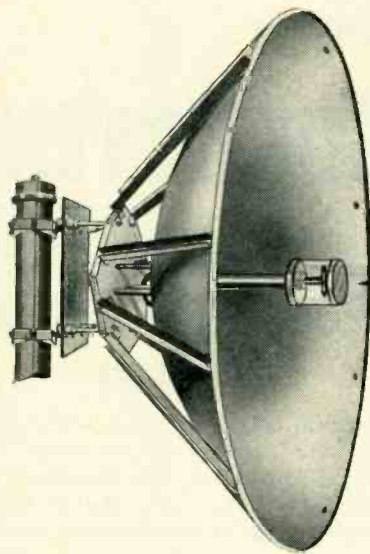
Both spring contact terminals, one which rides on the carbon impregnated resistance strip and the other against it, are made from phosphor bronze grade A (95% copper, 5% tin). This alloy has excellent spring characteristics and great resistance to fatigue from constant flexing.

A fixed pressure of the contact must be maintained on the resistance strip to insure a good electrical connection. Variations in this pressure would seriously affect the operation of the television, radio and similar electronic devices.

The shaft is also of free-cutting brass rod which simplifies the machining and the milling of the flat and tangs. (6154)



Variable resistor and component parts used in electronic work — Courtesy Clarostat Mfg. Co., Inc., Dover, N. H.



WHAT ARE *Your* REQUIREMENTS IN PARABOLIC ANTENNAS ?

For microwave systems . . . check these advantages of ANDREW Parabolic Antennas:

- DEPENDABILITY** — An actual record of 100% dependability. There has never been a single mechanical or electrical failure on an ANDREW Parabolic Antenna . . . anywhere in the world.
- COST** — Exceptionally low; made possible by high production.
- LIGHT WEIGHT — HIGH STRENGTH** — Achieved by spun aluminum reflectors braced by formed steel struts.
- ADJUSTABLE MOUNTING** — Through ± 10 degrees in azimuth and elevation.
- DEICING KITS** — Thermostatically controlled, available where required.
- CABLE** — $\frac{7}{8}$ " air dielectric Teflon insulated cable. Radiator is pressure tight. Fittings for solid dielectric cables also available.

SPECIFICATIONS

Frequency Range	. . . 890-960 MCS 1750-2110 MCS . . .			
	1002	1004	1006	1010	2002	2004	2006	2010
Type Number	1002	1004	1006	1010	2002	2004	2006	2010
Diameter of Parabola feet	2	4	6	10	2	4	6	10
Gain Over Half Wave Dipole Decibels	10	15	20	25	15	20	25	29
Beam Width, Half Power Points, Degrees	36°	22°	16°	11°	18°	10°	7°	5°
Net Weight, Pounds	10	64	150	380	10	65	150	380
Thrust Due to Wind Loading at 30 Pounds/FT Pounds	127	509	1145	3200	127	509	1145	3200

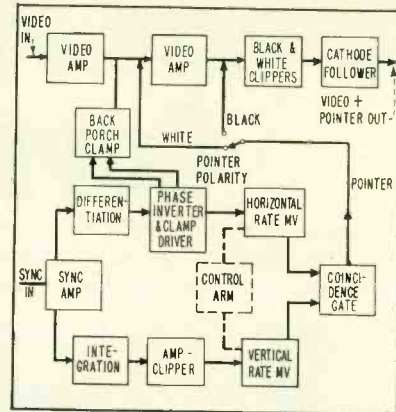


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Block diagram for the circuit enabling a black or white pointer to be inserted in the tv picture

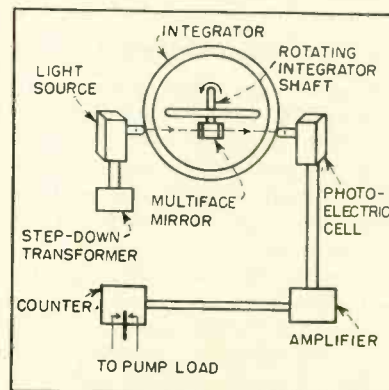
posite black-negative video, 0.5 to 2 volts peak to peak and 75 ohms. The separate sync signal is negative, 3 to 8 volts and of high impedance.

Batch Integrator

A NEW batch-type integrator accurately establishes a predetermined quantity of fluid by making or breaking an electrical contact when the desired amount or batch has been integrated.

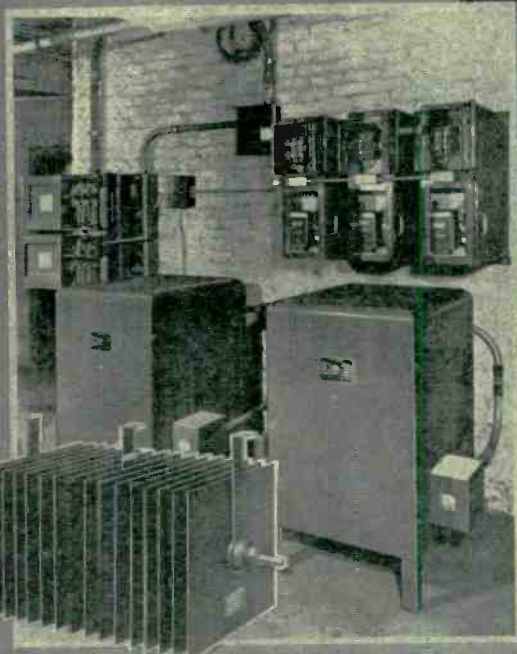
The control function is accomplished by using a photoelectric pickup unit that responds to reflections of a light beam from a multi-face mirror mounted on the rotating integrator shaft and an electric predetermined reset counter. The counter may be set for any desired quantity or batch of fluid.

The electric counter is set for the desired quantity and the process started by depressing the momentary contact button which energizes the pump circuit or other apparatus



Working drawing of the batch integrator control

HOW SELETRON RECTIFIERS GAVE CHICAGO A LIFT



PARTIAL LIST OF ELEVATOR INSTALLATIONS USING SELETRON RECTIFIERS IN THE CHICAGO AREA

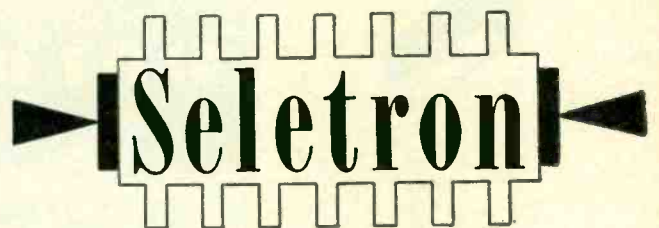
BUILDING	NO. OF RECTIFIERS	APPROX. NC OF ELEVATORS
Drake Hotel Towers, 179 E. Lake Shore Dr.	4 ea. 15 KW	6
Garden City Building, 1750 N. Ashland Ave.	2 ea. 10 KW	2
Jewish Charities, 241 S. Wells	2 ea. 20 KW	3
1356 North Dearborn Building	3 ea. 27 1/2 KW	4
60 E. Scott Street Building	2 ea. 14 KW	2
Bernstein Building, 74 S. Clinton	2 ea. 10 KW	2
Bush Temple, 303 North Clark	2 ea. 20 KW	3
Clinton Realty 522 E. Clinton	1 ea. 20 KW 1 ea. 14 KW 1 ea. 15 KW	4
Lansing Hotel, 1036 N. Dearborn	2 ea. 20 KW	2
Plaza Hotel, 155 W. Clark	3 ea. 10 KW	3
Sears & Roebuck Co., 312 N. May	3 ea. 25 KW	2
Cowman Club, 10 North Dearborn	2 ea. 20 KW	3
Churchill Apts., 1264 North State	2 ea. 17 KW	2
Western Elec. Bldg., 1736 S. Wabash	2 ea. 10 KW	2
70 East Cedar	2 ea. 14 KW	3
Michael Reese Hospital	4 ea. 50 KW	10
Stainway Drug Bldg.	1 ea. 10 KW	3
Graphic Arts Bldg.	4 ea. 25 KW	6
Watson Motors	2 ea. 20 KW	2
Chicagoan Hotel	2 ea. 27 1/2 KW	4
1220 North State Building	2 ea. 40 KW	4
Canterbury Apts.	2 ea. 14 KW	3
241 Van Buren Street Building	2 ea. 20 KW	3
Superior Elevator Co.	ea. 7 KW	1
245 E. Walton Building	ea. 7 KW	1
Clinton Machine Co.	3 ea. 10 KW	2
Western Electric Building	2 ea. 20 KW ea. 14 KW ea. 10 KW	6
Guzzola Drug Company	ea. 10 KW	1
A. Rubloff Building	2 ea. 14 KW	4
Goldenberg Furniture Company	ea. 10 KW	1
210 E. Pearson Street Building	3 ea. 20 KW	4
Illinois Electrolite	ea. 20 KW	2
Car Service Company	4 ea. 20 KW	4
SL Clair Hotel	4 ea. 25 KW	5
Eastgate Hotel	4 ea. 25 KW	4

WHEN THE POWER COMPANY changed over to alternating current in certain Chicago areas it meant that existing elevators operating on D.C. had to be converted fast, or the good people of the town would be "grounded."

Ther Electric & Machine Works of Chicago solved elevator rectification problems for considerably more than 100 famous buildings in the Windy City by designing complete power supply and regenerative braking equipment employing SELETRON rectifiers. The illustration shows a typical 3 bank unit with regenerative control, built for the Clinton Realty Co.

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SELETRON DIVISION

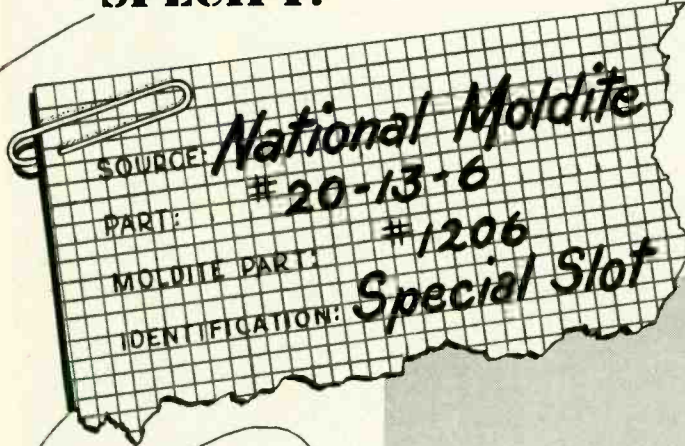
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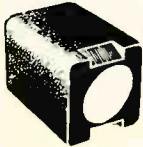
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that starts the flow of fluid.

An electric meter measures the flow and supplies a proportional current to the watt-hour type of continuous electric integrator. Speed of rotation of the integrator shaft is a direct measure of the rate of flow. Each revolution corresponds to a definite quantity of flow.

The counting is done by the photoelectric cell picking up the number of reflections of the light source from the rotating multiface mirror. As soon as the desired batch has been integrated the pump circuit is deenergized by the counter which then automatically resets itself. The process may then be repeated for the same batch or a new batch setting.

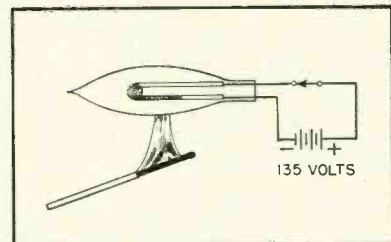
The electric counter will register up to 150 counts per minute. The maximum speed of the revolving integrator shaft, corresponding to maximum flow, is 25 rpm.

For a given calibration of the integrator, the range of batch control is varied by changing the number of faces (from one to six) of the revolving mirror. The instrument is manufactured by the Republic Flow Meters Co. of Chicago, Ill.

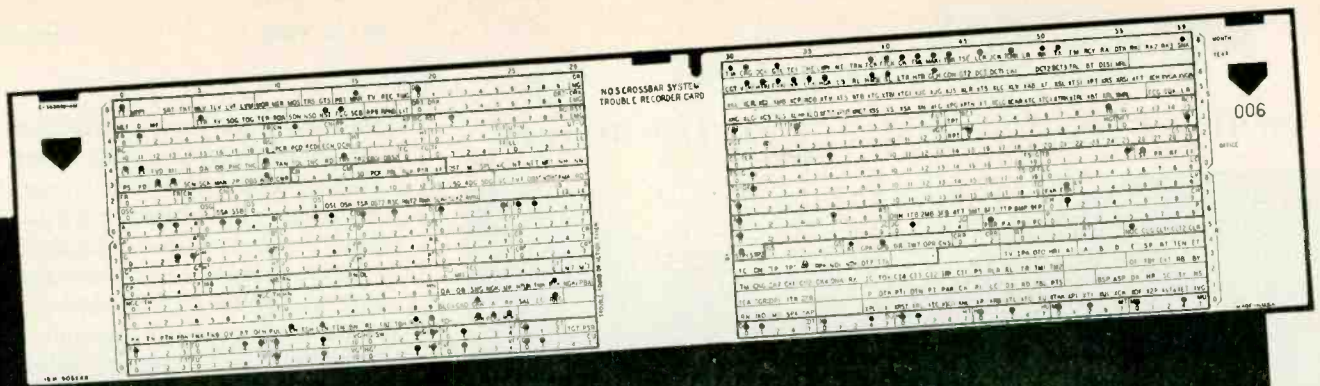
Novel Application for Neon Diodes

BY IRVING GOTTLIEB
*Electrical Engineer
Los Angeles, California*

A NEON BULB, connected as a relaxation oscillator, will function as a light-sensitive device, the response being a change in frequency when the illumination is changed. This phenomenon is ordinarily of no significance with respect to the



The luminous gas which uniformly surrounds the negative electrode before application of heat gradually collects as a brilliant ball of glowing gas in the end region of the electrodes



Another reason why your telephone gives so much for so little



Studying punched card record of dial system operation. Each card (top) can report 1080 items

In a large, modern dial telephone office, 2,000,000 switch contacts await the orders of your dial—and 10,000 of them may be needed to clear a path for your voice when you make a single telephone call. Within this maze of signal paths, faults—though infrequent—must be detected and fixed before they can impair telephone service.

The latest system developed by Bell Telephone Laboratories automatically detects its own faults, detours calls around them without delay—then makes out a “written” report on what happened.

The fault may be a broken wire, or a high resistance caused by specks of dirt on switch contacts. In one second, the trouble recorder punches out a card, noting in detail the circuits involved and the stage in the switching operation where the fault appeared.

Maintenance men examine the reports at intervals and learn what needs attention. Between times they go about their own duties in keeping service moving.

This is another example of how research at Bell Laboratories helps your telephone system operate at top efficiency, so the cost to you stays low.

BELL TELEPHONE LABORATORIES



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PRESTO...most carefully made recording discs in the world



step 4 - Inspection is important

Surface reflections in a recording disc can tell more than volumes to the skilled eye. That's why no mechanical test has ever replaced the examination of each PRESTO disc by trained inspectors.

Under a bank of fluorescent lamps diffused by a special glass screen, discs are slowly rotated. A ripple, a fleck in the brilliant surface automatically grades the disc. Only those passing the most critical surface test are allowed to carry the PRESTO "Green Label."

Rigid inspection of discs is further insurance that your instantaneous or master recording will produce full tonal quality, that it will react properly under recording, processing and playback conditions. This important fourth step in the manufacture of PRESTOS is another reason why they are known throughout the world as the most carefully-made, most permanent, best performing discs available.



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New York, New York

TUBES AT WORK

(continued)

usual applications of relaxation oscillators and escapes observation.

Interesting experiments can be conducted to detect frequency changes under various conditions of exposure to light. This little-known cause and effect relationship can be greatly enhanced by means of a "treatment", the result being a photoelectric transponder which behaves in an unusual and fascinating manner.

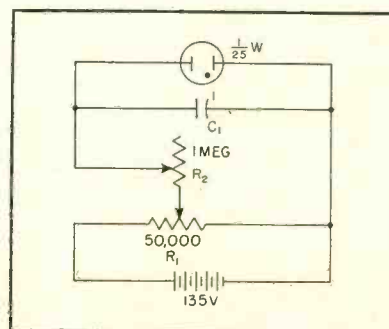
It will be shown that a neon bulb can be caused to flash during exposure to light but will be entirely inactive in darkness. In addition, the converse mode of operation can be demonstrated; the bulb can be caused to flash in the dark and be rendered inactive by illumination.

The foregoing experiments were performed with the small 1/25-watt butterfly-type bulb.

The sensitizing treatment consists of applying the flame of a match while the bulb is being energized by 135 volts. The bulb should be held in a horizontal position and the flame should be restricted as much as possible to the area of the glass immediately below the glowing electrode. A piece of window glass, a wire screen, or some other precautionary measure should be used to protect the eyes from possible explosion.

After a few seconds, the glowing gas will collect as a brilliant incandescent ball at the end of the electrodes. Just how long the heat should be continued to be applied after this occurs will have to be determined experimentally.

The circuit shown is that of a conventional relaxation oscillator. However, it is important to shield



Relaxation oscillator circuit for the photoelectric experiments

New 1951 • • MODEL V-4A

Heathkit VTVM KIT

HAS EVERY EXPENSIVE Feature

- ★ Higher AC input impedance, (greater than 1 megohm at 1000 cycles).
- ★ New AC voltmeter flat within 1 db 20 cycles to 2 megacycles (600 ohm source).
- ★ New accessory probe (extra) extends DC range to 30,000 Volts.
- ★ New high quality Simpson 200 microampere meter.
- ★ New ½% voltage divider resistors (finest available).
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- ★ Largest scale available on streamline 4½ inch meter.
- ★ Burn-out proof meter circuit.
- ★ Isolated probe for dynamic testing no circuit loading.
- ★ New simplified switches for easy assembly.



New
LOW PRICE **\$23.50**

The new Heathkit Model V-4A VTVM Kit measures to 30,000 Volts DC and 250 megacycles with accessory probes — think of it, all in one electronic instrument more useful than ever before. The AC voltmeter is so flat and extended in its response it eliminates the need for separate expensive AC VTVM's. + or - db from 20 cycles to 2 megacycles. Meter has decibel ranges for direct reading. New zero center on meter scale for quick FM alignment.

There are six complete ranges for each function. Four functions give total of 24 ranges. The 3 Volt range allows 33⅓% of the scale for reading one volt as against only 20% of the scale on 5 Volt types.

The ranges decade for quick reading.

New ½% ceramic precision are the most accurate commercial resistors available — you find the same make and quality in the finest laboratory equipment selling for thousands of dollars. The entire voltage divider decade uses these ½% resistors.

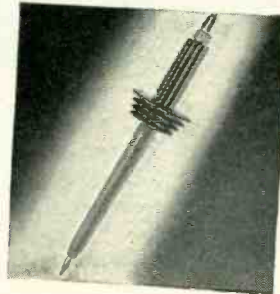
New 200 microampere 4½" streamline meter with Simpson quality movement. Five times as sensitive as commonly used 1 MA meters.

Shatterproof plastic meter face for maximum protection. Both AC and DC voltmeter use push-pull electronic voltmeter circuit with burn-out proof meter circuit.

Electronic ohmmeter circuit measures resistance over the amazing range of 1/10 ohm to one billion ohms all with internal 3 Volt battery. Ohmmeter batteries mount on the chassis in snap-in mounting for easy replacement.

Voltage ranges are full scale 3 Volts, 10 Volts, 30 Volts, 100 Volts, 300 Volts, 1000 Volts. Complete decading coverage without gaps.

The DC probe is isolated for dynamic measurements. Negligible circuit loading. Gets the accurate reading without disturbing the operation of the instrument under test. Kit comes complete, cabinet, transformer, Simpson meter, test leads, complete assembly and instruction manual. Compare it with all others and you will buy a Heathkit. Model V-4A. Shipping Wt., 8 lbs. Note new low price, \$23.50.



New 30,000 VOLT DC PROBE KIT

Beautiful new red and black plastic high voltage probe. Increases input resistance to 1100 megohms, reads 30,000 Volts on 300 Volt range. High input impedance for minimum loading of weak television voltages. Has large plastic insulator rings between handle and point for maximum safety. Comes complete with PL55 type plug.

No. 3366 High Voltage Probe Kit.
Shipping Wt., 2 pounds.

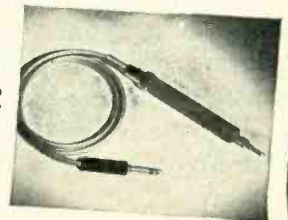
\$550

Heathkit RF PROBE KIT

Crystal diode probe kit extends range to 250 megacycles = 10% comes complete with all parts, crystal, cable and PL55 type plug.

No. 309 RF Probe Kit.
Shipping Wt., 1 lb.

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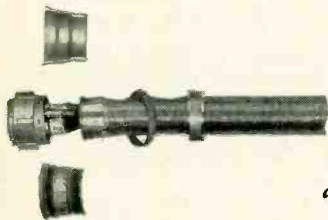
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Contacts, precision-machined from solid bar stock, electroplated with silver or gold.

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Type AN Connectors are made in 6 styles; straight and 90° cord plugs; box, wall, and extension cord receptacles; and special quick disconnect plugs. Fifteen diameters for inserts with contact arrangements from single to 100 contacts. Contact capacities from 5 to 200 amps. Peak voltages from 70 to 9,000 volts.



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the apparatus to prevent r-f pickup from broadcast stations. A surprisingly small amount of r-f pickup will serve to foul up the demonstration. Capacitor C_1 is a pyranol or other low-leakage type, conventional paper types are not suitable.

Clean the bulb with carbon tetrachloride and solder the wire leads to hook-up wire in such a manner to provide a minimum clearance between the bulb and other objects of four inches. For the initial testing, a 60-watt lamp should be located about five feet from the neon bulb. With the lamp off, the room should be completely dark.

Initial Adjustments

With the lamp turned on, adjust R_1 and R_2 until a flashing rate of approximately one flash per second is obtained. Next, find that setting of R_1 which barely allows the neon bulb to flash. If the flashing frequency is now greatly different from the suggested one-per-second rate, readjust R_2 .

Turn off the sixty watt lamp. One of three things will happen; the neon bulb will cease flashing, it will flash at a noticeably greater frequency, or there will be no discernible effect.

If the flash rate increases, reverse the battery polarity and repeat the adjustment procedure. This will result in the first effect. Once the neon bulb has displayed photoelectric sensitivity by virtue of the first or second effects, a flashlight may be substituted for the lamp. By finer adjustment of the potentiometers, it should be possible to trigger the neon bulb from a distance of at least thirty feet with a flashlight beam.

If it is desired to extinguish the flashing by means of a light beam, then the second effect is the proper mode of operation. The threshold adjustment of R_1 should in this case be made in total darkness rather than under 60-watt lamp exposure.

If no photoelectric effect is perceptible, try another neon bulb which was subjected to greater or less heat treatment. The writer, after considerable experimentation, has not been able to develop a better sensitizing method. The treatment

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14 kc to 1000 mc!

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15 MC
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400 MC
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Commercial equivalent of TS-587/U.
Sensitivity as two-terminal voltmeter, (95 ohms balanced)
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intensity measurements using calibrated dipole. Frequency
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A new achievement in sensitivity! Field intensity measure-
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Self-contained batteries. A.C. supply optional. Sensitivity as
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meter rod antenna, 2 microvolts-per-meter; rotatable loop
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UHF!
375 MC
to
1000 MC
NM - 50A

Commercial equivalent of AN/URM-17.
Sensitivity as two-terminal voltmeter, (50-ohm coaxial input)
10 microvolts. Field intensity measurements using calibrated
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Since 1944 Stoddart RI-FI* instruments have established the
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These instruments fully comply with test equipment require-
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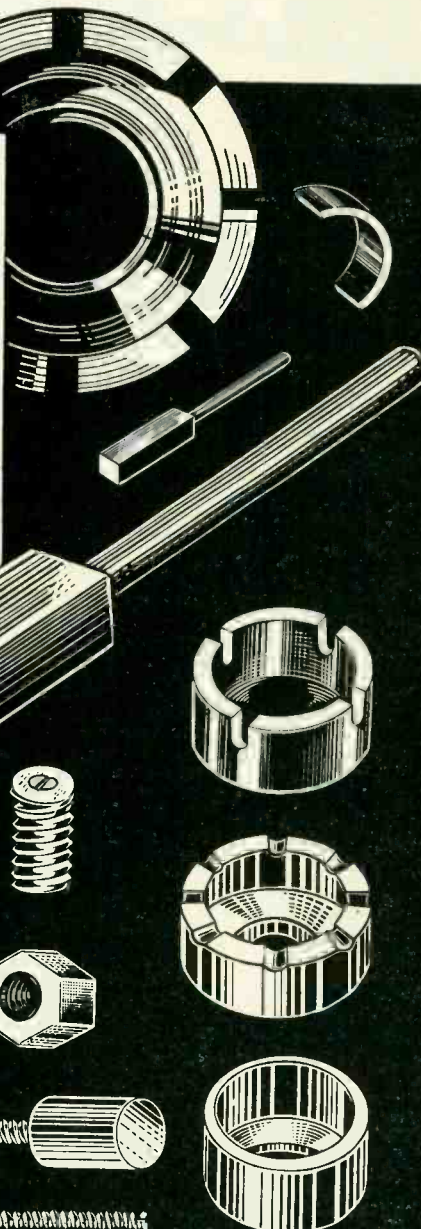
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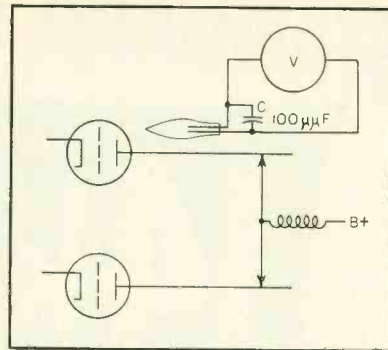
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Circuit for using neon bulb as a d-c source when exposed to r-f radiation. Capacitor C is connected at the terminals of the bulb

evidently makes one electrode more photoemissive than the other.

Another interesting property of gaseous diodes involves the generation of a d-c emf when the gas is ionized by external radiation. A four-watt 150-mc self-excited oscillator is employed to supply the radiant energy. It is not necessary to treat the neon bulb for this demonstration. It is only essential that the center of the induced ionization is closer to one electrode than the other.

Readings as high as ten volts on a 5,000-ohm-per-volt meter are obtainable. The polarity of this emf is determined by the electrode which is closest to the mass of glowing gas. As with the photoelectric experiment, one electrode assumes the role of anode while its mate functions as the cathode.

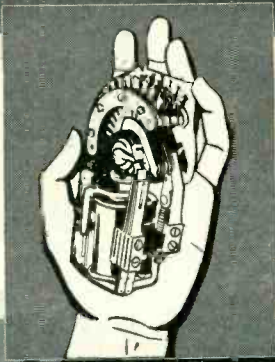
The 2050 thyatron also works well in this capacity. It is unnecessary to heat the filament; the screen and cathode seem to be the best pair of electrodes to use.

A gaseous diode mounted near a tank or antenna circuit could be used as a power-indicating device and should be particularly well suited for certain microwave techniques. For such and similar applications, the gaseous diode will be found a more rugged device than a crystal which is susceptible to erratic changes and burnout from r-f currents often induced by stray pickup.

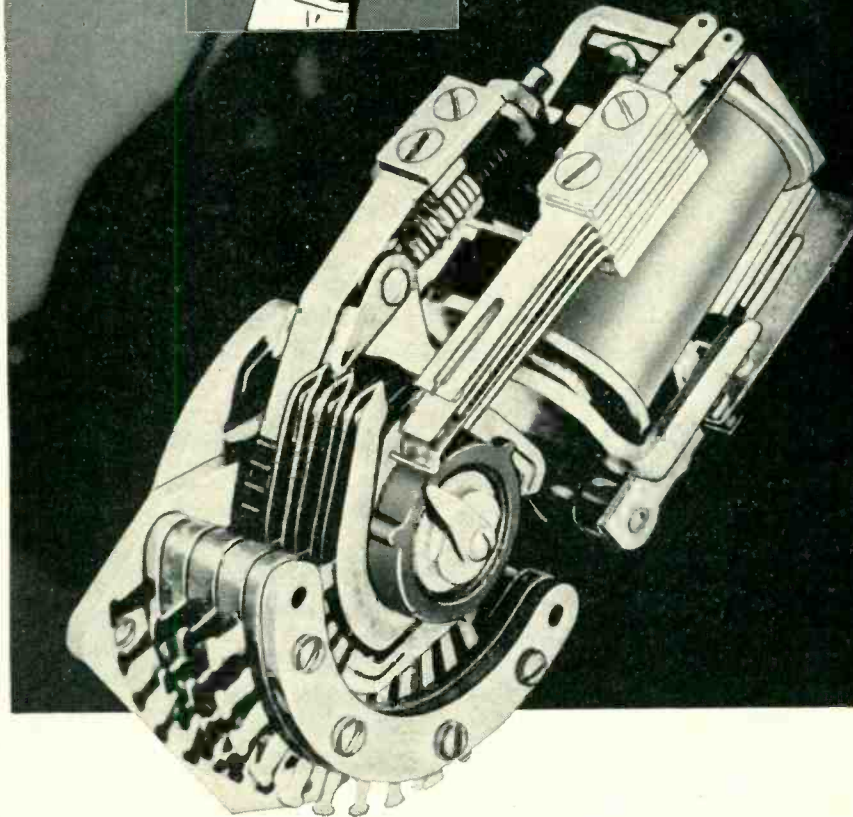
Sine and Square Wave Generator Selective Amplifier

THE ARTICLE with the above title appeared in the December, 1950, issue of ELECTRONICS. Through an

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Up to 6 Levels — 10-point plus home; yet it's Smaller Than Your Hand! Only $4\frac{1}{2}$ inches long — and about half that wide — Automatic Electric's new stepping switch averages only $13\frac{1}{2}$ ounces in weight. Yet it gives you *more* than other larger switches.

It's speedy . . . a typical three-level 10-point switch, at 48 volts D. C., self-interrupted, runs approximately 80 steps a second — impulse controlled, at 35 steps a second.

It's smoother . . . brush springs are in an "11th" position; wipers pass over them exactly as over bank contacts. No double load in any position — no "galloping."

It assures long life . . . smooth operation means longer life; in addition, all driving parts are especially armored against wear. In rigid laboratory tests, Type 44 Stepping Switches averaged 20,000,000 operating

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It's adaptable . . . meets your specific needs with a wide range of coils (for any D. C. voltage up to 110), bank levels, bridging and non-bridging wipers, interrupter springs and off-normal springs.

The Type 44 Stepping Switch has *less* weight — takes *less* space — and gives you *more* of everything else! Get complete data NOW on this revolutionary new switch. Call, wire, or write AUTOMATIC ELECTRIC SALES CORPORATION, 1033 W. Van Buren St., Chicago 7, Ill. In Canada: Automatic Electric (Canada) Limited, Toronto.

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TUBES AT WORK

(continued)



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- ✓ **LIFE EXPECTANCY** Extensive tests indicate that the life expectancy of Hornet units at continuous winding temperatures of 200 deg. C. is over 50,000 hours.
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- ✓ **EFFICIENCY** Regulation and efficiency of Hornet Transformers compare favorably with Class A units.
- ✓ **SPECIFICATIONS** Hornet Transformers meet the requirements of Government specifications covering this type of equipment.



Bulletin B300, containing full electrical and dimensional data on Hornet units, is now available. Write for it, or tell us your specifications for special units.



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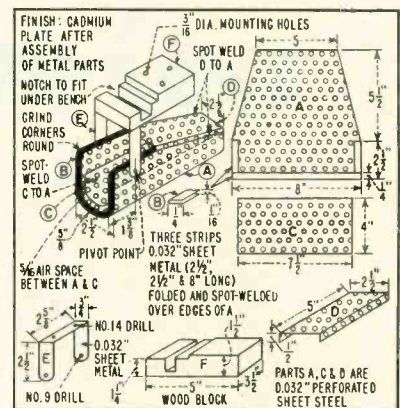
oversight credit was not given the author for his circuit design and analysis. The article should have carried a by-line crediting George Ellis Jones, Jr., Department of Chemical Engineering, The University of Pittsburgh, Pittsburgh, Pennsylvania.

SHOP SHORTCUTS

VOLTMETERS and milliammeters cannot be used for measuring accurately the output of a pentode tube in a circuit because of the high value of the pentode plate resistor. If a 0-150-volt electrostatic voltmeter is placed across the plate resistor, it will not draw any current and, consequently, will not load the plate circuit.

*Fred Lichtgarn
Chicago, Ill.*

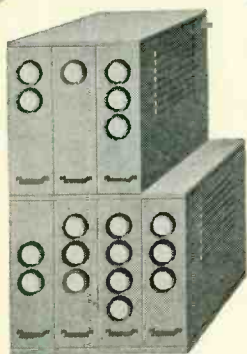
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the iron in this position, the heat rises up and away from the handle and the operator. A large fibre washer prevents the iron from sliding out the back of the holster. The line cord is kept out of the operator's way by being connected to an overhead outlet.

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(continued from page 126)

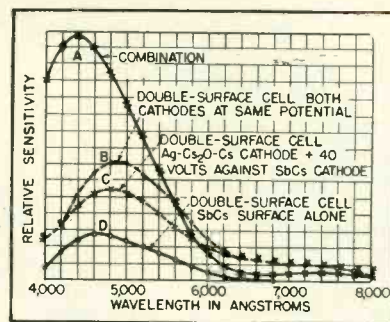


FIG. 3—Response of various types of phototubes including suggested combination unit

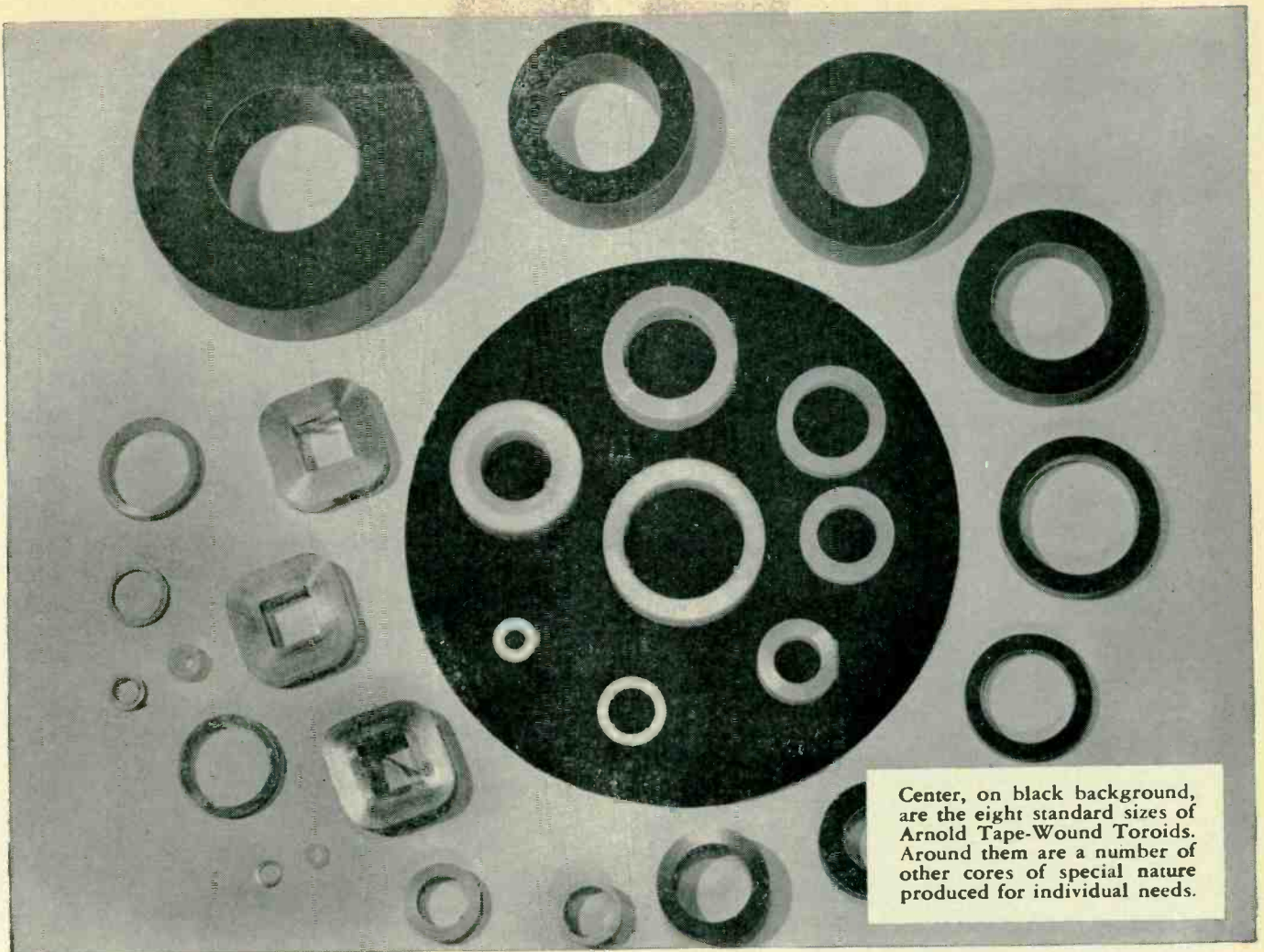
and curve A shows the combined response of two photoemissive tubes, one with a semitransparent Sb-Cs surface, the other with a Ag-Cs₂O-Cs surface placed one behind the other, the light shining on and through the Sb-Cs cathode. The use of a more transparent Sb-Cs surface would give a more uniform response throughout the spectrum.

“Although the double surface tube shows all the expected features, it does not seem practical as compared to the combination of two suitably-selected separate tubes. The conditions in a single tube are rather complicated and depend greatly on the geometry of the tube, the processing of the cathodes, and on the relative voltages applied to both cathodes and the anode. Two separate tubes could be processed more readily to maximum sensitivity of each surface and there would be no secondary emission to affect the Ag-Cs₂O-Cs surface.”

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Arnold Tape-Wound Toroids are available in eight sizes of standard cores—all furnished encased in molded nylon containers, and ranging in size from 1/2" to 2 1/2" I.D., 3/4" to 3" O.D., and 1/8" to 1/2" high.

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In addition to the standard toroids described at left, Arnold Tape-Wound Cores are available in special sizes manufactured to meet your requirements—toroidal, rectangular or square. Toroidal cores are supplied in protective cases.

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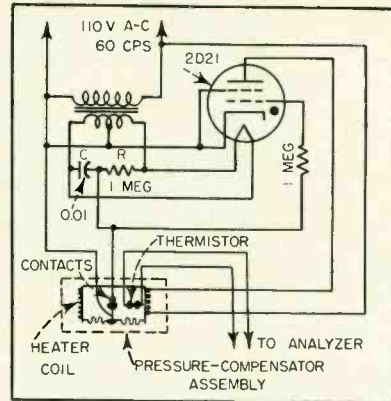
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Simple thyatron circuit for use with novel pressure-measuring unit

chamber exceeds the pressure of the gas within the chamber. A pair of electrical contacts are arranged so that a heater circuit is closed whenever the outside pressure presses the diaphragm inward. This heater circuit causes the gas in the chamber to expand, until it equals the pressure outside the chamber, at which time the heater contacts open. The temperature is thus held at some point where the pressure of the gas equals outside pressure.

A thermistor, also placed inside the chamber, along with the gas and heater contacts, can be used to measure the average temperature of the gas, and thus to determine the pressure of the gas by means of a calibration chart. The circuit of an instrument using this pressure-measuring device is shown in the illustration. According to Edward C. Blom, who describes this instrument in detail in *Instruments* (p 903, Sept. 1950), a model using this circuit has been in use over two years. The only maintenance required is the replacement of the thyatron once every six months or so.

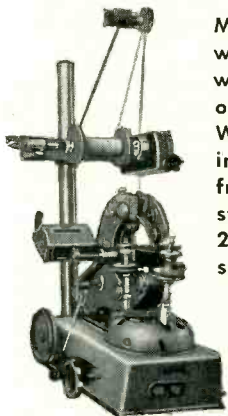
Resistance-Coupled Amplifier Bandwidth

B. A. LIPPMANN
Nucleonics Division
Naval Research Laboratory
Washington, D. C.

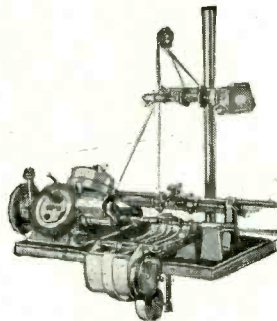
THE PRACTICE of examining the behavior of resistive amplifier coupling networks by an approximate method of analysis has apparently obscured the fact that the gain characteristic of this circuit is exactly equivalent to a single-tuned

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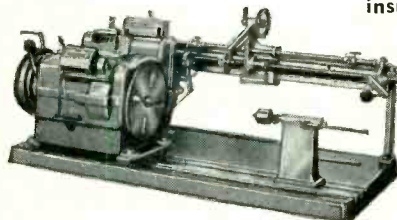


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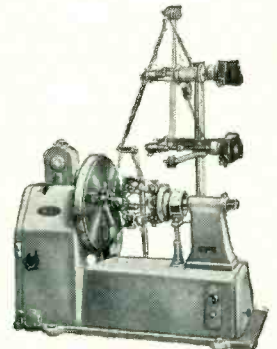


MODEL OOFA AUTOMATIC FINE-WIRE WINDER with removable semi or fully automatic paper interleaving attachment. Will wind wires from 24 to 44 AWG at certain speed ranges between 950 and 6000 RPM. Attachment available for winding two coils simultaneously. **MODEL OOFA-T**, similar to above, winds up to 12,000 RPM.

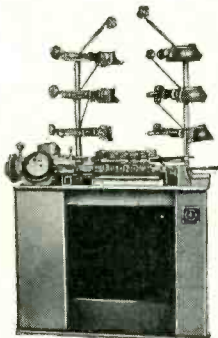
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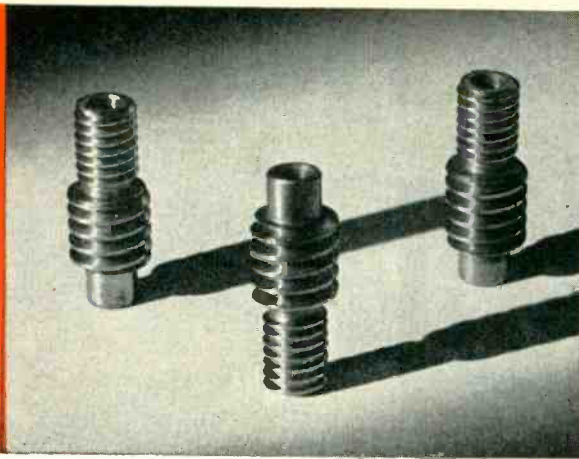


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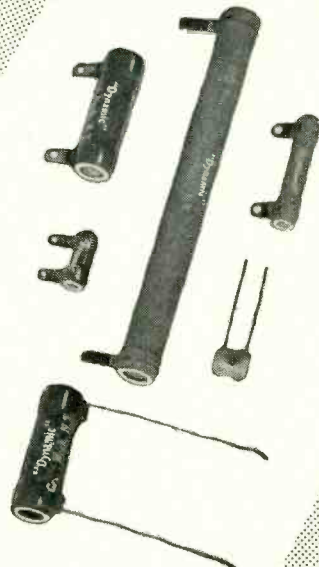
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circuit. In this article, the equivalence will be proved.

The standard uncompensated resistive coupling network takes the form shown in Fig. 1, where C_1 and C_2 include the tube and wiring capacitances, R_1 is the resultant of the load resistance and the plate resistance of the first tube taken as a parallel combination, and C_m is the coupling capacitor. Ordinarily, $C_m \gg C_1$ and $C_m \gg C_2$. Where approximate formulas are given, we shall understand them to refer to this condition.

The conventional analysis proceeds by examining the limiting forms the circuit takes at low, medium and high frequencies. For example, at low frequencies C_1 and C_2 are considered negligible and the voltage gain G is determined by considering the voltage divider formed by C_m and R_2 in series. The grid voltage on the second tube is $R_2[R_2 + 1/j\omega C_m]^{-1}$ times the plate voltage on the first tube. Using g for the transconductance of the first tube, its plate voltage is

$$-gR_1 \left(R_2 + \frac{1}{j\omega C_m} \right) / \left(R_1 + R_2 + \frac{1}{j\omega C_m} \right)$$

times the input voltage. The gain G is therefore given by

$$G = \frac{-gR_1 R_2}{R_1 + R_2 + 1/j\omega C_m}$$

so that the low-frequency 3-db

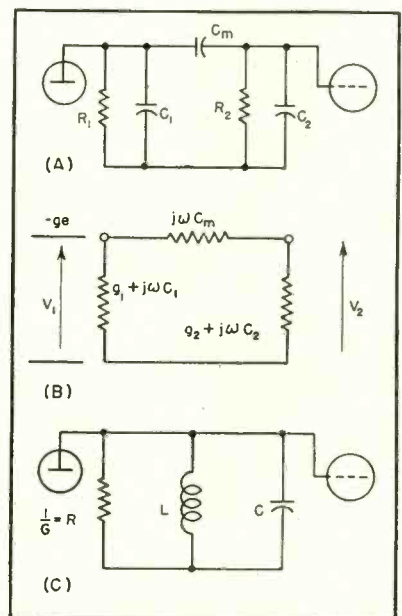


FIG. 1—Resistance-coupled circuit and equivalent

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laboratory work.

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11 megacycles. Sensitivity is 0.7 peak-to-peak volt per inch. Pulse response is such that a rise time of 0.01 microsecond will be reproduced as a rise time of 0.04 microsecond or less.

Crystal-controlled timing markers are provided in the Type 256-D for calibration of the delay circuit sweeps. Both delayed and undelayed sweeps may be started by external trigger pulses of either polarity or by a built-in trigger generator which provides 1-microsecond pulses of either polarity, having a rise time of 0.3 microsecond and amplitude greater than 100 volts. Trigger repetition rates up to 2000 P.P.S. are usable.

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Current	105 milliamperes	130 milliamperes	155 milliamperes
Power	0.90 watts	1.4 watts	1.9 watts
Impedance	85 + j240 ohms	80 + j180 ohms	77 + j149 ohms
OUTPUT			
Voltage max. (rotor output)	18.0 volts	15.5 volts	13.3 volts
Voltage at null	30 millivolts	20 millivolts	20 millivolts
Sensitivity	315 millivolts/degree	270 millivolts/degree	230 millivolts/degree
Voltage phase shift	18.5 degrees	24.5 degrees	28.0 degrees
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point is

$$\omega_1 = 2\pi f_1 = 1/(R_1 + R_2)C_m.$$

At medium frequencies, all three capacitors are considered to have negligible reactances compared with R_1 and R_2 and the effective network is just R_1 and R_2 in parallel. In this frequency range, the gain is a maximum and has no frequency variation.

Finally, at high frequencies, C_m is considered equivalent to a short circuit, so that the network reduces to the parallel combination of the other elements. This network has a falling characteristic with the 3-db point at

$$\omega_2 = 2\pi f_2 = (g_1 + g_2)/(C_1 + C_2)$$

where the conductances of R_1 and R_2 are g_1 and g_2 respectively.

We now show that a straightforward analysis of the network of Fig. 1A leads to the result that it is exactly equivalent to a shunt combination of R , L and C .

Our problem is to compute $G = V_2/e$ for the admittance network of Fig. 1B. The result is

$$G = V_2/e = \frac{-jg\omega C_m}{[g_1 + j\omega(C_1 + C_m)][g_2 + j\omega(C_2 + C_m)] + \omega^2 C_m^2}$$

$$= \frac{-g}{\left[\frac{g_1 C_2 + g_2 C_1}{C_m} + g_1 + g_2 \right] + j\omega \left(\frac{C_1 C_2}{C_m} + C_1 C_2 \right) - \frac{j g_1 g_2}{\omega C_m}}$$

We observe that if the coupling network were of the form shown in Fig. 1C, we would have

$$G = \frac{-g}{1/R + j\omega C - j/\omega L}$$

It follows that both networks will have exactly the same gain characteristic if we put

$$G = \frac{1}{R} = \frac{g_1 C_2 + g_2 C_1}{C_m} + g_1 + g_2$$

$$\cong g_1 + g_2$$

$$L = \frac{C_m}{g_1 g_2}$$

$$C = \frac{C_1 C_2}{C_m} + C_1 + C_2 \cong C_1 + C_2$$

The gain characteristic is therefore the same as that of a single-tuned circuit resonant at f_0 where

$$\omega_0 = \frac{1}{\sqrt{LC}} \cong \sqrt{\frac{g_1 g_2}{C_m (C_1 + C_2)}}$$

(continued on p 198)

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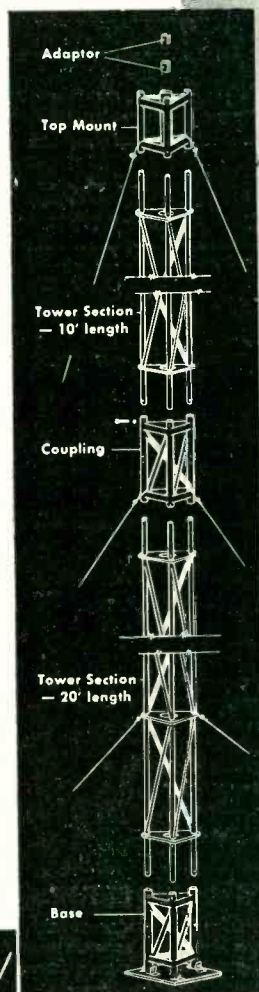
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- *Completely galvanized, light weight tubular steel . . . 20 ft. section 72 lbs.*

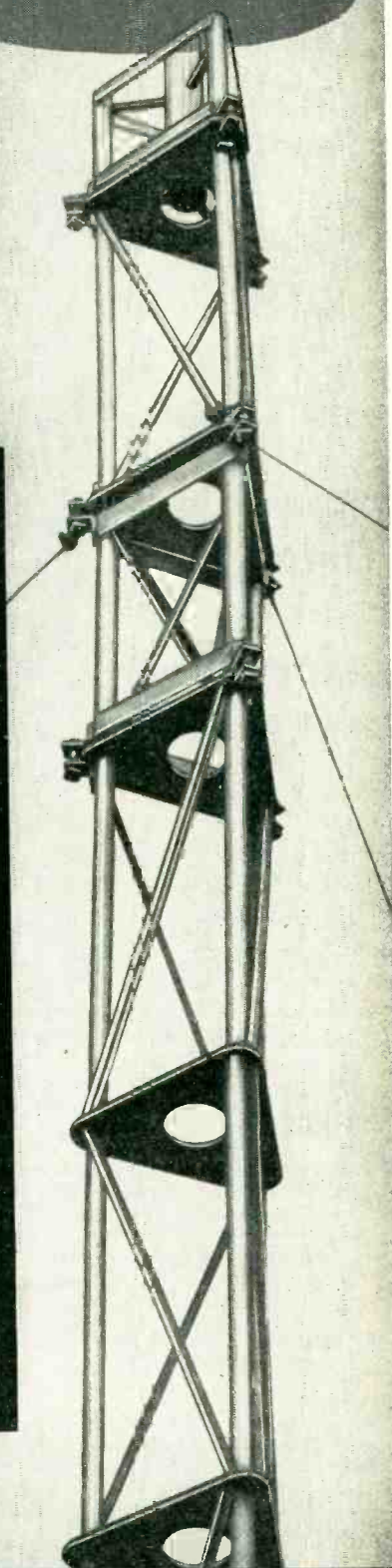
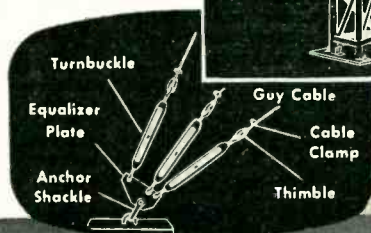
PRE-ASSEMBLED for fast, inexpensive installation

VEE-D-X towers are designed for use at any height from 10 to 140 feet. They are self-supporting up to 20 feet and, where space is limited, *semi-guyed** type installations may be used at 30, 40, and 50 foot heights. Sketch at right shows the basic parts and necessary accessories for a complete installation. Three types of top mount are available. VEE-D-X towers may be ordered in separate units or as a complete package for a specific height. (Either guyed or semi-guyed.) Write the LaPointe-Plascomold Corporation of Unionville, Conn. for complete information.

*Semi-guyed towers employ one set of guy cables attached at a height of 10 ft. up the tower and anchored at a 6 ft. radius from the base.



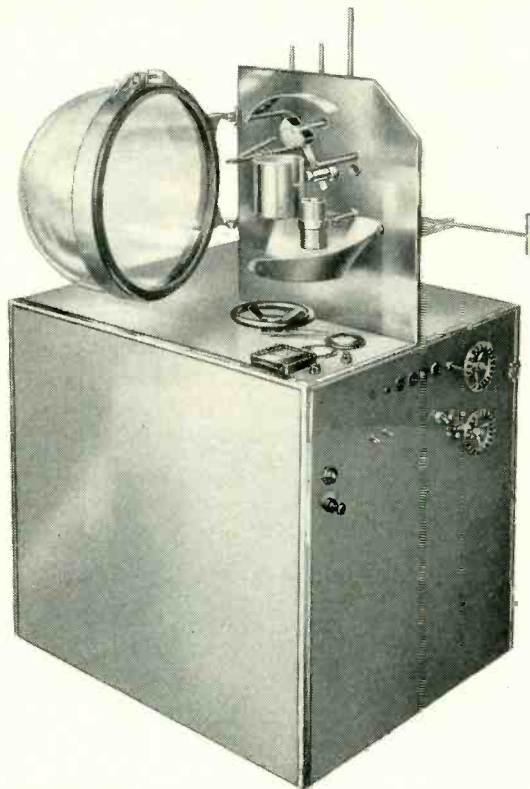
VEE-D-X



BUILDERS OF THE WORLD'S MOST POWERFUL ANTENNAS

NOW You can afford a High Vacuum Furnace

This ONE →
Versatile Unit lets you melt, pour, heat treat, degas



At last there is now available a single furnace that does away with the need to purchase equipment for each phase of your high-vacuum, high-temperature work. Because of its modest price, it will fall within the budget of most laboratories.

With this new furnace you can melt and solidify—melt and pour—add to the melt—stir—look into the hot zone—measure hot zone temperatures—introduce controlled atmospheres—degas—heat treat. It's a complete, versatile unit, capable of handling the widest variety of metallurgical research work. Write today.

FEATURES

- Ultimate vacuum of less than 5×10^{-6} mm. Hg.
- Working temperatures up to 2000° C.
- Temperature controllable within $\pm 5^{\circ}$ C.
- Hot zone reaches temperature within one minute.
- No refractories used in hot zone.
- 4" purifying type diffusion pump insures high capacity for out-gassing.
- Utilizes single turn low voltage resistance element of either tungsten or molybdenum $8" \times 2\frac{1}{2}"$ dia.
- Constant temperature zone $6" \times 2\frac{1}{2}"$ dia.
- Power supplied directly from mains to specially-designed variable auto transformer which is an integral part of unit.
- Either manual or automatic temperature control or both.
- Thermocouple vacuum gage is standard equipment. Other gages are available.
- Furnished complete with vacuum system, controls and gages including ammeter, volt-meter and temperature indicator.

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The Q and bandwidth Δf are

$$Q = \omega_0 RC \cong \frac{1}{g_1 + g_2} \sqrt{\frac{g_1 g_2 (C_1 + C_2)}{C_m}}$$

$$\Delta \omega = \frac{\omega_0}{Q} \cong \frac{g_1 + g_2}{C_1 + C_2}$$

To find the 3-db points, we recall that $\Delta \omega = \omega_2 - \omega_1$, and $\omega_0^2 = \omega_1 \omega_2$. Solving for ω_2 and ω_1

$$\omega_2 = (\Delta \omega / 2) + \sqrt{(\Delta \omega / 2)^2 + \omega_0^2}$$

$$\omega_1 = -(\Delta \omega / 2) + \sqrt{(\Delta \omega / 2)^2 + \omega_0^2}$$

For the two limiting cases,

$\Delta \omega / 2\omega_0 \gg 1$ and $\Delta \omega / 2\omega_0 \ll 1$, we get

$$\left. \begin{aligned} \frac{\Delta \omega}{2\omega_0} \ll 1; \omega_1 \cong \omega_0 - \frac{\Delta \omega}{2} \\ \omega_2 \cong \omega_0 + \frac{\Delta \omega}{2} \end{aligned} \right\} \text{error} \cong \frac{\Delta \omega}{4\omega_0}$$

$$\left. \frac{\Delta \omega}{2\omega_0} \gg 1; \omega_1 \cong \frac{\omega_0^2}{\omega} \right\} \text{error} \cong 3 \left(\frac{\omega_0}{\Delta \omega} \right)^2$$

$$\left. \omega_2 \cong \Delta \omega \right\} \text{error} \cong \left(\frac{\omega_0}{\Delta \omega} \right)^2$$

so that finally,

$$\omega_1 = \sqrt{\frac{g_1 g_2}{C_m \left(C_1 + C_2 + \frac{C_1 C_2}{C_m} \right)}} \left[\frac{C_m \left(g_1 + g_2 + \frac{g_1 C_2 + g_2 C_1}{C_m} \right)^2}{\sqrt{4g_1 g_2 \left(C_1 + C_2 + \frac{C_1 C_2}{C_m} \right)}} + 1 - \frac{\sqrt{C_m \left(g_1 + g_2 + \frac{g_1 g_2 + g_2 C_1}{C_m} \right)}}{2 \sqrt{g_1 g_2 \left(C_1 + C_2 + \frac{C_1 C_2}{C_m} \right)}} \right]$$

$$\omega_2 = \sqrt{\frac{g_1 g_2}{C_m \left(C_1 + C_2 + \frac{C_1 C_2}{C_m} \right)}} \left[\frac{C_m \left(g_1 + g_2 + \frac{g_1 C_2 + g_2 C_1}{C_m} \right)^2}{\sqrt{4g_1 g_2 \left(C_1 + C_2 + \frac{C_1 C_2}{C_m} \right)}} + 1 + \frac{\sqrt{C_m \left(g_1 + g_2 + \frac{g_1 C_2 + g_2 C_1}{C_m} \right)}}{2 \sqrt{g_1 g_2 \left(C_1 + C_2 + \frac{C_1 C_2}{C_m} \right)}} \right]$$

Or, since $\frac{\Delta \omega}{2\omega_0} \gg 1$ in the cases of interest to us,

$$\omega_1 \cong \frac{g_1 g_2}{(g_1 + g_2) C_m} = \frac{1}{(R_1 + R_2) C_m}$$

$$\omega_2 \cong \frac{g_1 + g_2}{C_1 + C_2}$$

These results justify the usual approximate analysis for the case

$$C_m \gg \frac{C_1}{C_2}$$

For the opposite extreme, C_m

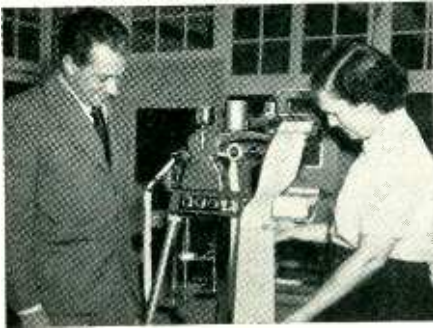
$$\ll \frac{C_1}{C_2} \text{ we get}$$

(Continued on p 200)



Instrument

NEWS

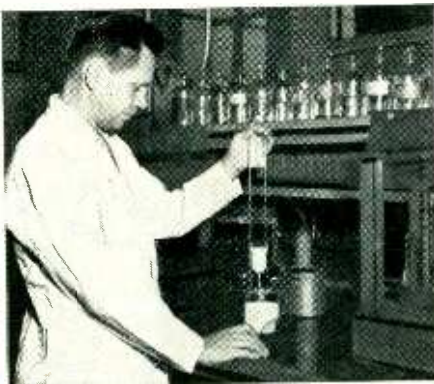


New Pacific Evenness Tester Uses Photoelectric Recorder

A new testing instrument developed by the Pacific Mills Worsted Division at Lawrence, Massachusetts, measures quickly and accurately the evenness and weight of textile strands. Known as the "Pacific Evenness Tester" and using a G-E photoelectric recorder, it largely eliminates the need for visual inspection of finished cloth, always a tedious and costly process.

The sensitivity of the system is indicated by the fact that a .002-inch deviation in strand thickness can represent full-scale deflection of the recorder.

The "Pacific Evenness Tester" is a tremendous step forward in the field of textile quality control. And it is one more proof of the versatility of the G-E photoelectric recorder. R. C. Wilkie (shown above), Manager of the Worsted Division's Engineering Research Department and designer of the new tester, says, "With its sustained accuracy, fast response, and high-sensitivity, the G-E photoelectric recorder is ideal for this application."



In the laboratories of the E. Ferbert Schorn-dorfer Company, Cleveland, Ohio, specialists in paints for industrial products, the Zahn viscosimeter is used as one means for maintaining uniformity and quality of finished product.

G-E OSCILLOGRAPH AIDS IN STUDIES OF BEACH AND OCEAN FLOOR EROSION

The General Electric Type PM-10-C3 oscillograph is playing an important part in the extensive studies of beach and ocean floor erosion now being made at La Jolla, California, by the Scripps Institute of Oceanography, part of the Graduate School of the University of California, in co-operation with the Army Corps of Engineers. The purpose of the studies is to find ways to minimize the serious harbor damage often caused by the action of waves.

Using a unique double strain gage pick-up and special signal generators and amplifiers, all designed and built by Scripps personnel, the velocities of the waves are measured in two directions and the results recorded on photographic film by the Type PM-10-C3 oscillograph.

The oscillograph itself is located in the laboratory while the gage unit lies on the ocean floor more than half a mile away. Interconnecting cables relay the delicate signals.

Mr. James Snodgrass (shown at right), technical director, says "the wide frequency



response and high sensitivity of the Type PM-10-C3 oscillograph, together with its adjustable resistances and high-speed camera control, make it particularly suitable for this application."

Magnets Balanced Quickly With Indicating Fluxmeter

Wilfred O. White and Sons, Inc., of Boston, Massachusetts, manufacturers of the famous *Constellation* spherical compass and other navigational instruments and associated equipment, are now using a General Electric indicating fluxmeter for checking the flux-density balance of permanent magnets used in their complete range of compasses.

The raw magnets are inserted in holes in a testing panel connected to the fluxmeter and especially designed for this application. The fluxmeter gives an immediate and accurate indication of their comparative strength. If one magnet is too strong, it is inserted into the "demagnetizer," another hole in the panel. The process is repeated until the desired balance is obtained.

With this system, the flux densities of the magnets can be brought to within 10 percent of each other, a high degree of balance for magnets of this type.



SECTION A602-196
APPARATUS DEPARTMENT
GENERAL ELECTRIC CO.
SCHENECTADY, N. Y.

Please send me information on the following products:

- Type PM-10-C3 oscillograph
- Type CE photoelectric recorder
- Indicating fluxmeter
- Zahn viscosimeter

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REGULATED D. C. UP TO 1000 VOLTS AT 500 M. A.

*Featuring continuously variable
output voltage Without Switching*

● Here are four power supplies especially designed to cover a wide range of applications in development and production. These instruments feature continuously variable output voltage, good regulation, low hum level, good stability and overload protection. Models 200-B, 204-A, 205-A and 207-B will operate from line input of 105 to 125 volts A.C. 50-60 cycles and provide rated regulation within this change. Examine the specifications carefully and you may find that one or more of these units has an application in your research or production program.



MODEL 204-A 0-500v D. C. at 300 MA.

Output Voltage:
0-500v D.C. at 300 Ma. regulated
6.3v A.C. at 6 Amps. unregulated
Regulation: Within 1% from 30-500 v
Hum: Within 10 mill volts at full load
Meters: 0-300v D.C.
0-300 Ma. D.C.
Negative or positive side of
high voltage output may
be grounded.

MODEL 207-B 200-1000v D. C. at 500 MA.

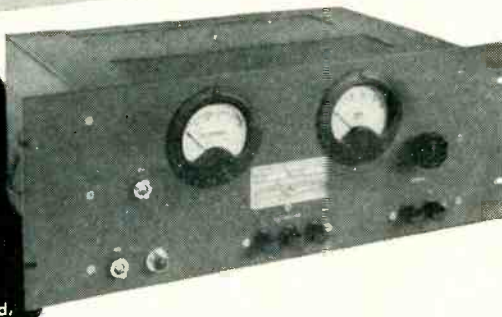
Output Voltage
200-1000v D.C. at 500 Ma. regulated
Regulation: Within 1% from 200-1000
Volts
Hum: Within 20 millivolts at full load
Meters: 0-1000v D.C.
0-500 Ma. D.C.
Negative side of high voltage
grounded.

MODEL 205-A 100-325v D. C. at 150 MA.

Output Voltage:
100-325v D.C. at 150 Ma. regulated
0-150v D.C. at 5 Ma. regulated by VR tube
6.3v A.C. at 6 Amps. unregulated
Regulation: Within 1% from 100-325v D.C.
Hum: Within 10 millivolts at full load
Meters: None
Negative or positive side of high voltage
output may be grounded.

MODEL 200-B 0-325v D. C. at 125 MA.

Output Voltage:
0-325v D.C. at 125 Ma. regulated
6.3v A.C. at 6 Amps. unregulated
Regulation: Within 1% from 20-325 V
Hum: Within 10 millivolts at full load
Meters: 0-300v D.C.
0-150 Ma. D.C.
Negative side of high voltage grounded.



Detailed information on any or all of the instruments above will be sent upon request. Price and delivery information will also be forwarded at the time of your request. Send for Catalog "A"—there is no obligation.

ELECTRONIC MEASUREMENTS COMPANY

Red Bank  New Jersey

REGULATED POWER SUPPLIES — VACUUM TUBE VOLTMETERS — SIGNAL GENERATORS

$$G = \frac{1}{R} \cong \frac{g_1 C_2 + g_2 C_1}{C_m} \quad \omega_o \cong \sqrt{\frac{g_1 g_2}{C_1 C_2}}$$

$$L = \frac{C_m}{g_1 g_2} \quad Q \cong \sqrt{\frac{g_1 g_2 C_1 C_2}{g_1 C_2 + g_2 C_1}}$$

$$C \cong \frac{C_1 C_2}{C_m} \quad \Delta\omega \cong \frac{g_1 C_2 + g_2 C_1}{C_1 C_2} =$$

$$\frac{g_1}{C_1} + \frac{g_2}{C_2}$$

It is easily seen that the equivalent circuit is characterized by an inherently low Q. Indeed, since the original circuit of Fig. 1A is aperiodic, the equivalent circuit of Fig. 1C must have $Q < \frac{1}{2}$. In practice, Q is much smaller than $\frac{1}{2}$. For a 100-cps to 10^6 -cps bandwidth, for example, $Q \cong \sqrt{10^2/10^6} = 0.01$.

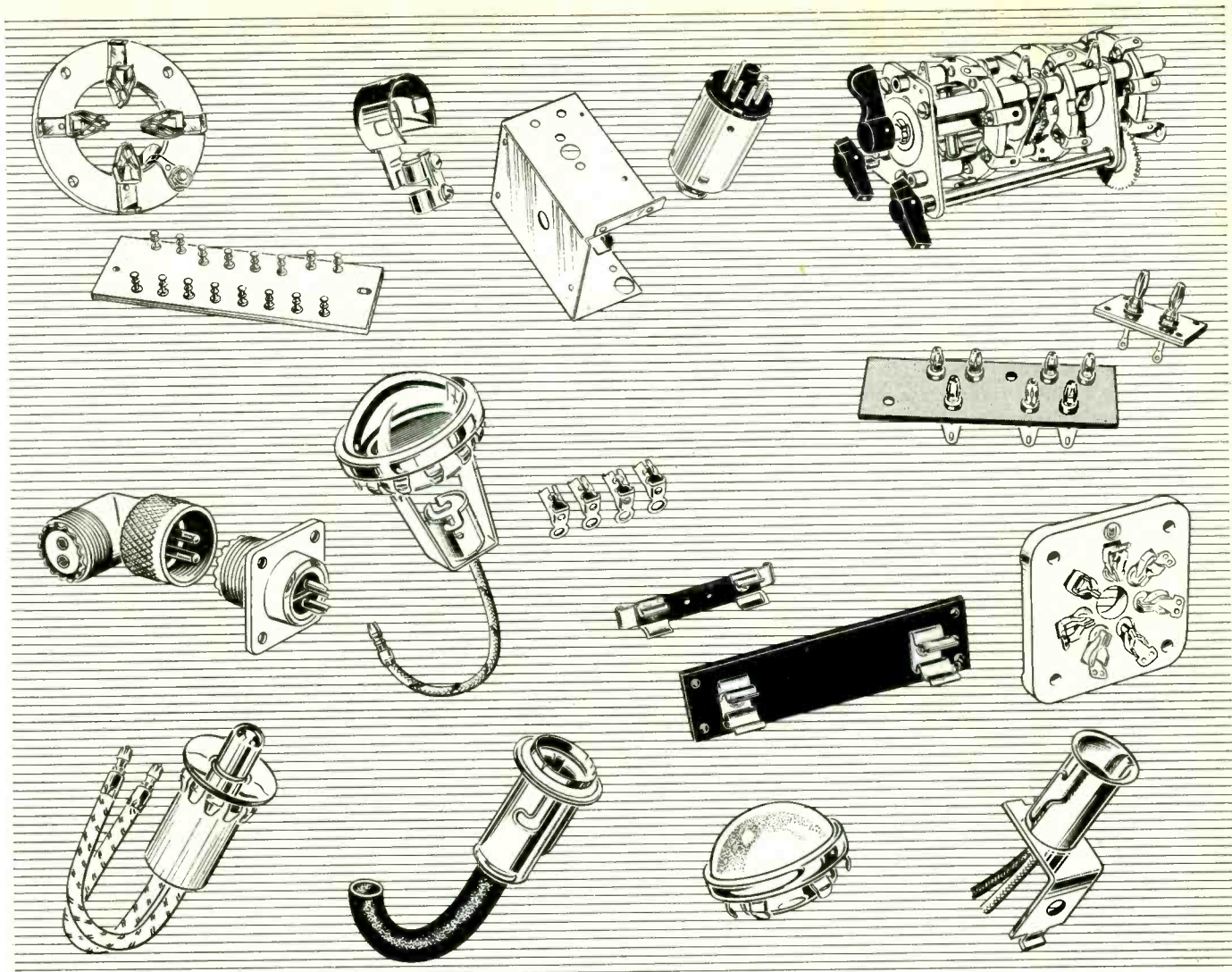
Since this analysis shows that the circuit is exactly equivalent in its gain characteristic to a single-tuned circuit, it suggests the feasibility of combining this circuit with others in cases where an extremely low Q is required. The point of view taken here also suggests that several of these circuits might be stagger-tuned to produce a wide-band video amplifier without additional compensation. However, since $Q < \frac{1}{2}$, this circuit could only be used as the center stage of an odd number of stagger-tuned circuits.

New Accuracy in Speed-of-Light Measurements

THE SPEED OF LIGHT has been measured with an accuracy of 0.0002 percent by a special microwave system at Stanford University. The new figure of 186,280.0 miles per second is believed to be 10 to 20 times more accurate than the previously-accepted value of 186,272 which was drawn from



Accurate measurements of resonant frequency of microwave cavity permit determination of the speed of light with 0.0002-percent accuracy



Do you remember?

Old hands in the electronics field will recognize some familiar items in the selection above. They are typical of the many components and assemblies we supplied for use by the Services from 1940-45. We also illustrate several new parts, representative of our current production.

With the present expansion of military procurement, we stand ready as before to supply the all-important components promptly . . . and in quantity. Just let us know your needs.

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Here may be the answer to your RECORDING problem

Sanborn Amplifier Recorders are being found outstandingly useful in a wide variety of industrial recording applications. Records are produced *directly*, and continuously, by *heated stylus* on plastic coated record paper (Permapaper), are in *true rectangular* coordinates, and are sharp, clear, and *permanent*. Elimination of the *ink flow* type of recording permits the use of these recorders in any position and at any angle. The writing arm (or arms) is driven by a D'Arsonval moving coil galvanometer with an extremely high torque movement (200,000 dyne cms per cm deflection).

The single channel Model 128 is a vacuum tube recording voltmeter capable of reproducing electrical phenomena from the order of a few millivolts to more than 200 volts. Standard paper speed is 25 mm/sec. Slower speeds of 10, 5, and 2.5 mm/sec. are available. A variety of interchangeable amplifiers is available.

The multi-channel Model 67 provides for the simultaneous registration of *up to four* input phenomena on one record using, in a multiple system, the same principles and methods as the single channel Model 128.

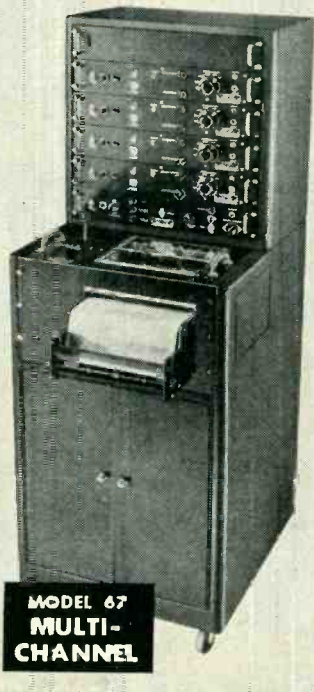
In addition, this vertically mounted, metal cased amplifier-recorder provides a choice of eight paper speeds: 50, 25, 10, 5, 2.5, 1.0, 0.5 and 0.25 mm/sec., and further provides for the use of 4-, 2-, or 1-channel recording paper. Complete versatility of recording is offered in this unit by means of interchangeable amplifiers which permit the registration of stresses, strains, velocities, etc., along with the usual D.C. or A.C. phenomena.

The recorder and amplifier units of which the above models are comprised are also available separately.

SANBORN AMPLIFIER- RECORDERS



MODEL 128
SINGLE
CHANNEL



MODEL 67
MULTI-
CHANNEL

For complete catalog giving tables of constants, sizes and weights, illustrations, general description, and prices, address:

SANBORN COMPANY
Industrial Division
CAMBRIDGE 39, MASS.

Sanborn Recorders and Amplifiers have evolved from those originally designed by Sanborn Company for use in electrocardiographs, and have, by actual practice, proven to have wide applications in the industrial field as well.

averages computed by many workers during the past 25 years.

The basis of the measuring system is a microwave cavity whose dimensions are known down to the millionth part of an inch. These accurate dimensions, and an accurate measurement of the resonant frequency of the cavity, allow calculation of the speed with which radio waves, and thus light waves, travel.

To allow the extremely accurate determination of cavity dimensions, contour maps of the covers of the cavity were made to allow mathematical calculation of any deviations that might occur. Spacer rods, which hold the cover in place, are measured with an accuracy that permits calculation of their dimension changes, down to the ten-thousandth of an inch, when compressed by the weight of the disc cover. The rods themselves had to be equal within a few millionths of an inch. The temperature of the room in which the measurements are made is held to within 0.01 degree C.

The development work on the new system took five years. The actual measurement process is relatively simple, once the equipment is set up. The photograph shows Edward Ginzton and Arthur W. Hornig positioning the equipment to measure the inside dimensions of the microwave cavity.

Ratio and Product Control By Shield-Grid Thyratrons

BY CHARLES F. SPITZER
Yale University
New Haven, Connecticut

IN MANY instances of process control, it is desirable to actuate a relay or to trigger an indicating circuit whenever the ratio of two quantities deviates from a preset value. In other instances it may be desirable to maintain the product of two quantities constant and to obtain an indication if a certain limit has been exceeded. These results are readily obtained through the use of a shield-grid thyatron. The 2D21 thyatron has been chosen in the following investigation since its miniature design and relatively



For Negative Resistance-Voltage Characteristics

GLOBALAR

TRADE MARK

TYPE BNR RESISTORS

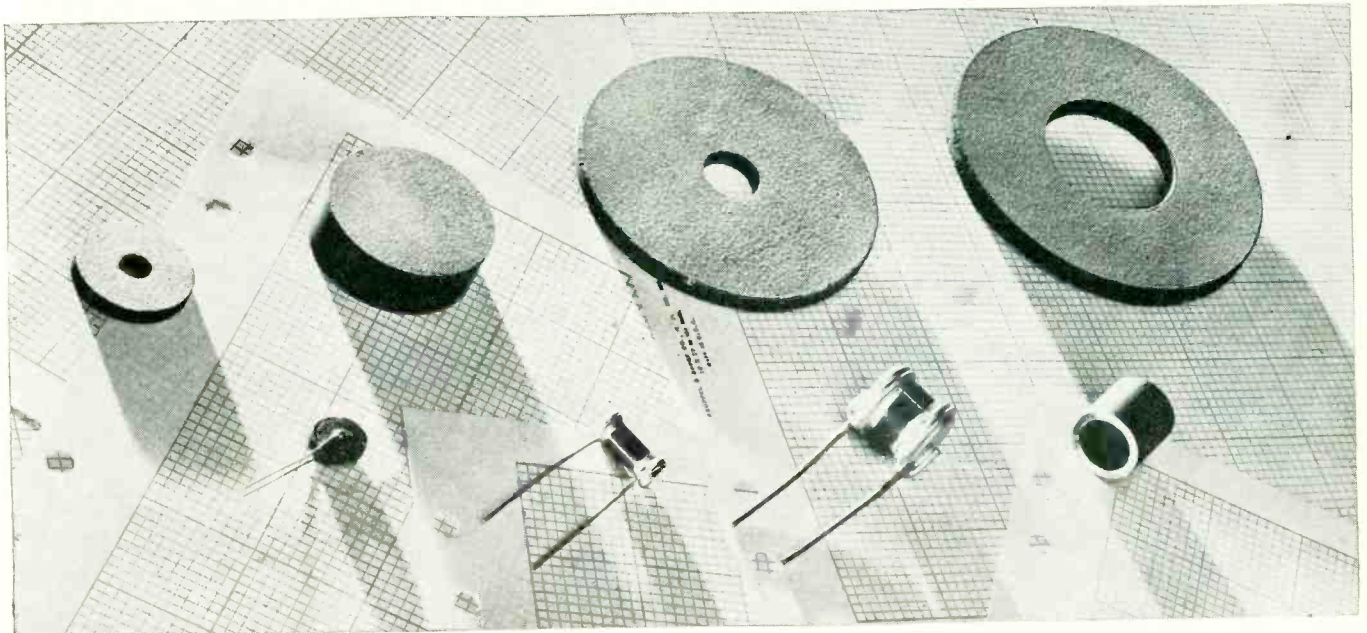
Typical applications where these resistors operate successfully include:

- 1 Small motors to prevent arcing of governor contact points.
- 2 Stabilizing rectifier circuits by limiting peak voltages.
- 3 Voltage control circuits in electronic devices.
- 4 Protection of solenoids in direct current circuits.

Responding instantly to voltage changes, GLOBALAR type BNR Silicon Carbide Resistors provide increased resistance as a potential is decreased. Conversely, as a potential is applied, resistance decreases. These resistors are what is commonly referred to as voltage sensitive. They are used to dampen the effect of transient voltages and provide instant protection for electrical circuits.



Bulletin GR2 contains useful engineering data on GLOBALAR BNR Ceramic Resistors. Copies will be supplied immediately upon request. Write Dept. V-11, The Carborundum Company, GLOBALAR Division, Niagara Falls, N. Y.



Resistors of this type are readily made to meet exact specifications. Working samples are available when necessary. To be sure of receiving resistors made to correct specifications, the following information should be furnished:

- a. Type of apparatus in which resistors are to be used.
- b. Method of mounting and space limitations.
- c. Normal operating voltage and peak voltage if available.
- d. Resistance and inductance of the circuit if available.
- e. Ohmic resistance of the resistor and allowable plus or minus tolerance.
- f. Maximum voltage applied continuously or intermittently.
- g. Duration of load and elapse of time between applications.

Furnishing these data will also avoid unnecessary delay and confusion.

GLOBALAR Ceramic Resistors

BY **CARBORUNDUM**

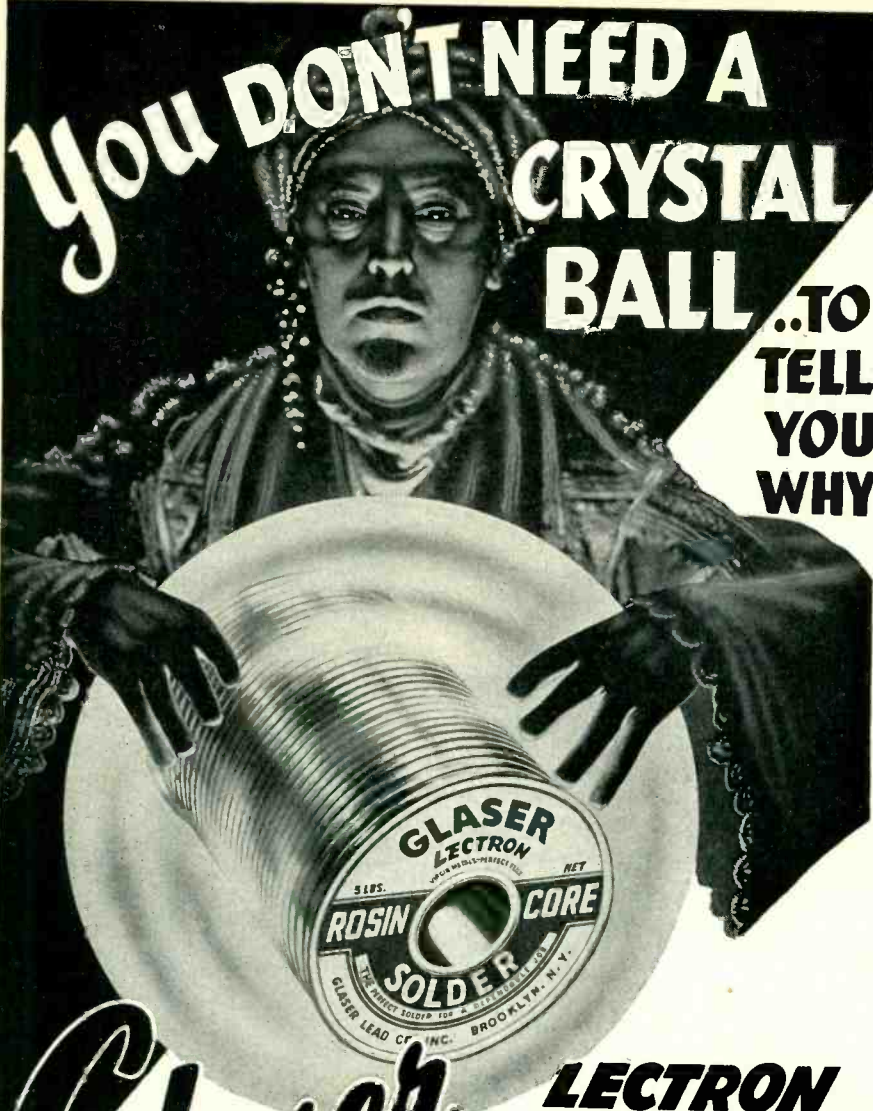
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large current carrying capacity (100 ma continuously) make it particularly suitable for compactly built control devices.

Ratio Limiting

The characteristic curves of the tube under consideration are shown in Fig. 1. In the region above each curve the tube conducts, and below each curve it remains cut off.

For a plate voltage of 300 volts, the characteristic consists of three nearly straight lines, marked *a*, *b* and *c*. Line *a* has a small slope ($= -0.25$) while line *b* has a fairly steep slope ($= -7.65$). Line *c* merges into line *b*, and has a somewhat steeper slope than the latter.

If it is desirable to obtain an indication that the ratio $\Delta E_g/\Delta E_s$ has exceeded a certain value, a static operating point *P* may be chosen (by proper biasing). Then, if operation takes place along line *b*, that is if ΔE_s is positive and ΔE_g is negative, the tube will fire if the ratio $\Delta E_g/\Delta E_s$ has exceeded the value 7.65. Other ratios are readily available through the use of attenuators (or amplifiers) for the original signals from which ΔE_s and ΔE_g are obtained.

If less than optimum accuracy is permissible, the range of operation can be greatly extended by replacing lines *b* and *c* by a single line of average slope. This will allow ΔE_g to swing over more than 40 volts,

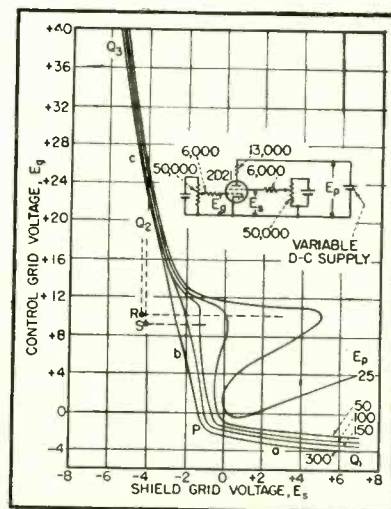


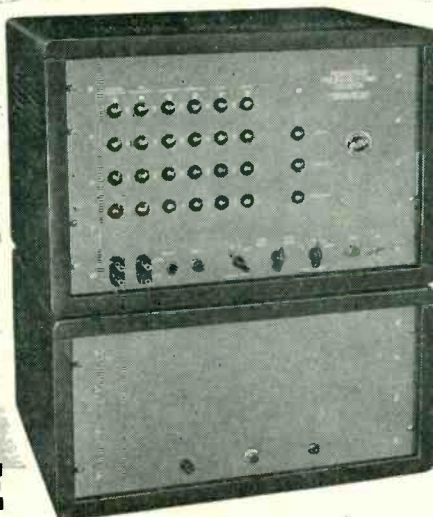
Fig. 1—Characteristics of a 2D21 thyratron, with d-c on the plate. For ratio control the static operating point is chosen at *P*, *Q*₁, *Q*₂ or *Q*₃, whichever the problem demands. For product control operating point is set at *R* or *S*

NEW! FREQUENCY AND TIME MEASUREMENTS ACCURATELY... CONVENIENTLY

FREQUENCY RATIO MEASUREMENTS

DIRECT RPM READING TACHOMETER

SECONDARY FREQUENCY STANDARD



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$$f = \frac{n}{t}$$

ANY FACTOR MAY BE MEASURED FOR FIXED VALUE OF THE OTHER

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TIME INTERVAL MEASUREMENTS

TOTALIZING COUNTER

The Universal 6-IN-ONE MEGACYCLE

FREQUENCY-TIME COUNTER

Now, the Potter Instrument Company offers all-in-one equipment, the features heretofore available only in separate counting systems. Two complete counting channels, a 100 kc crystal oscillator time base and unique gating circuits are combined to provide the new FREQUENCY-TIME COUNTER.

by *Potter*

FREQUENCY MEASUREMENTS	0 to 1 mc range by counting cycles per pre-selected time or by measuring time per pre-selected count. Accuracy 0.001 % minimum.
TIME INTERVAL MEASUREMENTS	0 to 10 seconds \pm 10 micro-seconds.
FREQUENCY RATIO MEASUREMENTS	Ratio of two external frequencies can be measured.
SECONDARY FREQUENCY STANDARD	100 kc crystal oscillator with divided frequencies available at 10, 1 kc and 100, 10, 1 cps.
TOTALIZING COUNTER	Six decades, pulses 0 to 1 mc, sine wave 10 cps to 1 mc.
DIRECT RPM READING TACHOMETER	Through the use of an external 60 count per revolution photoelectric disc generator an accuracy of \pm 1 rpm is obtained.

FEATURES

WIDE FREQUENCY RANGE — Pulses 0 to 1 megacycle — sine waves from 10 cps to 1 mc.

EXTREMELY HIGH ACCURACY — 0.001% from 0 to 1 megacycle.

VERSATILITY — Frequency measurements, time intervals, frequency ratios, high speed counting, rpm measurements, and a secondary frequency standard — all in one instrument.

RAPID MEASUREMENT — No adjustments or interpolations — only a few seconds for a complete measurement.

DIRECT DECIMAL READING — Frequency or time displayed on six Potter Counter Decades using the 1-2-4-8 large neon glow lamp decimal indication. Readable even under high ambient illumination.

AUTOMATIC OR MANUAL RECYCLING — The counter will retain the measurement until reset or will automatically recycle after displaying the measurement for a selected time.

NO ADJUSTMENT — Stable decade counter frequency dividers, rather than multivibrators are used to establish the precise time base.

DEPENDABLE — The exclusive four-lamp Potter decades provide a direct on-off indication of the counter stages without the complexity and unreliability of a readout matrix. An associated glow lamp for each tube in the counting and dividing circuits simplifies tube servicing.

PERMANENT RECORD — Other versions of the Frequency Time Counter can be supplied with high speed recording devices.



POTTER INSTRUMENT COMPANY
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P
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Type MC-9

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ERIE, PENNSYLVANIA

with a corresponding ΔE_s of nearly 5 volts.

If Q_1 is chosen as the static operating point and operation takes place along line *a*, that is, again, if ΔE_s is positive and ΔE_c is negative, the tube will fire if the ratio of $\Delta E_s/\Delta E_c$ exceeds the value 0.25. Again, other ratios are readily available through the use of attenuators (or amplifiers for the signals from which ΔE_s and ΔE_c are obtained. In general, point *P* and line-*b* operation are preferable if the ratio to be indicated is greater than unity, while Q_1 and line-*a* operation are better suitable for ratios of less than unity.

If it is desirable to obtain an indication that the ratio $\Delta E_s/\Delta E_c$ has dropped below a certain value, point *P* and line *a* operation may be chosen (ΔE_s negative and ΔE_c positive). The tube will then fire if $\Delta E_s/\Delta E_c$ drops below the value 0.25, with other ratios obtainable through attenuators or amplifiers.

If point Q_2 and line-*b* operation are chosen (ΔE_s negative and ΔE_c positive), the limiting ratio will be 7.65 and the tube fires if the signal ratio is less than this value with other ratios becoming available, as before, through attenuators or amplifiers. If less than optimum accuracy is permissible, lines *b* and *c* can again be merged and their slopes replaced by an average value. In this manner the operating range is greatly extended. For ratios below unity, operating point *P* should be used, while for ratios above unity operating point Q_2 is more suitable.

Ratio Limiting Applications

One application of this circuit might be to indicate whether the percent distortion of an amplifier exceeds a certain value. Through the use of two such circuits, the ratio of two quantities can be kept within close limits; in this case one circuit operates when the ratio drops below the preset value, the other when the ratio exceeds it. Thus, liquid mixtures of two components may be accurately controlled by automatically adjusting the flow of each component liquid, for example.

It is particularly noteworthy that the response of the tube appears



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SELF-LOCKING NUTS
can't work loose, either

FLEXLOCs always **STAY LOCKED**, regardless of vibration. They're one-piece, all-metal, have nothing to lose or forget. Temperatures to 550° F. don't bother them, and you can use them again and again with no appreciable loss of torque.

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FLEXLOC Self-Locking
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STANDARD PRESSED STEEL CO.

JENKINTOWN 10, PENNSYLVANIA

The RCA "TV Duo"...



... the last word in *precision* and *versatility*

RCA WR-59B Television Sweep Generator

What it does—Provides fast and accurate sweep alignment and trouble shooting of TV front ends . . . sound and picture if amplifiers . . . discriminators and ratio detectors . . . trap circuits . . . video amplifiers . . . and if amplifiers in FM sets.

What it features—Preset switch positions for TV channels 2 to 13 . . . continuous tuning from 300 kc to 50 Mc . . . flat output, within ± 1.5 db even at maximum sweep width . . . fundamental oscillator output on all TV channels . . . filtered beat-frequency-fundamental output on if/vf range . . . zero-voltage reference line provided by return-trace blanking . . . dual piston attenuator with maximum attenuation ratio of 20,000 to 1 . . . continuously variable sweep width up to 10 Mc . . . output frequency-modulated at the fundamental frequency by a precision-type vibrating capacitor, for long life and good linearity . . . balanced rf output cable terminated in 300 ohms . . . fully shielded circuits and filtered power line . . . resistance-terminated if/vf output cable.

For complete details ask your RCA Test Equipment Distributor for Bulletin 2F753.

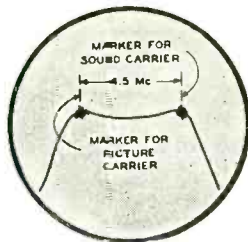
RCA WR-39B Television Calibrator

What it does—Provides dual markers for rf picture and sound carriers . . . provides signals for peak alignment of stagger-tuned if amplifiers . . . develops vertical bar pattern for horizontal linearity adjustments . . . generates a crystal-controlled AM signal for alignment of inter-carrier sound if's . . . provides triple markers for sound discriminator adjustment . . . allows adjustment of local oscillators in TV front ends with crystal accuracy . . . checks reception on all 12 channels by means of video signal obtained from single channel of a TV set.

What it features—Variable-frequency oscillator operating on fundamentals over entire range . . . sound and picture carrier frequencies marked on expanded, easily-read scale . . . two crystal oscillator stages with 3 crystals supplied . . . wide-band modulator stage with range of 0 cps to 30 Mc . . . crystal standard supplying over 600 calibration check points at 0.25-Mc intervals . . . bar-pattern generator for

linearity adjustments.

For complete details ask your RCA Test Equipment Distributor for Bulletin 2F751.



"Scope pattern of dual markers for rf picture and sound carriers, produced by the "TV Duo.""

Available from your RCA Test Equipment Distributor

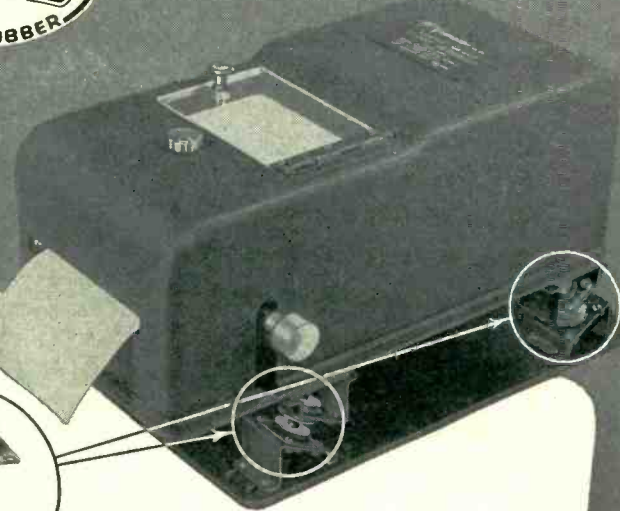


RADIO CORPORATION of AMERICA
TEST EQUIPMENT
HARRISON, N. J.

ACCURATE and DEPENDABLE FLIGHT RECORDS *Protected by*



MOUNTINGS



Sensitive equipment requires protection from shock and vibration to assure original accuracy and dependability. The Giannini Flight Recorder illustrates how the G. M. Giannini Company of Springfield, N. J., uses LORD Mountings to insure the precise recordings of four simultaneous test operations.

Note that standard LORD Mountings are used in tandem to supply universal freedom of movement . . . and that they are focalized at the center-of-gravity of the recorder. This arrangement of LORD Mountings permits the instrument to be used in either vertical or horizontal position without loss of mounting effectiveness.

This method of applying LORD Mountings was recommended by LORD engineers to meet the particular conditions under which the instrument would operate. If you have a problem involving product protection or improvement through control of vibration, we suggest that you submit it to us for analysis and recommendation. Write to attention of Product and Sales Department.

LORD MANUFACTURING COMPANY · ERIE, PA.

Canadian Representative: Railway & Power Engineering Corp. Ltd.

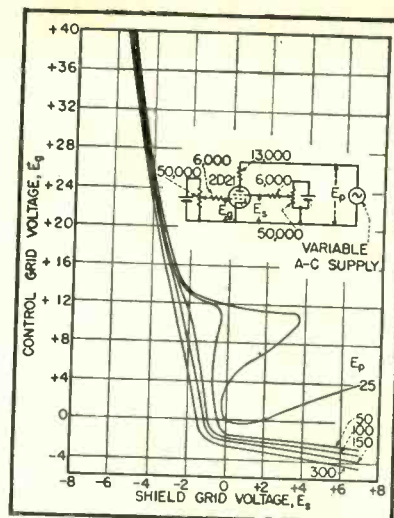


Fig. 2—Characteristics of a 2D21 thyatron, with a-c on the plate. These curves are very similar to those of Fig. 1, illustrating that either type of plate excitation is suitable for ratio or product control

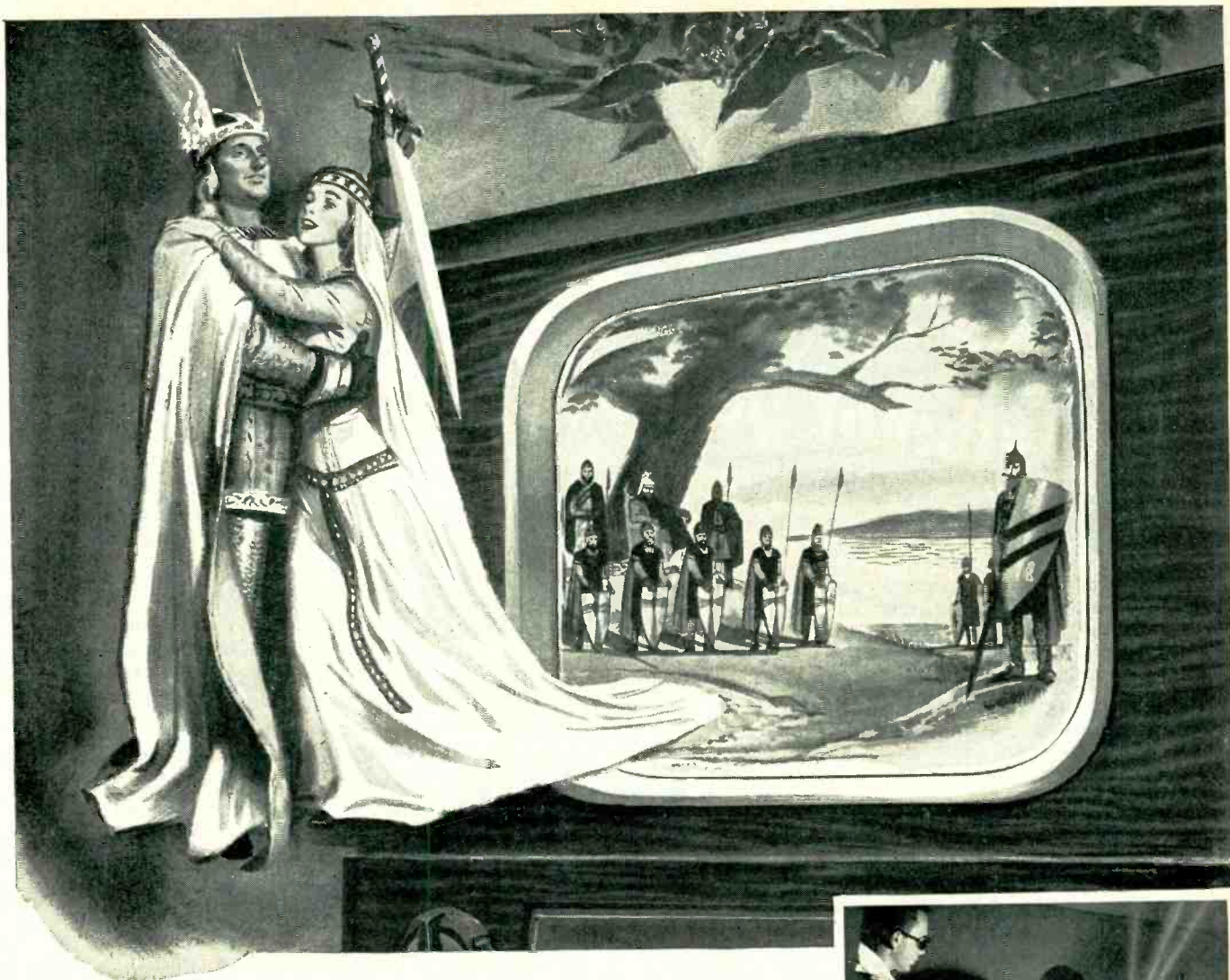
relatively independent of the plate voltage between 150 and 300 volts, (and probably above) as reference to Fig. 1 discloses. Thus, small variations in plate supply voltage have almost no effect on the slopes of lines *a*, *b* and *c*, or on the location of the operating point.

Product Limiting

Again referring to Fig. 1, it is noted that the characteristic curve for a plate voltage of 25 volts has a very noticeable bend near the point ($E_s = 12, E_c = -2$). Over a certain range, this characteristic is very nearly hyperbolic with asymptotes intersecting at $R(E_s = -4.3, E_c = +10)$. The equation of this hyperbola is approximately $E_s E_c = 7$ between the points ($E_s = -3.2, E_c = +18$) and ($E_s = +3; E_c = +11$). An operating point is then chosen near *R* such as to keep the tube extinguished if the product $E_s E_c$ is less than 7. If the characteristic curve for a plate voltage of 50 volts is chosen, a very similar result is observed.

The equation of the curve is again very nearly $E_s E_c = 7$, but over a smaller range. The points ($E_s = 3.3, E_c = +18$) and ($E_s = -1.0, E_c = +11.4$) limit hyperbolic operation. The asymptotes intersect at $S(E_s = -4.1, E_c = +9)$ and an operating point is chosen near this point.

It is clear that products other than $E_s E_c$ can again be readily



This, we can't quite do!

But TUNG-SOL does make electron tubes that accurately synchronize the television receiver with the transmitter—cathode ray tubes that present a picture of unexcelled clarity.

How well we do it, is indicated by the fact that TUNG-SOL tubes meet fully the performance requirements of every leading television set manufacturer.

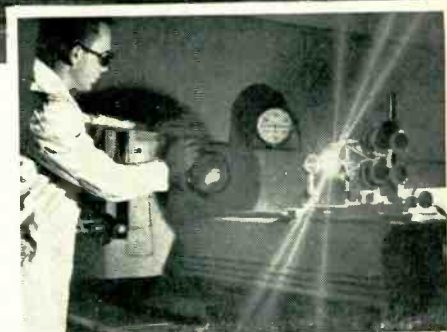
There is no mystery to the source of TUNG-SOL quality. We just work hard at it. Raw materials are carefully inspected—thoroughly tested. Then, using the most modern statistical quality control methods, TUNG-SOL produces tubes to standards of uniformity and reliability that are unsurpassed in the electronic industry.

Finally, before any tubes can be shipped, they must be certified by TUNG-SOL's Quality Control Department. This means a complete re-check of each day's output to make certain of a strict adherence to

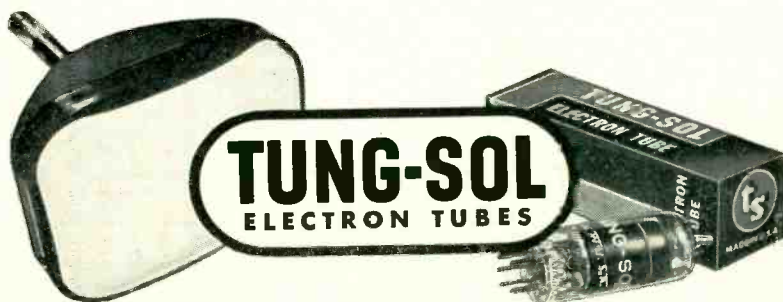
specifications. Every TUNG-SOL tube is made to back up the TUNG-SOL slogan—"Make the best that can be Made."

If you use electron tubes for radio, television, or special-purpose applications, we'd like to have the opportunity of demonstrating the many advantages of doing business with TUNG-SOL.

TUNG-SOL LAMP WORKS INC., Newark 4, N. J.
Sales Offices: Atlanta, Chicago, Dallas, Denver, Detroit, Los Angeles, Newark



Quality is built-in, not "tested-in." Nevertheless, the guarantee of built-in quality is unlimited testing. Here is one of TUNG-SOL's numerous and exacting quality control tests—the chemicals used in the screen of the TUNG-SOL TV picture tube are analyzed in the spectograph to determine purity.



FOR RADIO, TV AND SPECIAL PURPOSES

For High Temperature, Space-Saving HOOK-UP WIRE...

**Specify
Rome
Synthinol* 901**

Here's the answer to your space problem . . . a radio and television hook-up wire with an 8 mil wall. Insulated with Rome Synthinol 901 thermoplastic compound, plus nylon sheath or lacquered braid, it is fully Underwriters approved for continuous operation at 90° C., above or below the chassis, in approved applications. Available in sizes 24 AWG to 16 AWG, it replaces heavier, space-consuming 1/64" and 1/32" insulations.

For Space Savings Compare These Diameters:

Tinned Conductor Size	Maximum Diameter Over Nylon Sheath (Inches)
24 AWG Solid	.051
24 AWG 7/.0079	.055
22 AWG Solid	.056
22 AWG 7/.010	.061
20 AWG Solid	.063
20 AWG 10/.010	.069
18 AWG 16/.010	.088
16 AWG 26/.010	.100

Available in a wide range of colors, Rome Synthinol 901 insulation has these advantages:

Increased resistance to heat deformation • Excellent heat aging properties • Increased resistance to oils, chemicals, greases, moisture and flame • Clear, permanent colors • Improved solderability • Improved space factor.

Whatever your requirements, including military types, look to Rome Cable for electronic wires of quality you can depend upon.

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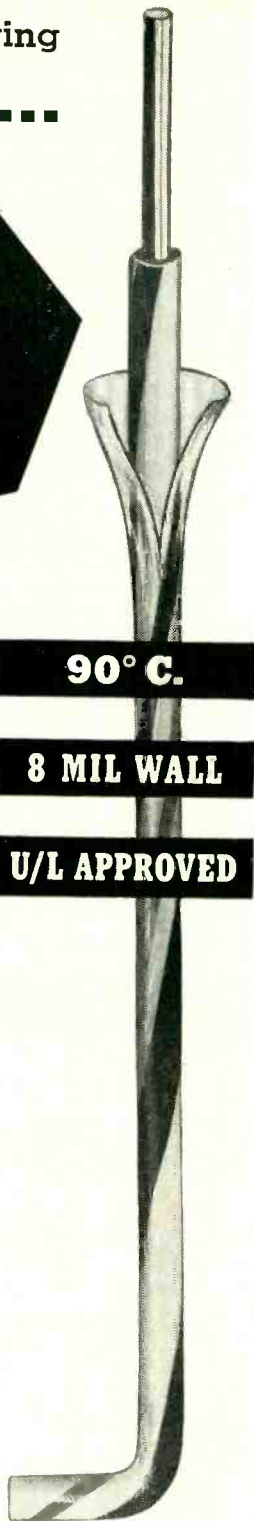
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ROME CABLE CORPORATION
ROME, NEW YORK



*T. M. Reg.

obtained by the use of amplifiers or attenuators preceding this product-limiting stage.

Since the control grid and shield grid lose control once the plate circuit of the thyatron conducts, it is necessary to reset the device by opening the plate circuit. It has been further observed that above a grid voltage of about 12 volts interruption of the plate circuit does not extinguish the tube. The reason is evidently that the control grid-cathode circuit is ionized and remains so unless it also is opened.

Figure 2 shows the characteristics of the 2D21 thyatron when the plate is supplied from a-c. Otherwise, the circuit is the same as that of Fig. 1. As will be noted, the curves are very similar to those of Fig. 1. Thus, when using the circuit for ratio limiting (and if the control grid voltage is kept below 12 volts), resetting takes place automatically. In this form the circuit lends itself exceptionally well to use in continuous control devices. If the control grid voltage exceeds 12 volts a hysteresis effect is observed which necessitates the opening of the control grid circuit to reestablish control. The reason is, as before, that the control-grid-cathode circuit remains ionized, otherwise.

The ability of a thyatron to fire when the E_c/E_a ratio deviates from a preset ratio was used in a device designed to measure the ratio of voltages which were, in turn, determined by the high and low frequency content of a signal. In this arrangement it gave satisfactory service over an extensive period of use. It must be realized that tube replacement will require recalibration of the device, in general.

ERRATUM NOTICE:

In the September *Electron Art* department, an error was made in crediting the development of the "Electrodynamic Ammeter for VHF". This was called to our attention by H. R. Meahl, of the General Electric Company. In accordance with his request, this notice is being published, calling attention to his letter which appears in this month's *Backtalk* department.

DUMONT

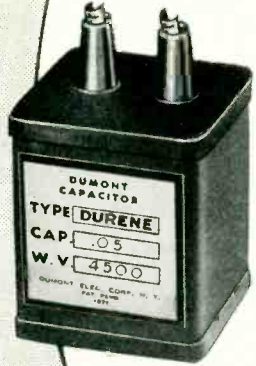
**TYPE S
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CAPACITOR**



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"ZERO-LOSS"
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CAPACITORS

**TYPE S1
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POWER FACTOR
.0005
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PLASTIC
FILM
IDEAL
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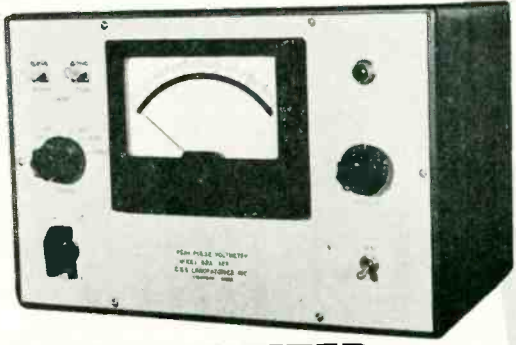
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MFR'S OF
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VOLTMETER

Far more versatile than conventional types, the C.G.S. peak pulse voltmeter reads *rapidly* and *accurately* on pulse widths of .25 microseconds and at repetition rates of 10 pps. The instrument reads on either positive or negative pulses. Controls include an on-off, range selector and input polarity switch; zero set control. A switch which throws a D.C. restorer into the circuit provides accurate peak to peak measurements of sine and square waves.



- SPECIAL FEATURES —**
- Wide Voltage Range — 5 scales from 10 to 5000 volts full scale.
 - Pulse Width 0.25 microseconds to 50 milliseconds.
 - Accuracy $\pm 3\%$ of full scale.
 - Input Impedance 200,000 ohms.

Write for Catalog Sheet Giving Full Information — Or Contact Us Concerning Your Own Individual Problems. Our Staff is at Your Service. Write Dept. A

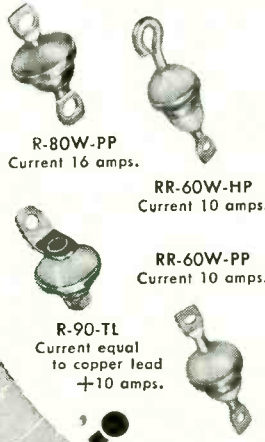


C. G. S. LABORATORIES, INC.
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Announcing: AN IMPORTANT ADDITION TO THE E-I FAMILY OF SEALED LEADS—

NEW R and RR SERIES TERMINALS



A completely new line of double barrel terminals that provide added protection against flashover without any appreciable increase in terminal size. The double barrel results in a longer leakage path on both ends of the terminal while the upper barrel increases the mechanical strength of the terminal and facilitates soldering. For information call or write today.

- Write for These Descriptive Bulletins:
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E-I INC. ELECTRICAL INDUSTRIES
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Timing Ideas

PRECISION PERFORMANCE

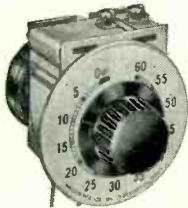


Manufacturers, recognizing that components of quality insure outstanding product performance, look to Haydon® at Torrington for timers and timing devices. All Haydon timers are made with the same precision as the Haydon motor — your guarantee of satisfactory performance. If you need a special design, you'll find Haydon's extensive engineering and development facilities without equal for service and results.

A few examples of basic Haydon timing units are featured below.

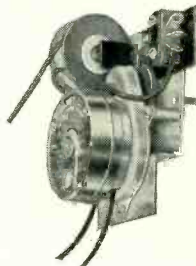
SERIES 8010 INTERVAL TIMER WITH BUZZER

Compact, low cost timer for volume production. Wide range of intervals. Audible (buzzer) signal optional. Quick break. Load contact rated 10A, ½ HP 250 VAC.



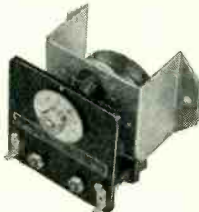
SERIES 8006 INTERVAL TIMER

Designed for heavy duty, this unit is available in quantities in standard models. Wide range of intervals. HOLD feature optional. Quick break. Totally enclosed. Switch rated 28A, 1 HP 250 VAC.



SERIES 5900 TIME DELAY RELAY

For use where positive, accurate time delay relay is imperative. Automatic reset. Fixed models for volume production; adjustable models in 4 delay ranges for general use.



SERIES 5700 ELAPSED TIME INDICATOR

Synchronous timing motors with cyclometer type counters for metering elapsed time. Rugged models for wide range of timing, recording operations; in several registers, resettable or non-resettable.

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For complete design and engineering specifications, write for catalog: Timing Motors No. 322 — Timers No. 323 — Clock Movements No. 324. Yours without obligation.



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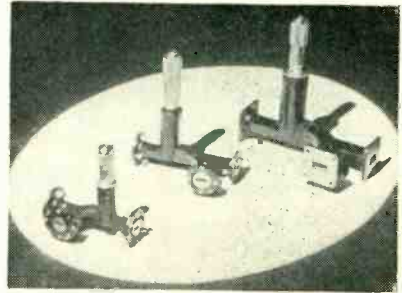
HAYDON Manufacturing Co., Inc.
2425 ELM STREET

TORRINGTON, CONNECTICUT
SUBSIDIARY OF GENERAL TIME CORPORATION

NEW PRODUCTS

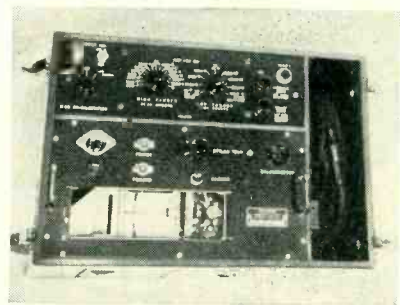
(continued from page 130)

voltage supply that is continuously variable from 100 to 325 v and delivers from 0 to 150 ma, with a ripple of less than 5 mv; and a bias supply that is continuously variable from 0 to 150 v and delivers 5 ma. Its a-c output is 6.3 v, 10 amperes, center-tapped, unregulated.



Cavity Frequency Meters

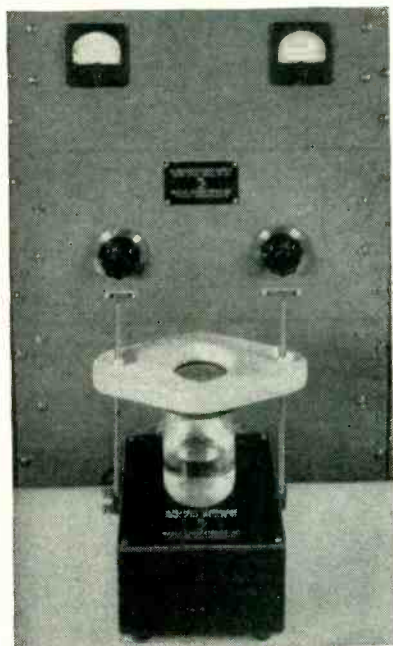
SPERRY GYROSCOPE CO., Great Neck, N. Y. The cavity frequency meters illustrated are low-Q broadband instruments designed for both transmission and absorption indications. They are extremely useful for general search-type frequency measurements in the laboratory and in the field; and may also be used for setting oscillators and signal sources to a predetermined frequency with an accuracy of 0.1 percent. Model 348 is designed for the 13,000 to 18,000-mc range; model 349—19,000 to 26,000 mc; and model 350—26,500 to 39,000 mc. Each model consists of a cylindrical cavity with one end joining the broad side of a standard section of waveguide. The cavity is tuned by means of a plunger which is driven by a micrometer head. Individual calibration curves are furnished with each instrument.



Recording Instruments

MILLIVAC INSTRUMENT CORP., P.O. Box 3027, New Haven, Conn., has

available a series of direct-reading recording instruments of unusual voltage and current sensitivity. The MR-61A has a sensitivity of 3×10^{-12} amperes per mm of deflection; the MR-67A has $20 \mu\text{v}$ per mm and an input impedance of 6 megohms; and the MR-65A, a maximum sensitivity of $0.2 \mu\text{v}$ per mm with an input impedance of 1,000 ohms. Chart width is 5 centimeters. Standard paper speeds are 25 and 10 mm per second. Frequency range is d-c to 20 cycles for the 61A and 67A, and d-c to 10 cycles for the 65A, all within 3 db.

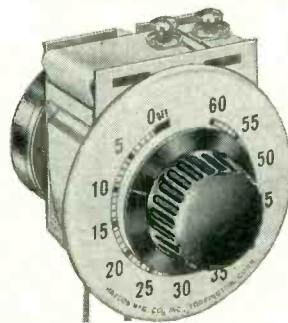


Ultrasonic Generator

MASSA LABORATORIES, INC., 5 Fottler Rd., Hingham, Mass. Model GA-1010 ultrasonic equipment has been made available to meet the demands of industrial laboratories where the higher frequency quartz crystals were not found satisfactory. It includes a 1-kw magnetostriction transducer, operating at approximately 24 kc and having an exposed flat vibrating surface of 20 sq cm. The structure is oil filled and is provided with a water-cooled radiator to permit the continuous long-time operation of the apparatus without harmful temperature rise. The ultrasonic power supply equipment for operating the transducer is operated from 115-v, 60-cycle power mains. In addition to safety interlocks and relays, the

Timing Ideas

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IF you're looking for a rugged, heavy duty interval timer, this Haydon® unit will save you time and money. It will meet every test for stamina, dependability and efficiency; is designed as a versatile, multi-purpose unit. Whatever your need for an interval timer may be, see the Haydon Series 8006 first.

CHECK THESE 8006 FEATURES

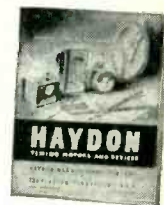
1. Standard models for intervals of 1, 15, 60 and 180 minutes; dial and knob optional.
2. Other models for intervals up to 24 hours or more are available, without dial or knob.
3. HOLD feature furnished if wanted.
4. Heavy duty switch is rated 28A, 250 VAC; 1 HP 250 VAC.
5. Heavy contact pressure; ample follow-through is assured.
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7. Removable dust cover for timer; totally enclosed motor.
8. Settable in either direction, to start or when operating.
9. May be used under conditions of high temperature and humidity.

ALL HAYDON TIMING DEVICES GIVE YOU

these advantages of the dependable Haydon Motor: Total enclosure — Very small size — Slow (450 rpm) rotor for long life, quiet operation — Controlled lubrication with separate systems for rotor and gear train — Mounting and operation in any position.

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EISLER Television Tube MACHINERY



No. 102-VID



No. 57-VID

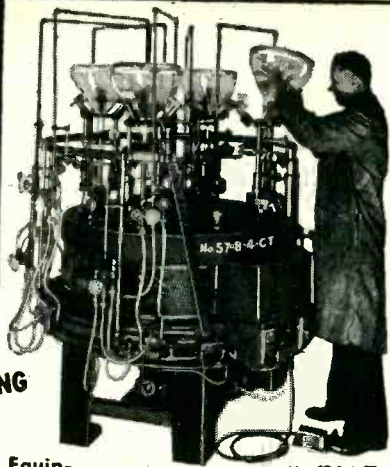
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- PRODUCTION ENHANCING

EISLER'S Electronic Equipment is especially Designed and Built to your exact requirements.
From 5" to huge 24" Television Tube

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- Consultation without any obligation on your part is cordially invited.

EISLER ENGINEERING CO., INC.
751 SOUTH 13th ST. • NEWARK 3, NEW JERSEY



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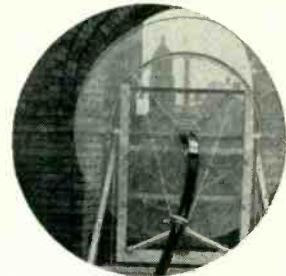
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AN ELEPHANT'S TRUNK!

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Molded directly to cable as one-piece Neoprene units MINES electrical connectors are Jerk-proof, Shatter-proof and Wear-resistant—Special construction and resilient rubber mounting of pins and spring loaded sockets insure a long life of low contact resistance—and the famous MINES Water-Seal automatically protects connections from dirt, oil or water.

A wide variety of sizes, shapes and pin combinations are available to meet the portable power requirements of TV, FM, AM or PA Circuits. No. 4A093 Male plug illus.

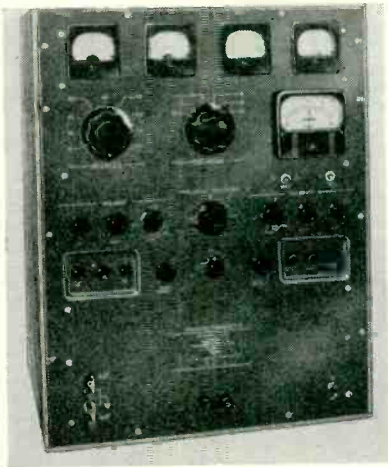
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power supply includes dials for adjusting the frequency and output.



Phase Meter

THE W. L. MAXSON CORP., 460 W. 34th St., New York 1, N. Y. Model P-1060 phase meter, originated as an aid to design of single-sideband transmitters by the U. S. Air Force, provides means for precise determination of phase relationships throughout the audio spectrum of 30 to 20,000 cps. The instrument is accurate to 0.1 degree. Its self-calibrating feature permits the operator quickly to check accuracy without recourse to complex calibrating apparatus and techniques. The power supply for the electron-tube circuits is integral with the instrument chassis. It is designed to operate from an unregulated 105 or 125-volt, 60-cycle circuit.



Oscillograph Tube

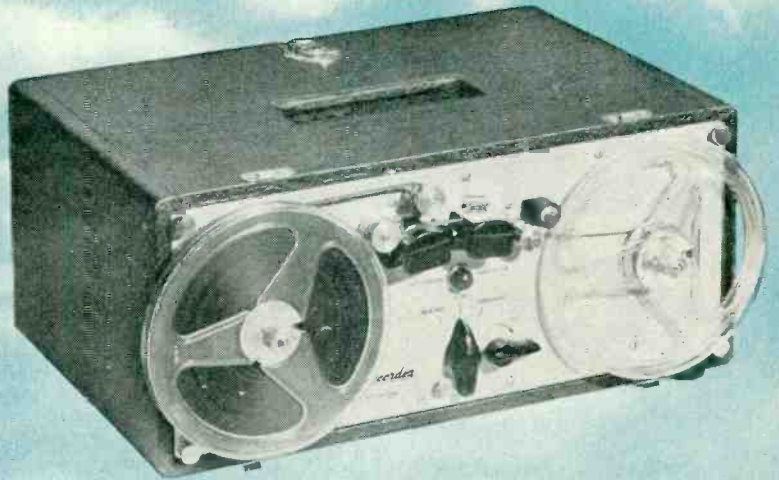
RADIO CORP. OF AMERICA, Harrison, N. J. Model 7JP1 is a 7-in. c-r tube of the electrostatic focus and deflection type designed to provide excep-

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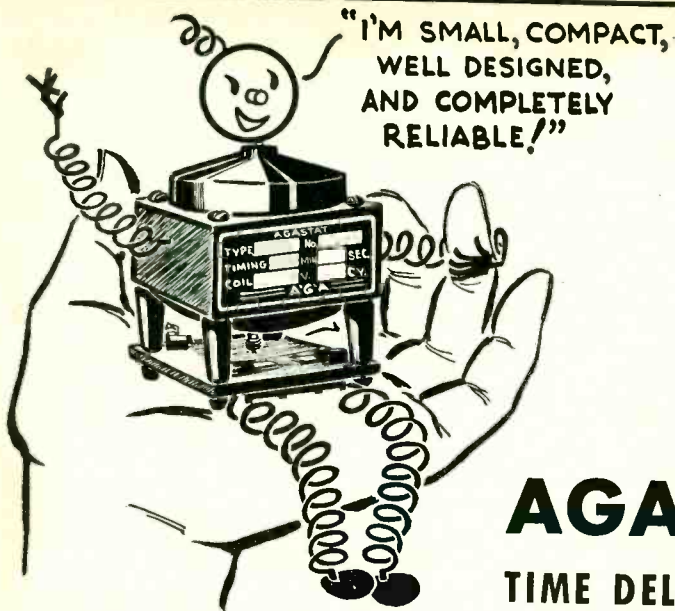
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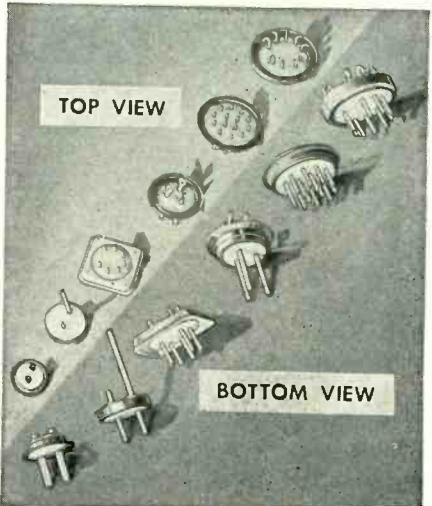
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Marine Radios

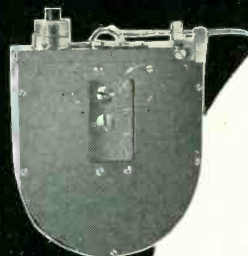
STANDARD ELECTRONICS CORP., 25 W. 43rd St., New York 18, N. Y., is producing four types of marine radios ranging in power from 12 to 80 watts and designed to cover pleasure and commercial craft requirements. The 12-watt unit for small boats includes a standard broadcast band that can pick up all radio broadcasts available from shore. Another model, 15 in. wide x 9 in. deep, operates at 35 watts and has 5 channels. The 50 and 80-watt units both have six transmitting and receiving channels. All operate on low battery drain and feature complete high-precision low-drift crystal control of each transmitting and receiving channel.



Null Detector and VTVM

THE FREED TRANSFORMER CO., INC., 1718-36 Weirfield St., Brooklyn 27, N. Y. The No. 1210 null detector and vtvm has been designed for a-

Edin instruments



OSCILLOGRAPH GALVANOMETER

No's. 8001, 8002, 8003 and 8004 ink-writing galvanometers have sensitivities from 3.5 to 40 volts per cm., resonant frequencies from 15 to 120 cps., resistances from 1000 to 2000 ohms, frequency response up to 350 cps., and a single-jewel pivot construction. Units are designed for multiple operation up to 10 channels in a total width of 12 inches.



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No. 8100 direct coupled amplifier has a voltage amplification of 13,000 with a maximum output of 70 volts. Frequency response from d.c. to 10,000 cps. is flat within 10%. Input impedance is 2 megohms; output impedance is 150 ohms. Input may range from 0.1 mv. to 100 volts. Stability is better than 0.1 mv. per thirty minutes, or 0.5 mv. per day. Attenuator is stepped for factors from 1 to 1000.



OSCILLOGRAPHS

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No. 8121 special amplifier has a time constant of 1 second, an exponential response to a square wave at high gain, input impedance of 1 megohm, and input from 0.1 mv. to 1000 volts. At low gain, No. 8121 becomes a DC amplifier with a voltage gain of 100 and an input of 10 mv./mm.

HIGH-GAIN AMPLIFIER

No. 8130 amplifier has a voltage gain of 1,000,000 and includes a built-in pre-amplifier. Frequency response is from 1 to 200 cps. Input may range from 10 microvolts to 100 millivolts. This amplifier is particularly suited for Biological studies.

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- GALVANOMETERS
- No. 8100 AMPLIFIER
- No. 8130 AMPLIFIER
- SPECIAL (Enclose details)

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ALMO RADIO COMPANY

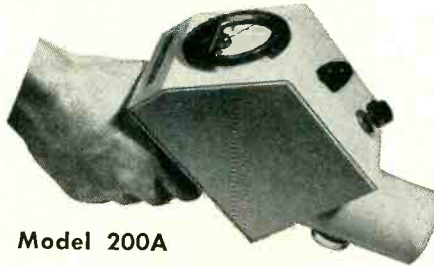
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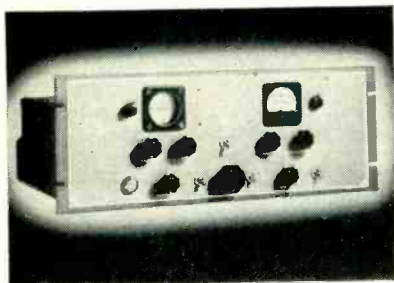
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bridge measurements. It provides simultaneous measurement of the voltage across the unknown and the balance of the bridge. The vtvm has a sensitivity of 0.1, 1, 10 and 100 volts. Input impedance is 50 megohms shunted by 20 μ f. Frequency range is from 20 cycles to 20,000 cycles. Null detector gain is 94 db.



Multiplier Photometer

PHOTOVOLT CORP., 95 Madison Ave., New York 16, N. Y. Series 520 line-operated supersensitive electronic multiplier photometer is designed for the exact measurement of extremely low light values down to 1/10,000 microlumen. The model 520-A illustrated is intended primarily for density measurements. It has an indicating meter of logarithmic response. The top scale of the meter is calibrated in optical density and has approximately uniform divisions of 0.02 density. The bottom scale is a photometric scale that reads light intensities in arbitrary units from 0 to 100. Bulletin 360 gives a complete description and price list for the line.



R-F Shift Converter

NORTHERN RADIO Co., INC., 143 W. 22nd St., New York 11, N. Y. Type 107 model 2 radio-frequency shift



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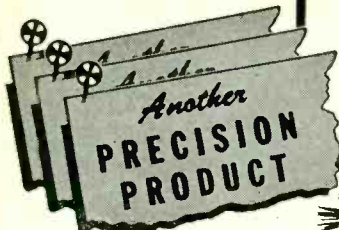
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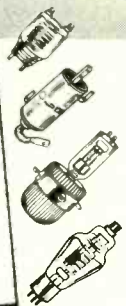
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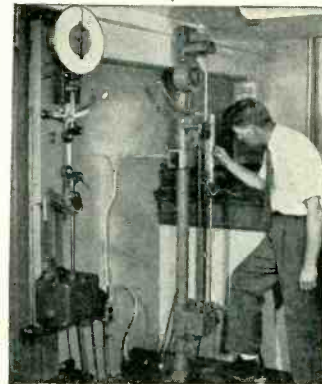
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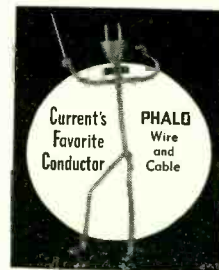
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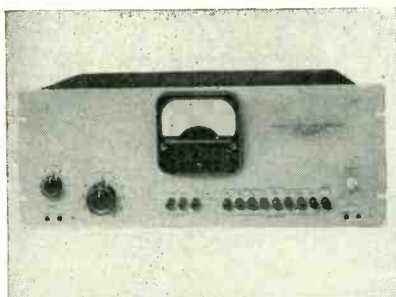
Corner of Commercial Street
Worcester, Mass.

converter is a dual-channel unit which converts mark and space tones into d-c pulses and drives teleprinters, tape and other recorders directly. Its integral 2-in. oscilloscope provides an outstanding tuning pattern for precise receiver adjustment during initial setup and while keying. It is capable of keying speeds up to 600 wpm. The unit also features 100 to 1,000-cps frequency shift. Mark frequency is set at 2,975 cps.



Frequency Standard

AMERICAN TIME PRODUCTS INC., New York City, N. Y. Type 2005 frequency standard is a compact source of accurate frequency at a commonly needed power level. It is useful in running small motors, timers and clocks; also in making frequency measurements, providing timing marks in oscillographs and high-speed cameras. Output frequency is 60 cycles, accurate to 1 part in 100,000 in a temperature range from 0 to 60 C. Output power is 10 watts at 115 volts approximate sine wave. Input is 115 volts, 50 to 400 cycles at 45 watts.



Distortion and Noise Meter

DAVEN Co., 191 Central Ave., Newark 4, N. J. Type 35-A distortion and noise meter provides a rapid accurate means of measur-

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PRECISION POTENTIOMETERS

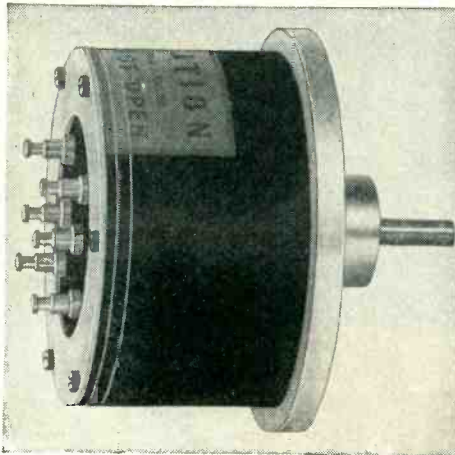
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We invite your inquiries and specifications.

Write for Bulletin F-68.

THE GAMEWELL COMPANY
Newton Upper Falls 64, Massachusetts



A minor modification of the standard sinusoidal potentiometer type RL-11-C (as illustrated) permits operation up to 1800 RPM. After a test of 28 million cycles at 1800 RPM, one of these units showed negligible wear.



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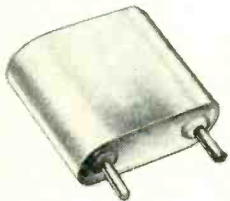
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JK Stabilized H17

Frequency range 200 kc to 100 mc. The pin spacing is such that two units can be mounted in a loctal socket. A small extremely light weight hermetically sealed unit. Moisture and dustproof. Designed especially for use where space is at a premium. The crystal is plated and wire mounted. Pin diameter of the H17 is .050".


The H17L and the H17W are also available in the same frequency range. The H17L has a pin diameter of .093", and the H17W has wire leads.



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ing distortion, noise and hum level in audio-frequency equipment. No balancing or time-consuming tuning is required to make measurements. A pushbutton balances the unit automatically. The fundamental circuit of the meter comprises a series of eight fixed band rejection filters covering the 50-cycle to 15-kc range, followed by a stable, high-quality, wide-range (50 cycles to 45 kc), high-gain amplifier. Two amplifier gain controls are provided—one a step type covering the range +40 to -60 in 10-db steps; the other a continuously variable control covering the ± 10-db range.



Frequency Standard & Test Set

FREED TRANSFORMER CO., INC., 1718-36 Weirfield St., Brooklyn, N. Y., have introduced the model 1360 frequency standard and test set. It consists of a crystal-controlled oscillator, a modulator and a c-r oscilloscope for observation of Lissajous figures. Accuracy is better than 2 cycles or 0.1 percent, whichever is greater. Main advantages are the ease of adjustment procedure and the fact that any low-frequency oscillator can be used as an audio-frequency source for alignment of telemetering equipment. Catalogs and price lists are available.

Tape Recording Head

SHURE BROTHERS, INC., 225 W. Huron St., Chicago, Ill. Model TR5 tape recording head combines the functions of record, playback and erase in a single unit with excellent frequency response and output level. A special feature is the use of a deep-drawn mu-metal shield for optimum hum reduction. Record and playback coil impedance is

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In other respects, too, Sessions Switch-Timer movements are distinctively different from conventional clocks. There's no center-disc, and clock hands are easily readable. What's more, the low speed

motor is "kitten-quiet" without annoying buzz from high speed gears.

Other outstanding features include: "Sleep-Slector" lullaby switch on some models to turn radio off automatically at any preset time up to 90 minutes; automatic radio shut-off 1½ to 2 hours after timer turn-on (for the forgetful), 10 and 15 amp. switch (UL approved). In addition, you have your choice of front or back controls, round or square bezel, etched or screened numerals, luminous or in any color. Dial and hand styling to specifications. All movements factory tested and guaranteed for one year. Feel free to inquire for details, or send coupon below for catalog.

Sessions

SWITCH TIMERS

The Sessions Clock Company, Timer Div., Dept. 4, Forestville, Conn.

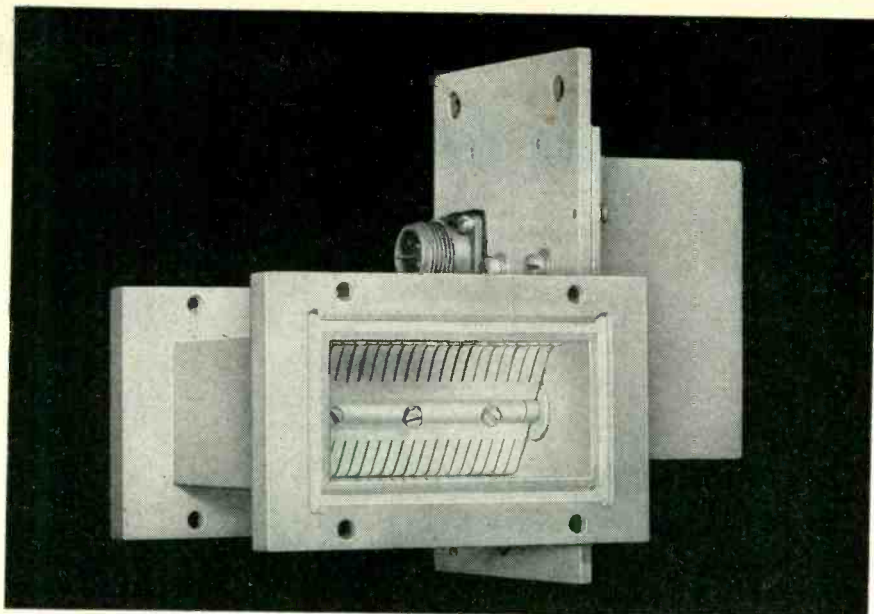
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Microwave "Shutter" by TERPENING

The "shutter" you see in the waveguide section above is designed to close automatically when the radar is not operating. This prevents damage to the crystal detector, which might be caused by radiation from other nearby radars.

Specifications called for very high attenuation when closed, extremely low attenuation when open, and fully automatic operation.

As designed and produced in quantity in our plant, the performance of this component exceeded our customer's expectations. For example:

- with the solenoid-actuated shutter in closed position, attenuation is greater than 40 db,
- with shutter open, attenuation is negligible—a few hundredths of one db.

This is a typical example of the work we are set up to handle—from design through production—from single component to entire transmission line. Although our engineering staff, laboratories, and fully equipped shop are usually busy on government contracts, our unusual facilities may permit us to work with you on special components for military microwave systems. We shall be happy to talk with you about your present and/or future needs.



L. H. TERPENING COMPANY

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TRADE MARK

1,650 ohms at 1,000 cps, while erase coil impedance is 1,000 ohms at 40 kc. Output level is 5 db above 1 mv at 1,000 cps at tape speed of 3.75 in. per second. Overall dimensions are 0.685 in. maximum height, 1.240 in. wide and 1.031 in. deep.



Amplifier Kit

TRIAD TRANSFORMER MFG. CO., 2254 Sepulveda Blvd., Los Angeles 64, Calif., has introduced the HF-10 amplifier, produced especially for those who like to build their own sound reproducing systems. It features a frequency response within 1 db from 20 to 20,000 cycles. Distortion is less than 2 percent from 50 to 18,000 cycles at full 10 watts output; less than 1 percent from 20 to 20,000 cycles at 5 watts. Gain is 74 db from crystal microphone or radio receivers, 96 db through pre-amplifier. Complete specifications, circuit diagram and prices are shown in bulletin HF-10.



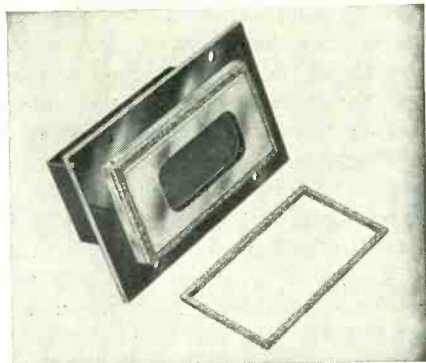
Counting Rate Meter

RADIOACTIVE PRODUCTS, INC., Detroit 26, Mich., announces the model C-2, 3 counting rate meter for use with Geiger tubes. The instrument has application in monitor installations and also in the recording of x-ray diffraction patterns and other transient phenomena. Pulse inte-

**"We have found
Metex Electronic Gaskets
excellent for HF currents
inexpensive to assemble."**
Sylvania Electric Products Inc.

Sylvania has been using Metex gaskets for over a year as conductive shields for their TR tubes used in radar and micro-wave ranging equipment.

To quote their experience: "We have found Metal Textile knitted wire gaskets excellent for conducting high frequency currents without boundary arcing. The gaskets are resilient, and yet do not deform too readily. Best of all, the material is inexpensive to assemble through soft soldering techniques."



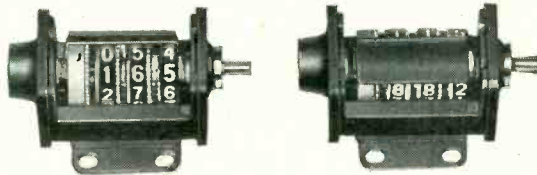
A Sylvania Electric TR tube showing Metex gasket loose and in position

The properties—electrical and physical—which make Metex Electronic Gaskets effective in this, and other demanding HF and UHF applications are due to their being made from *knitted* (not woven) wire mesh. The hinge-like action of the knitted mesh permits controlled resiliency of the finished gaskets. These can be die-formed to close dimensional tolerances, when required. There is practically no limit to the metal or alloy which can be used.

If the equipment you are manufacturing or designing requires a resilient conductive or shielding material, our engineers will welcome the opportunity of working with you. A letter, addressed to Mr. R. L. Hartwell, Executive Vice President and outlining your requirements, will receive immediate attention.

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Companion shutter counters used as dual direction indicators. One counter adds while the other subtracts. Shutter blanks out counter which is on negative side of 000.



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These are a few of the "specials" developed by Durant for Radar and Electronic applications. When one of the many standard Productimeters is not the exact answer to a problem, Durant engineers modify, combine, or develop entirely new counters to meet the particular requirements of the job.



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grating circuit of the Geiger-tube power supply is adjustable to full-scale ranges from 100 to 50,000 counts per minute. Response time of the circuit is independently variable from 480 seconds to 0.1 sec. Better than 1-percent circuit linearity has been achieved and provisions for driving an external recording meter are provided.

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Literature

Deflection Amplifier. Sylvania Electric Products, Inc., Emporium, Pa. Three loose-leaf perforated catalog sheets cover the type 6BL7GT duotriode deflection amplifier. Included are ratings, typical operating conditions, physical specifications, circuit applications and characteristics charts.

Switch Listings. Unimax Switch Division, The W. L. Maxson Corp., 460 W. 34th St., New York 1, N. Y. Makers and designers of equipment for the armed forces will find useful information about precision, snap-acting switches in the interchangeability guide recently issued. It is pictorially indexed with outline drawings of switches used in aircraft and other applications requiring precise control or



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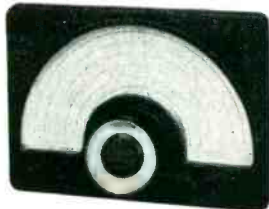
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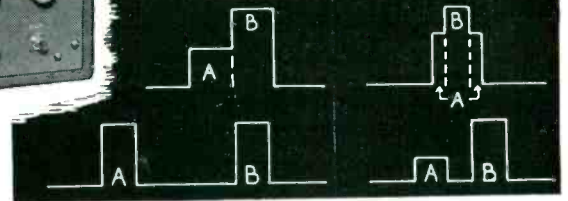
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TYPICAL PULSE COMBINATIONS



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PULSE DURATION individually adjustable from 0.15 to 1.5 microseconds; RISE TIME is .05. DECAY TIME 0.10 microseconds. SPACING between pulses variable from -0.5 to +10 microseconds. REPETITION RATE adjustable in 3 ranges, 1 to 10, 10 to 100 and 100 to 1000 cycles; can be externally triggered. OUTPUT IMPEDANCE approximately 400 ohms, maximum output voltage, -200 v. CONTROL CALIBRATION ACCURACY $\pm 5\%$ over entire range.

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COMPLETE INFORMATION is yours for the asking; please request Bulletin E-902.

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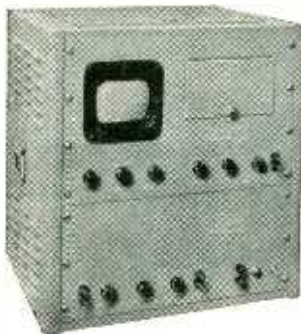
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Resolution: Continuously variable from 2KC to better than 500 CPS.



PANADAPTOR SA-3, SA-6 PANALYZOR SB-3, SB-6 For General RF Spectrum Analysis

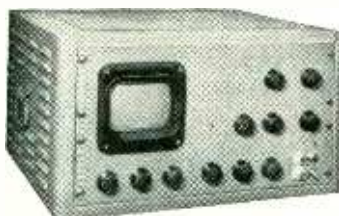
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limit switching, lists AN numbers and gives the corresponding company type numbers.

Radio In Petroleum Industry. General Electric Co., Syracuse, N. Y., has available a new booklet covering broadly the use of two-way radio in the petroleum industry. It treats the general uses of two-way equipment, types of systems, licensing regulations, equipment capabilities, special installations, relaying, costs of installations and savings experienced by operators using two-way radio in their work.

Regulated Power Supply. Oregon Electronics, 206 S. W. Washington St., Portland 4, Oregon. Bulletin 53* covers the model D6 dual-output, heavy-duty, regulated power supply. The unit treated supplies d-c continuously variable from 0 to 600 v at 400 ma. Chief features and technical specifications are given.

Lever Key. Circuit Controls Co., 3201 Peoria St., Steger, Ill. A single-sheet bulletin describes the model 1 lever key intended to be used in medium-duty multiple-circuit switching. Illustrations, typical applications and general ordering information are included.

Rotary Switches. Electro Switch Corp., 167 King Ave., Weymouth 88, Mass. Rotary multiple tap and transfer switches that conform to Navy and Underwriters' Laboratories requirements are described in catalog 1950-JR. Sectional, cut-away and exploded views of typical switches show details of the design. Contact possibilities shown include single- and double-break as well as shorting and non-shortening action. Four-, eight- and sixteen-position switches are listed.

Audio Equipment. Sun Radio & Electronics Co., Inc., 122-124 Duane St., New York, N. Y., has ready for distribution the new edition of its 100-page audio equipment handbook. A large section is devoted to questions and answers most common to high-fidelity aspirants or owners. The balance of the handbook contains listings, prices and information on hundreds of components and subas-

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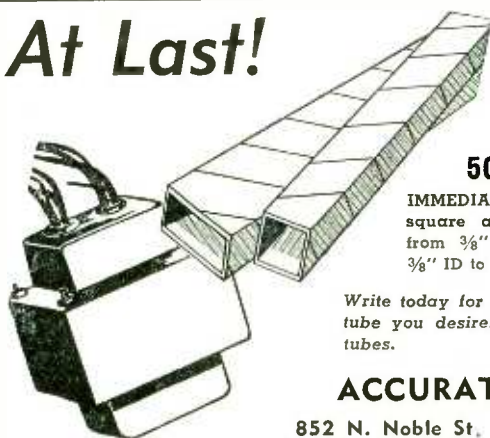
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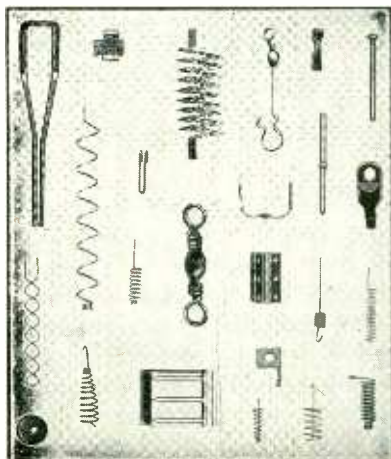
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Radio Hook-Up Wire. Rome Cable Corp., 330 Ridge St., Rome, N. Y. Three data sheets describe the various standard types of radio hook-up wires now available. Those included are Underwriters' Laboratories' approved thermo-plastic types for 90 C and 80 C temperatures, rubber-insulated types for 75 C temperature and military approved types WL, SRIR, SRHV, SRI and SRIB. The insulation thicknesses and coverings as shown in the tables are required on approved types, or as noted.

Relay Catalog. Potter & Brumfield, 221 N. Main St., Princeton, Indiana. The 24-page catalog 109 contains new information on relays, shaded-pole motors and timers. Its comprehensive presentation facilitates ordering procedure, offers valuable assistance in development problems and in selecting the proper type relay to meet every requirement. Fully illustrated, the catalog contains pictures and schematic drawings of over 150 models, showing accurate over-all and mounting dimensions. Easy-to-read charts list complete coil and contact data on every relay.

Insulation Tape. Insulation Manufacturers Corp., 565 W. Washington Blvd., Chicago 6, Ill. Complete application and technical data on Silastic tape, Type R class H electrical insulation are given in bulletin 680. The type described, made by coating woven glass cloth with a partially vulcanized silicone rubber, is an extremely flexible insulation combining the heat stability qualities of the silicones, the resilience of rubber-like materials and the excellent physical and nonflammable properties of glass.

Portable F-M Radiotelephone. Doolittle Radio, Inc., 7421 S. Loomis Blvd., Chicago 36, Ill., has issued a 2-page bulletin on the Littlefone portable f-m radiotelephone that now provides increased power and range to facilitate 2-way communication in many fields of operation. The unit described

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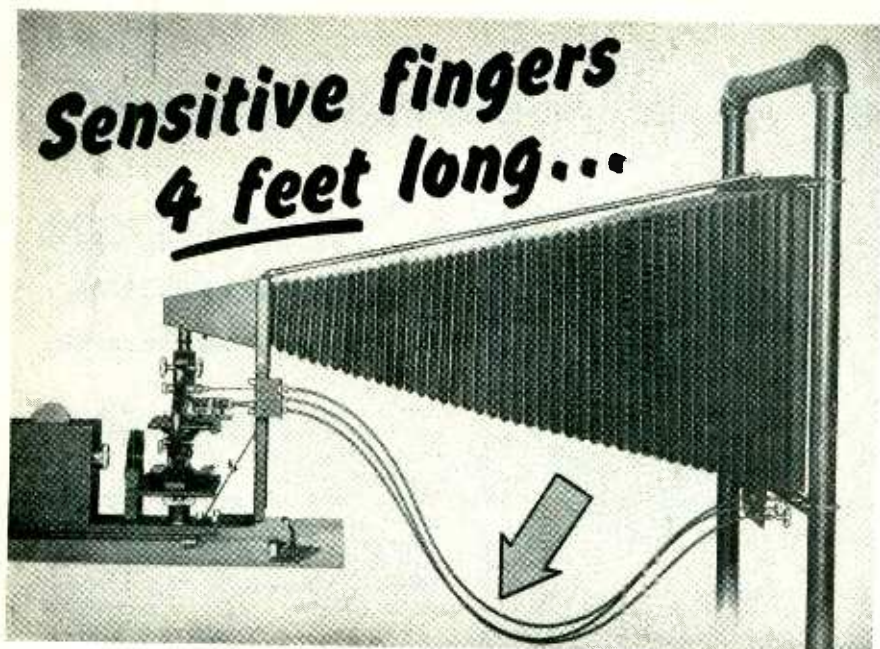


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Acrylic Extrusion Molding Powder. Rohm & Haas Co., Washington Square, Philadelphia 5, Pa., has published a technical bulletin showing the recent modifications in Plexiglas VM acrylic molding powder that have made it as easily handled for extrusion as for injection molding. Physical properties of the powder described are unchanged but the improved formulation makes possible extrusions by standard techniques, with oven drying usually sufficient.

Tube Data. Sylvania Electric Products Inc., Emporium, Pa. Three recent technical data bulletins cover the type 5845 emission limited control diode, type 6CD6G beam power amplifier and type 6W6GT beam power amplifier respectively. Ratings, typical operating conditions, circuit applications, physical specifications and characteristics charts for each are given.

Spectrum Analyzer. Vectron, Inc., 235 High St., Waltham, Mass. A recent 2-page bulletin describes the spectrum analyzer, a superhet receiver with a 5-in. c-r oscilloscope output indicator. An illustration of the unit is included, and its chief uses and technical specifications are given.

Miniature Test Equipment. Oak Ridge Products, 239 E. 127 St., New York 35, N. Y., has literature available on its line of miniature test equipment. It includes mailing pieces, a reprint of an advertisement and a reprint of a technical article dealing with the model 103 signal generator; model 101 substitution tester and model 102 high-voltage meter. Chief features, technical data and prices are shown.

Transmitter Kit. E. F. Johnson Co., Waseca, Minn. Catalog 705 is a four-page treatment of the Viking I transmitter kit, a completely

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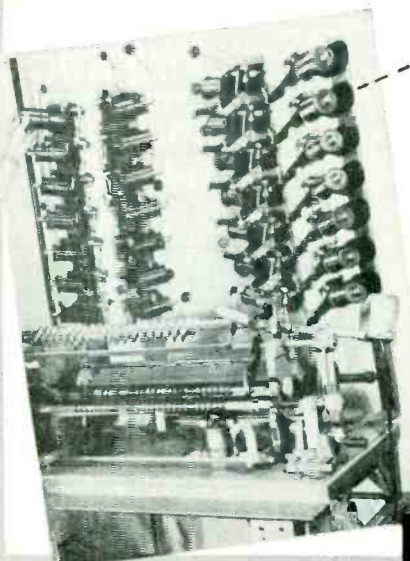
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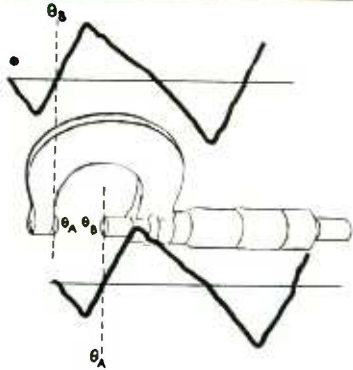
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TIC's New 320-A Phase Meter is the first commercially available instrument for the direct measurement of the phase difference between two recurrent mechanical motions or two electrical signals independent of amplitude, frequency, and wave shape.

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In audio facilities, ultrasonics, servomechanisms, geophysics, vibration, acoustics, aerial navigation, electric power transformation or signaling . . . in mechanical applications such as printing register, torque measurement, dynamic balancing, textile and packaging machinery and other uses where an accurate measure of the relative position of moving parts is required . . . the Phase Meter is a long needed measuring instrument never before available—a new tool for a heretofore neglected field of measurement.

Price: Relay Rack Mount \$525.00. Cabinet for above \$25.00

**Add Type 500-A Wide Band
Decade Amplifier**

Designed for use with the phase meter at voltage levels below one volt and as a general purpose laboratory amplifier—features high gain negligible phase shift and wide band width. Unique circuitry—which employs three cathode followers—offers wider frequency range, higher input impedance and lower output impedance than other types. Panel switch selects proper feedback compensation when either optimum amplification or phase shift operation is desired. Outstanding specifications: Amplification—10; 100; 1000 selected by rotary switch . . . Accuracy—±2% nominal . . . Frequency response—±0.5db from 5 cycles to 2 mc on gain of 10; ±0.5db on 5 cycles to 1.5mc on gain of 100; ±0.8db from 5 cycles to 1mc on gain of 1000 . . . Phase shift—0 ± 2° from 20 cycles through 100 kc . . . Gain stability—constant with line voltages (105-125v).

Prices: Single Type 500-A in cabinet, \$205.00 (Rack mount, \$200.00)
Dual Type 500-AR in cabinet, \$425.00



TIC TECHNOLOGY INSTRUMENT CORP.
1058 Main Street, Waltham 54, Massachusetts

Engineering Representatives

Cleveland, Ohio—Prospect 1-6171 Manhasset, N. Y.—Manhasset 7-3424 Chicago, Ill.—Uptown 8-1141
Boonton, N. J.—Boonton 8-3097 Rochester, N. Y.—Genesee 3547-M Cambridge, Mass.—Blair 4-1731
Canaan, Conn.—Canaan 849 Hollywood, Cal.—Hollywood 9-6305 Dayton, Ohio—Michigan 8721, Dallas, Texas—Dixon 9918

designed and engineered transmitter furnished unassembled but complete in every detail including wiring harness and ample assembly instructions. A circuit diagram of bandswitching the 10 to 160-meter transmitter is included.

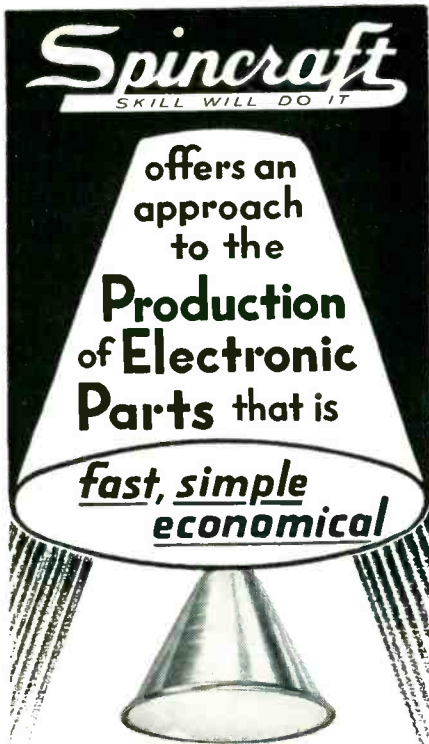
Fast Pulse Amplifier. Hewlett-Packard Co., 395 Page Mill Road, Palo Alto, Calif. Volume 1, No. 11 of the Journal is a well illustrated description of the model 460B fast pulse amplifier, which is designed for a maximum output level of 125 volts open circuit—high enough to give more than full deflection on the type 5XP- c-r tube or a 2-in. deflection on a type 5CP- tube. Prices for the unit and its various accessories are shown.

F-M & TV Antenna. Tricraft Products Co., 1535 N. Ashland Ave., Chicago 22, Ill. Technical information on the new P-38 uni-directional f-m and tv antenna is found in a single-page bulletin. Among the features of the unit described are peak reception on all channels, seven separate and distinct radiating elements, and a 23-degree beam which rejects ghosts, interference and noise.

Cathode-Ray Tubes. Sylvania Electric Products Inc., Emporium, Pa., has published a 12-page booklet tabulating characteristics of 194 c-r tubes for tv receivers, oscilloscope and radar applications. The tubes described include 103 designed for magnetic deflection and 91 electrostatic types with screen sizes ranging from 2 to 22 inches. Data supplied includes: heater current and voltage; nominal dimensions, basing, persistence and fluorescence of screen; maximum design center ratings; and typical operating conditions.

TV Field Equipment. Radio Corp. of America, Camden 2, N. J. Form 2J-6881 is a six-page illustrated folder giving information on the company's latest field tv equipment, including an improved friction head, a new tripod, new field desk, and a rotatable mount and remote control for microwave parabola.

Radioactivity Measurement. Landsverk Electrometer Co., Pip-



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A 1	74	1.7	0.11	0.36
A 2	74	1.3	0.24	0.44
A 34	73	0.6	1.5	0.88

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C 1	7.3	150	2.5	0.36
PC 1	10.2	132	3.1	0.36
C 11	6.3	173	3.2	0.36
C 2	6.3	171	2.15	0.44
C 22	5.5	184	2.8	0.44
C 3	5.4	197	1.9	0.64
C 33	4.8	220	2.4	0.64
C 44	4.1	252	2.1	1.03

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NEW PRODUCTS

(continued)

pin Road, Cincinnati 31, Ohio. The model L-75 analysis unit, an instrument for radioactivity measurement, and its accessories are illustrated and described in bulletin A-2. Construction, operation, sensitivity and advantages, as well as other uses of the unit, are discussed.

Testing Facilities & Services. Inland Testing Laboratories, 2745 Janssen Ave., Chicago 14, Ill., announces a new 24-page, fully illustrated brochure covering the test facilities, equipment and their capabilities of an organization specializing in complete qualification testing of components and assemblies made under government contracts in accordance with military specifications.

Pressuregraph and Supplementary Instruments. Electro Products Laboratories, Inc., 4501 North Ravenswood Ave., Chicago 40, Ill. This bulletin gives features and specifications for the company's Pressuregraph, Syncro-Marker, and Dynamic Micrometer. Illustrations of the equipment are shown.

Vibration Test Equipment. The Calidyne Co., 751 Main St., Winchester, Mass. Bulletin No. 4401 describes the company's model 44 Shaker and its associated rotary power supply and console, models 45A and 45B. Included are installation details, a listing of outstanding features of the equipment, and guaranteed performance curves.

Television Equipment. Polarad Electronics Corp., 100 Metropolitan Ave., Brooklyn 11, N. Y., has issued a new catalog on television equipment for broadcast, manufacturer and laboratory use. It fully describes in 14 pages a line of television cameras, synchronizing generators, monitors, tv amplifiers and tv power supplies designed for broadcast operation.

TV Antenna Gain Chart. Technical Appliance Corp., Sherburne, N. Y. Engineering bulletin No. 64 contains actual measurements in db gain over half-wave dipoles for all popular antenna types. It is helpful to the serviceman in select-

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McGRAW-HILL publications

ELECTRONICS — January, 1951

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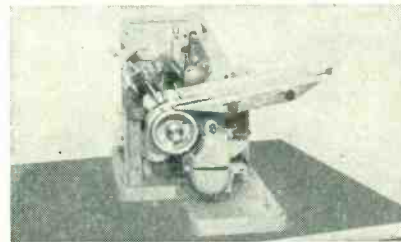
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The MARKEM 20A — marks radio tubes, miniatures, resistors, capacitors, and other cylindrical objects clearly, durably with Markem rubber plates and quick-drying, heat-resistant inks.

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MARKEM machine
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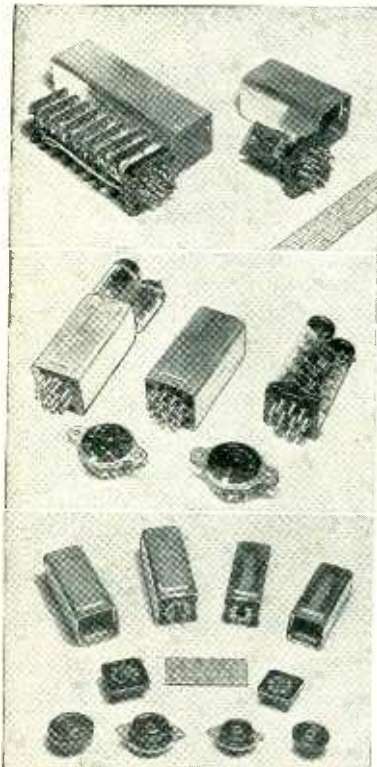
Keene 27,
New Hampshire

ALDEN COMPONENTS FOR PLUG-IN UNIT CONSTRUCTION

Until recently there has been no one place where components specifically designed for plug-in unit construction were available. It was necessary for engineers to design and have parts custom made or improvise with standard components in makeshift arrangements. To provide the type of design necessary, Alden engineers are working with the industry developing a whole series of components specifically for plug-in construction.

The first problem undertaken by Alden engineers was a base specifically for plug-in unit construction. . . . the conventional tube type bases proved unsatisfactory; they didn't stand up, the boss broke and the pins bent. To overcome these difficulties Alden designed an entirely new base. . . . the Non-Interchangeable Series bases have no molded center boss to break, pins are strong and stubby—do not bend or break out and are Non-Interchangeable to prevent danger of mismatching and costly burned out units.

Out of this work we feel that Alden's is the one place where you now can take your unitizing problems and obtain the standard bases, sockets, mountings and housings to answer most of your needs. As illustrated below, the Alden Non-Interchangeable and miniature bases have tremendous flexibility and are fast becoming the standard for plug-in construction.



20 PIN NON-INTERCHANGEABLE BASES & SOCKETS

The scope of the Alden "20" base as a mounting medium is almost unlimited. . . . cards, brackets and balls can be easily and securely attached with standard assembly tools. For holding components and miniature tube sockets the Alden Terminal Card Mounting System on the Alden Base gives ease of layout and wiring assembly. Open units for heat dissipation or shielded units for protection against dust or rough handling both lend themselves to mounting on the Alden Base with the same facility.

11 PIN NON-INTERCHANGEABLE BASES & SOCKETS

Smaller than the "20" but with the same features, the Alden "11" base and sockets are rugged for long life and Non Interchangeable to isolate critical voltages or signals and prevent burned out units. The retention force of pins and socket clips can be varied from light to heavy. Locating rings and alignment indicator quickly center base and socket for insertion. These and other features make it practical to incorporate plug-in construction in your design.

7 AND 9 PIN MINIATURE BASES & SOCKETS

Miniature and sub-miniature circuits, potted circuits, and miniaturized components easily become compact, sturdy plug-in units with the Alden 7 and 9 pin miniature plug-in bases and sockets. A wide selection of housings and mounting components are available for use with these bases.

Of particular importance is the Alden Terminal card Mounting System. Miniature circuits can be assembled on the card and the assembly can be mounted on the base to form a complete miniature unit.

Write for new booklet on "Components for Plug-in Unit Construction."



ALDEN PRODUCTS COMPANY

117 NORTH MAIN STREET, BROCKTON 64E, MASSACHUSETTS

ing the antenna type for specific areas in relation to channels operating and signal strength.

Quantitative Measuring Instrument. Allen B. Du Mont Laboratories Inc., 1000 Main Ave., Clifton, N. J. Form 10014-WP is an 8-page bulletin treating of the type 303 quantitative 10-mc c-r oscillograph, an instrument which incorporates circuits for the accurate calibration of time as well as amplitude. Specifications, chief features, and circuits (amplifiers, sweep and sync, and calibrator) are included.

F-M Communications Monitor. Hewlett-Packard Co., 395 Page Mill Road, Palo Alto, Calif. Volume 1, No. 12 of the Journal deals with the model 337 monitor for f-m communications services. The instrument described directly measures and continuously indicates both the carrier frequency and modulation deviation of an f-m transmitter operating in the range from 30 to 175 mc. Circuits and technical specifications are included.

Instrumentation Data. Minneapolis-Honeywell Regulator Co., Brown Instruments Division, Wayne and Windrim Aves., Philadelphia 44, Pa. Instrumentation data sheet No. 9.1-3 describes in a 4-page folder methods for accurate and rapid measurement of useful power with a check on reactive power to prevent overloading of generators. The system under discussion provides a continuous record of the power output of individual generators, the station and the system total.

Automatic Sample Counter. Special Instruments Laboratory, Inc., 1003 Highland Ave., Knoxville, Tenn. A single-sheet bulletin discusses the model 101 Auto Analyzer, designed to solve the problems encountered in accumulating large quantities of data from radioactive samples. The radioisotope analytical instrument described costs \$2,725.

Magnetic Tape Recording. Amplifier Corp. of America, Twin-Trax Division, 398 Broadway, New York

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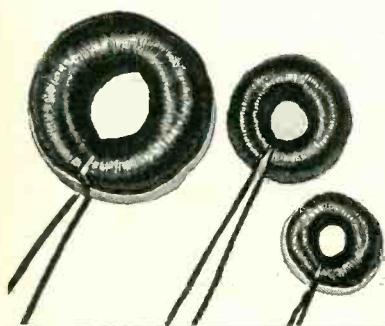


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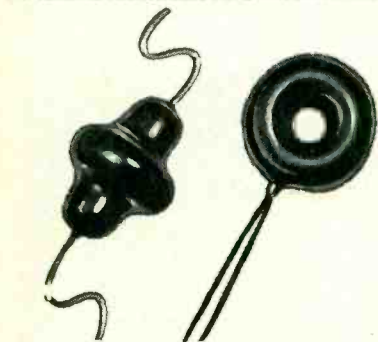
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(continued)

13, N. Y. A recent 128-page booklet and its 16-page supplement cover the elements of single and dual-track magnetic tape recording, as well as its applications. Among the 21 chapters are discussions of the recording process, playback process, erase process, unique magnetic tape phenomena and the inherent advantages of magnetic recording. Price of the profusely illustrated booklet is one dollar.

Controls and Resistors. Clarostat Mfg. Co., Inc., Dover, N. H. Catalog No. 50 offers a choice of resistors, controls and resistance devices. Cataloged resistors include cement-coated power resistors, flexible glass-insulated resistors, plug-in ballasts and voltage dividers, and automatic line-voltage regulators. Other items are tv beam benders, constant-impedance output attenuators, L-pads, T-pads and the handy power resistor decade box.

Hum Eliminator. Kalbfell Laboratories, Inc., 1076 Morena Blvd., San Diego 10, Calif. A recent mailing piece covers the model 503A bridged-T filter that is specially designed for use at the input terminals of a vtvm or c-r oscilloscope. The filter described attenuates hum at least 50 db. Special features, applications and prices are given.

Rosin Core Solder. Anchor Metal Co., 87 Walker St., New York 13, N. Y., has issued a bulletin on Shurflo rosin core solder, a new development in cored solders bringing together a superior rosin flux with virgin metals making a combination that is particularly adapted to all solder connections where corrosion is an important factor. Chief advantages and properties of solders are shown in the single-sheet bulletin.

Pocket Reference Book. Radio Corp. of America, Harrison, N. J., has completed the 1951 edition of its pocket reference book giving basic data on tubes, electronic components, test equipment, batteries and miniature lamps. A special feature in the new edition



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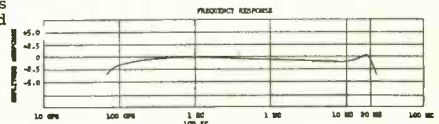
- Flat frequency response from 100 cps to 20 mc \pm 1.5 db.
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- Frequency compensated high impedance attenuator calibrated in 10 db steps from 0-50.
- Fine attenuator covers a 10 db range.
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This unit is designed for use as an oscilloscope deflection amplifier for the measurement and viewing of pulses of extremely short duration and rise time, and contains the Video Amplifier Unit, Power Unit and a low Capacity Probe.

Specifications

Input Impedance: Probe—12 mmf + 470,000 ohms; Jack—30mmf + 470,000 ohms; Output Impedance 18mmf + 470,000 ohms, each side push pull; Max. Input Volts: 500 peak to peak with probe; Max. Output Volts: 120 volts peak to peak (push pull); Power: 115 volts 50/60 cps AC Line; Size 19/4"x22"x14 3/4".



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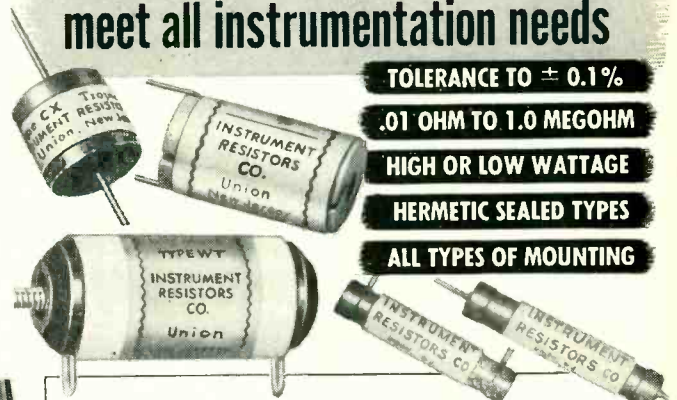


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is an authoritative article on tv trouble-shooting. Additional television information includes charts on tv channels and carrier frequencies, tv signal data, tv receiver alignment, test-pattern analysis and air-path distance of reflected signals. The section on electron tubes has also been completely revised.

C-R Oscillograph. Allen B. Du Mont Laboratories, Inc., 1000 Main Ave., Clifton, N. J., has available a two-page advertising reprint giving technical information on its type 303 quantitative 10-mc c-r oscillograph. The leaflet illustrates the instrument itself and includes a frequency response chart, an oscillogram, complete description of the unit and an outline of its chief advantages.

Modulated Light Relay. Electronic Control Corp., 1573 E. Forest Ave., Detroit 7, Mich., has devoted a 4-page folder to the modulated light relay, a photoelectric relay which is not affected by other sources of light; is not affected by smoke, fog, dust, or line-voltage variations; will operate over long distance, through furnaces or ovens, and on invisible light. An illustrated description, specifications, mechanical dimensions and ordering information are given.

Aircraft Circuit Breakers. Heine-mann Electric Co., Trenton 2, N. J. The 8-page, 2-color bulletin No. 3300 describes fully magnetic, nonthermal aircraft circuit breakers, which will operate in a range of from -65 to 185 F, vibration proof for 10 G. The Aero-Magnette breakers discussed have definite instantaneous trip point independent of time-delay characteristics and are not affected by ambient temperature. Also included are ratings, time overload curves for a-c and d-c, suggested uses and diagrams giving specifications of available mountings, covers and handles.

Selenium Rectifier. Clark Electronic Laboratories, Palm Springs, Calif. A recent 4-page folder covers a selenium rectifier with ratings available from 5 to 500 kw at any voltage from 6 to 600 or

Specify **BREEZE "Monobloc"**
Waterproof and Pressure Sealed
CONNECTORS



The only APPROVED Monobloc System for Advanced Radar, Communications, and Electronic Equipment

Breeze "Monoblocs", with single piece plastic inserts offer outstanding advantages in assembly, wiring, mounting and service in the field.

- Removable contact pins
- Single hole panel mounting
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Breeze "Monobloc" Waterproof and Pressure Sealed Connectors available in aluminum, brass, steel . . . all sizes and capacities . . . fully tested and approved.

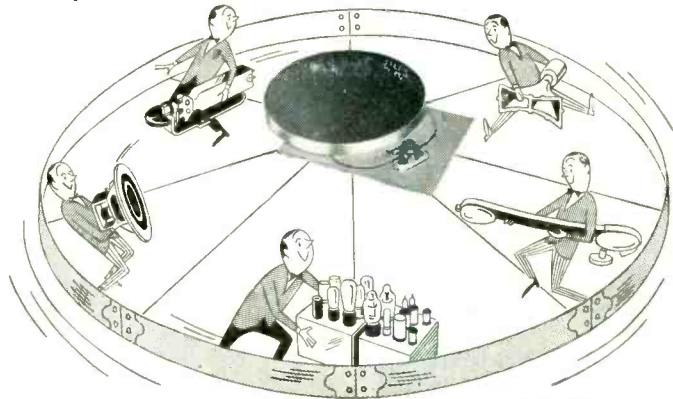
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If you have a tough connector problem ask BREEZE for the answer.

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PANORAMIC RADIO PROD.
PICKERING & COMPANY
RCA-VICTOR DIVISION
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SAT. REVIEW OF LIT.
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This line-up of famous names in the Sound Reproduction Industry is, indeed, an outstanding tribute to the quality of REK-O-KUT Turntables. Since the turntable is the "heart" of the reproduction you, too, should insist on the best — insist on REK-O-KUT.

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**PHOTOELECTRIC
TOWER LIGHTING
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Turn-on 35 ft.-candles—off at 55 ft.-candles—independent of time of day or weather conditions.
Low first cost—negligible maintenance.
3000 watts contact capacity.
Over 20,000 in use for tower and street lighting.
Complete details available — ask for Bulletin 63305.

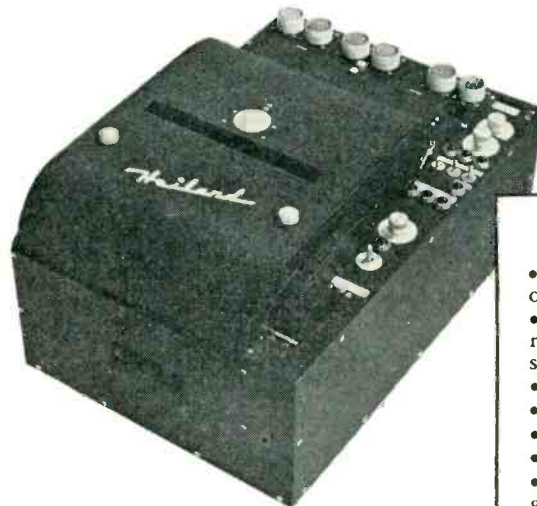
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from operating surface

dependable instruments



Type A-708...24-channel



FEATURES

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Sizes designed for normal requirements.
 Rigid construction — Round corners.
 Tight fitting inside covers for easy sealing.
 Cases or covers available separately.
 Mass Production means high quality at low competitive prices.
 Lojack covers and cases can be furnished with holes pierced, reinforcing brackets, channels or strips, tapped holes, studs, weld nuts, tapped inserts, etc., to better meet your specifications.
 Height of case variable.

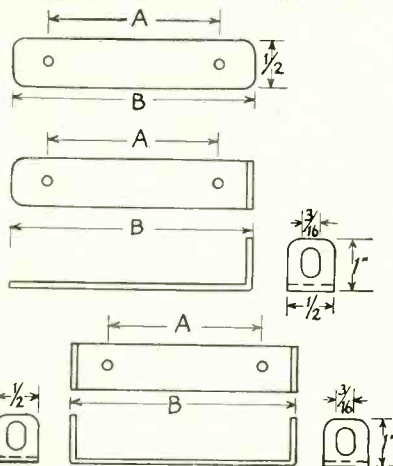
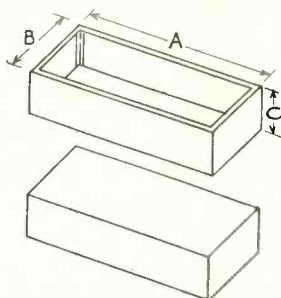
Core	Length	Width	Height
EE26-27	1-1/4"	1-1/2"	2"
EI-21	1-1/2"	1-3/4"	2-5/16"
EI-625	1-3/4"	2-1/8"	2-9/16"
EI-75	2-1/8"	2-7/16"	2-15/16"
EI-11	2-7/16"	2-15/16"	3-3/8"
EI-3A	2-15/16"	3-1/8"	3-11/16"
EI-12	2-7/8"	3-3/16"	3-3/4"
EI-112	3-3/16"	3-1/2"	4-1/4"
EI-195	3-1/2"	3-7/8"	4-5/8"
EI-137	3-7/8"	4-1/4"	5-1/16"
EI-13	4-1/4"	4-3/4"	5-1/2"
EI-36	4-3/4"	5-1/4"	6-3/4"
EI-175	4-7/8"	5-1/2"	6-5/16"
EI-19	5-1/4"	6-1/4"	8-1/16"

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ALUMINUM OR STEEL UNFINISHED

	B	A	C	Mat Thickness
LJ-151	5	7	2	.037
LJ-251	7	9	2	.037
LJ-351	7	12	3	.050
LT-451	11	17	3	.064
LJ-551	13	17	3	.064

Cover Plates for All Sizes
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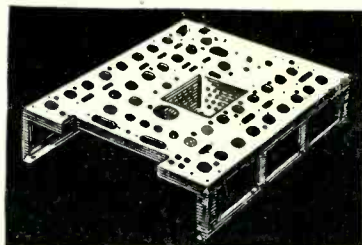
A — 2" to 3 3/4"
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Our model shop offers:—

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NEW PRODUCTS

(continued)

higher. The units described come complete in a steel cubicle containing rectifying plates, a dry-type transformer with class-B fireproof insulation, and control apparatus to fulfill the specifications desired.

Infrared Pyrometer. Hanson-Gorrill-Brian, Inc., One Continental Hill, Glen Cove, N. Y., has issued a single-sheet bulletin describing and illustrating its infrared pyrometer which measures temperatures of surfaces where physical contact methods and optical pyrometers are not usable. Accuracies of temperature measurements of the unit treated are within ± 5 F. Chief advantages and prices are given.

Subminiature Tubes. Sylvania Electric Products, Inc., Emporium, Pa., has published data providing average characteristics of 30 commercially available subminiature electron tubes ranging from 0.200 in. to 0.383 in. diameter. Also provided in the characteristic chart are useful suggestions for mounting, shielding and application to obtain maximum life for tube types including those rated up to 5,000 hours. Two tables are also included for easy cross reference between experimental and RTMA type numbers and classification of types with respect to applications.

Logarithmic Attenuator. Kalbfell Laboratories, Inc., 1076 Morena Blvd., San Diego 10, Calif., has available a mailing piece dealing with the model 511B Logaten, a logarithmic attenuator with a dynamic range of 50 db. The unit described controls an ambient temperature range of 32 to 100 F. Technical data, chief uses and a price list are included.

Power and Control Cable. The Rome Cable Corp., Rome, N. Y., recently published a 60-page power and control cable catalog designed as a handy guide for easy selection and specification. It gives complete technical data, descriptions and recommended uses for the company's complete line. Considerable space is devoted to the subject of insulations and their applications and to approved shielding practices.

FOR THE "GOLDEN EAR" CROWD

THE STRAIN-SENSITIVE PHONOGRAPH PICKUP

Here's why this truly faithful reproducer appeals to people gifted with the "Golden Ear" . . . why the STRAIN-SENSITIVE PICKUP developed by the PFANSTIEHL CHEMICAL COMPANY brings out the brilliance of great voices and orchestras . . . the latent music on your records that other pickups leave untouched.

- The STRAIN-SENSITIVE PICKUP is an amplitude transducer with a CONSTANT RESISTANCE of about 250,000 ohms.
- Signal output is at a practically CONSTANT IMPEDANCE level.
- Excellent transient response.
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- LINEAR RESPONSE free from peaks or resonances.

Cartridges are available for both standard and micro-groove, and can be had with Famous PFANSTIEHL M47B Precious Metal Alloy or diamond tipped styl.

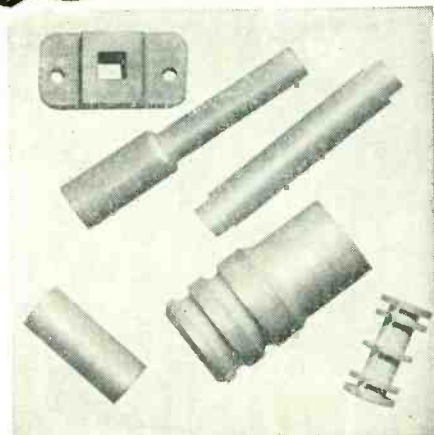
A special preamplifier is necessary to provide the correct D.C. voltage for the pickup element and to provide the first stages of signal gain. Four styles are ready, or, if you prefer, you can build your own from the circuit in the literature.

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Design engineers and manufacturers in the radio, electrical and electronic fields are finding in LAVITE the precise qualities called for in their specifications . . . high compressive and dielectric strength, low moisture absorption and resistance to rot, fumes, acids, and high heat. The exceedingly low loss-factor of LAVITE plus its excellent workability makes it ideal for all high frequency applications.

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for HIGH MEGOHM RESISTORS

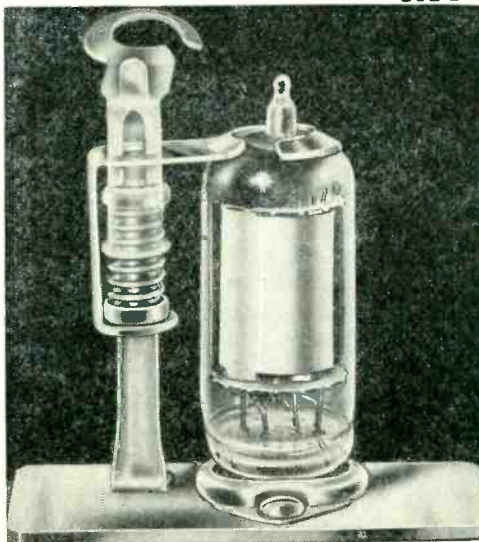
RPC Type H Resistors are furnished with resistance values as high as 50 million megohms (5×10^{13} ohms). Their advanced design insures highest stability with extremely low noise level, polarization effects, and voltage and temperature coefficients. Available in sizes suitable for any circuit requirement. Standard resistance tolerance $\pm 10\%$.

RPC Type H Resistors are rugged, durable units jacketed in polyethylene to provide maximum protection against mechanical damage and humidity. These resistors are eminently suited for electrometer circuits, radiation equipment, photo cell circuits and as high resistance standards. Moderately priced. Write for catalog today.

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New BIRTCHER TUBE CLAMP FOR MINIATURE TUBES



POSITIVE PROTECTION AGAINST LATERAL AND VERTICAL SHOCK!

The New Birtcher Type 2 Tube Clamp holds miniature tubes in their sockets under the most demanding conditions of vibration, impact and climate. Made of stainless steel and weighing less than 1/2 ounce, this New clamp for miniature tubes is easy to apply, sure in effect. The base is keyed to the chassis by a single machine screw or rivet . . . saving time in assembly and preventing rotation. There are no separate parts to drop or lose during assembly or during use. Birtcher Tube Clamp Type 2 is all one piece and requires no welding, brazing or soldering at any point.

If you use miniature tubes, protect them against lateral and vertical shock with the Birtcher Tube Clamp (Type 2). Write for sample and literature.

Builder of millions of stainless steel Locking Type Tube Clamps for hundreds of electronic manufacturers.

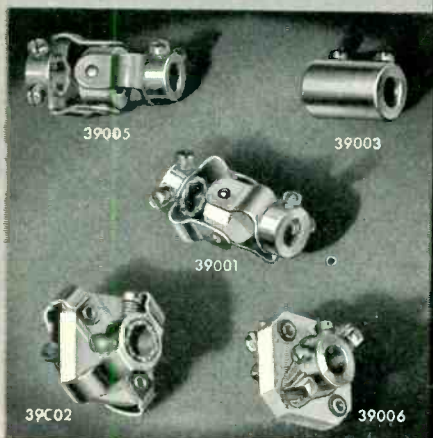
The **BIRTCHER** Corporation

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Designed for



Application



FLEXIBLE COUPLINGS

The No. 39000 series of Millen, "Designed for Application" flexible coupling units include, in addition to improved versions of the conventional types, also such exclusive original designs as the No. 39001 insulated universal joint and the No. 39006 "slide-action" coupling (in both steatite and bakelite insulation).

The No. 39006 "slide action" coupling permits longitudinal shaft motion, eccentric shaft motion and out-of-line operation, as well as angular drive without backlash.

The No. 39005 is similar to the No. 39001, but is not insulated and is designed for applications where relatively high torque is required. The steatite insulated No. 39001 has a special anti-backlash ball and socket grip feature, which, however, limits its serviceable operation to torques of six inch-pounds, or less. All of the above illustrated units are for 1/4" shaft and are standard production type units.

**JAMES MILLEN
MFG. CO., INC.**

MAIN OFFICE AND FACTORY
**MALDEN
MASSACHUSETTS**



NEWS OF THE INDUSTRY

(continued from page 134)

as instructors, technical writers, and professional engineers in the field of communications and electronics.

Although veterans are accorded preference, there are a sufficient number of openings to provide for the appointment of nonveterans who can qualify. Salaries range from \$3,825 to \$6,400 a year. Applicants for electronic engineering positions should have at least one year of professional experience in addition to an appropriate bachelor's degree or a master's degree for the salary of \$3,825 a year. Additional experience may be qualifying for higher salaries up to \$6,400.

Persons with 4 years or more of practical experience in the construction, maintenance or repair of radio or radar are especially needed for instructor positions. Men with teaching experience in addition to their technical background in these fields may be employed at salaries ranging from \$3,825 to \$4,600 a year. Openings are in microwave radio relay, radar, radio electronics, fixed station radio, central office techniques, teletype installation and maintenance, repeater and carrier, and dial central office techniques.

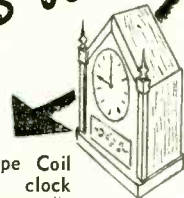
Technical writers with 3½ to 5½ years of experience in preparing reports, manuscripts or manuals dealing with electronics, radio, radar or communications may qualify for positions at salaries of \$3,825 to \$5,400 a year.

Applicants should complete Standard Form 57, which is available at any first or second class post office, and submit it to the Civilian Personnel Branch, Building T-530, Ft. Monmouth, N.J. For applicants who can report in person, interviews will be held between 8:00 a.m. and 3:00 p.m., Tuesday through Friday.

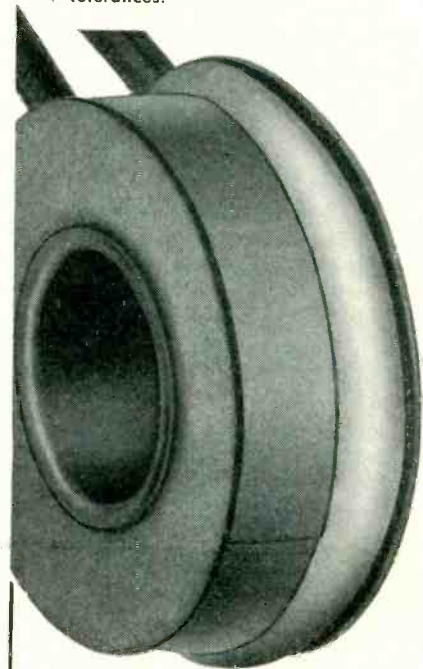
IRE Elects Officers for 1951

ELECTION of Ivan S. Coggeshall, general traffic manager of Western Union Telegraph Company's overseas communications, as president of the Institute of Radio Engineers for 1951 was recently announced by the board of directors in New

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SPECIFIC COILS
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This Bobbin Type Coil is supplied to clock makers: Some use 37#, others may specify 38# or 40# wire; Deep wax or lacquer impregnation; enamel, formex, or nylon wire insulations. At Coto, it is usual to work to close tolerances.



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When you need electrical coils, why not take advantage of 34 years of experience, engineering competence, and modern production facilities. Coto coils are built for you, to your specifications.

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January, 1951 — ELECTRONICS

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Made by a new process to a uniform, high quality for continuous, heavy-duty service.

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SPLENDID ISOLATION



SIGNAL GENERATOR TF867

stabilised output control. Output is variable from 4V to 0.4μV and calibration indicates the true artificial signal e.m.f. irrespective of load.

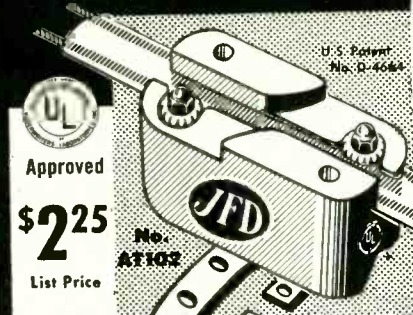
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THE WORLD'S LEADING TWIN LEAD TELEVISION LIGHTNING ARRESTER



Approved

\$225

List Price

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SAFE TV GUARD

Protects television sets against lightning and static charges. Simple to install everywhere and anywhere... no stripping, cutting or spreading of wires. More than 500,000 in use today!

See your jobber or write to —

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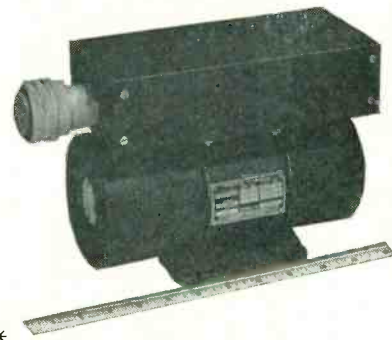
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FIRST In Television Antennas and Accessories

400-800 CYCLE AC

From 5.5v to 230v
DC Input

New **Carter*** High Frequency

- **LIGHT WEIGHT**
Filter Model Shown
Weight only 22 lbs.
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10" x 4 1/2" x 7 3/4"
(Filter Model as shown)
- **PRECISION BUILT**
Shaft and bore fits
held to less than
.0002"
- **ARMATURE**
Triple and quad-
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windings static-
ally and dynamic-
ally balanced
- **BALL BEARINGS**
Require no mainte-
nance or lubrication
in normal service
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INDUCTOR ALTERNATOR

Newly developed in the Carter research and engineering departments, this new rotary power supply is ideal for aircraft, geophysical, government and laboratory research, and other applications demanding a small, mobile source of up to 100 watts high frequency AC. Primarily designed for 24 - 29v. DC airborne equipment, but available at any input voltage 5.5v to 230v. Inductor principle eliminates slip rings and brushes. Electrically isolated input and output units. Separate DC plate output also available in addition to the h.f. AC.



WRITE for Bulletin #350. Contains complete illustrated information on the New Carter Inductor Alternator, mechanical and electrical specifications, performance chart, etc. Yours FREE for asking!

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NO MAGIC just use **ATR**
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STANDARD AND HEAVY DUTY INVERTERS



For Inverting D. C. to A. C.

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I. S. Coggeshall

York. The new president has been active in the adoption of electronic methods and devices in the telegraph and submarine cable field. He will succeed Raymond F. Guy, manager of radio and allocation engineering of the National Broadcasting Company.

Jorgen C. F. Rybner of Copenhagen, professor of telecommunications at the Royal Technical University of Denmark and noted author of Danish and English textbooks on network theory, was elected vice-president. He will succeed Sir Robert Watson-Watt of London, an authority on military radar.

Directors elected by the Institute for 1951 are: William H. Doherty, director of electronic and television research for Bell Laboratories, Murray Hill, N. J.; George R. Town, associate director of the engineering experiment station at Iowa State College, Ames, Iowa; Harry F. Dart, office manager of the electronics engineering department of Westinghouse Electric Corp., Bloomfield, N. J.; Paul L. Hoover, head of the department of electrical engineering, Case Institute of Technology, Cleveland, Ohio; William M. Rust, Jr., head of geophysics research for Humble Oil and Refining Co., Houston, Texas; and Allan B. Oxley, chief engineer of RCA Victor Co., Montreal, Quebec.

In addition, the following directors will continue to serve on the Board during 1951: S. L. Bailey, R. F. Guy, W. L. Everitt, D. G. Fink, W. R. Hewlett, J. W. McRae,

2 KW VACUUM TUBE BOMBARDER OR INDUCTION HEATING UNIT



For Only \$650.

Never before a value like this new 2-KW bench model "Bombarder" or high frequency induction heater . . . for saving time and money in surface hardening, brazing, soldering, annealing and many other heat treating operations.

Simple . . . Easy to Operate . . . Economical Standardization of Unit Makes This New Low Price possible.

This compact induction heater saves space, yet performs with high efficiency. Operates from 220-volt line. Complete with foot switch and one heating coil made to customer's requirements. Send samples of work wanted. We will advise time cycle required for your particular job. Cost, complete, only \$650. Immediate delivery from stock.

Scientific Electric Electronic Heaters are made in the following range of Power: 1-2-3½-5-7½-10-12½-15-18-25-40-60-80-100-250KW.

Scientific Electric

Division of

"S" CORRUGATED QUENCHED GAP CO.

107 Monroe St., Garfield, N. J.

High Sensitivity . . . Logarithmic AC VOLTMETER

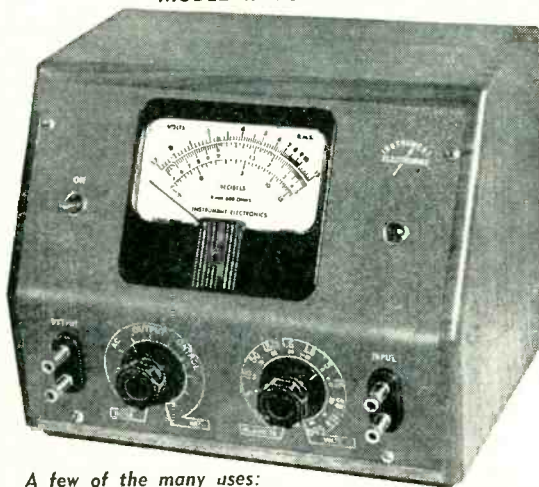
50 MICROVOLTS TO 500 VOLTS

MODEL 47 VOLTMETER

**SELF-CONTAINED
ALL AC OPERATED UNIT**
An extremely sensitive amplifier type instrument that serves simultaneously as a voltmeter and high gain amplifier.

- Accuracy $\pm 2\%$ from 15 cycles to 30 kc.
- Input impedance 1 megohm plus 15 uuf. shunt capacity.
- Amplifier Gain 25000

Also MODEL 45
WIDE BAND
VOLTMETER
.0005 to 500 Volts!
5 Cycles 1600 kc.



A few of the many uses:

- Output indicator for microphones of all types.
- Low level phonograph pickups.
- Acceleration and other vibration measuring pickups.
- Sound level measurements.
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Write for Complete Information

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LITTLE NECK, L. I., N. Y.



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SEE OUR
CATALOG IN
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FALSTROM service is fast, competent, complete. It includes forming, punching, welding and finishing. Piping, wiring and accessories can be built in when desired. Falstrom engineers will even procure and install your instruments to your specifications. All work performed by Falstrom is done by engineers and technicians thoroughly familiar with each phase of production. Mechanics skilled in working with steel, aluminum and stainless steels assure finest workmanship. Falstrom installations are in service throughout the electrical, chemical and petroleum industries — have been an accepted standard of excellence since 1870. For a practical, economical solution to your metal forming problems, go to Falstrom!

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"Hard-to-Get" Components



Custom Components

Metal-plastic components designed and manufactured to order. Write for quotations specifying electrical and mechanical characteristics. Describe application. No obligation.

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Multi-contact connectors and mating chassis counterparts. Melamine or alkyd insulation; steel or brass nickel-plated shells. Banana springs are heat treated beryllium copper. Unexcelled low resistance contact. Highest quality... good for thousands of connects and disconnects.

Special Connectors to Order—Miniatures; water tight and pressure proof types to JAN specifications.

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Since 1918 PIONEERS IN ELECTRONICS AND PLASTICS

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From 10 Microseconds to 3 Seconds

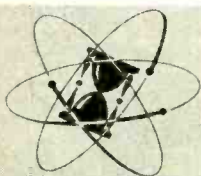
The time interval between any two components in electrical, mechanical or electro-mechanical systems can now be measured, simply and accurately, with American Chronoscope Equipment.

The Model 211 Input Adapter used in conjunction with the Model 110 American Chronoscope separates the functions of STARTING and STOPPING the measurement of time. Simply connect the Start and Stop leads from the adapter to any two components of a system under test. Only the first complete elapsed time interval presented is accepted. This reading is indicated on the Chronoscope and remains fixed until reset.

PRICES

Model 110 Chronoscope . . . \$475
Model 211 Input Adapter . . . \$265

For complete description on these and other Chronoscopes and Adapters, write for Bulletin 200A



American Chronoscope

C O R P O R A T I O N
M O U N T V E R N O N , N . Y .

316 WEST FIRST ST.

H. J. Reich, F. Hamburger, Jr., J. D. Reid, and A. V. Eastman.

Taxicab Radio Advances

INITIAL use of commercial radio communications equipment in the 450 to 460-mc band for the general mobile radio services was recently announced by Link Radio Corp., New York, N.Y. A pioneer move by two major taxicab companies in the uhf range was made officially in a request by the Yellow Cab Co. and the Cab Sales and Parts Corp., both of Chicago, Ill., to the FCC for what will eventually call for the installation of 3,666 mobile units and 16 base stations.



Under the mobile radio service rules established by the FCC in May 1949, the taxicab service was allocated 10 frequencies in the 450 to 460-mc band for developmental purposes, ranging from 452.05 to 452.95 mc. Commercial application was made permissible by the FCC in its directive of May 1949. The radio services which may use the 450 to 460-mc band are remote pickup broadcast; land transportation, which includes railroads, taxicabs and urban transit; public safety, which includes police, fire, forestry-conservation, highway maintenance and special emergency; industrial, which includes power radio, petroleum, forest products, motion picture, relay press and special industrial; and domestic public.

The system applied for in the construction permit request will use eight multiple main-station transmitters to cover the city in checkerboard fashion so that the traffic-handling capability of the radio circuits may be multiplied to enable dispatchers to control, via two-way radio, a large number of taxicabs in the Chicago area.

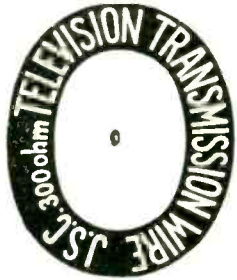
Each main station transmitter will have an output of 100 watts and each mobile transmitter will have an output of 10 watts.

Radio Engineers Announce Awards

ROBERT B. DOME, electrical consultant for General Electric Co., Syra-

**MORE THAN
50,000 TV SETS
MONTHLY**
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TV manufacturer, installation engineer, TV sponsor and televiewer all form an inseparable chain, securely linked by the world's finest television transmission wire. J S C is justly proud of its important role in the development and progress of television. Rigid adherence to the principle of "quality before quantity" will pave the way to greater accomplishments for J S C!

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SQUARE, ROUND
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 1/2" to 30" LONG
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 TOLERANCES to .002"

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*Protect Coil Accuracy and Stability
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Years of specialized "know-how" easily enable PARAMOUNT to provide exactly the shape and size tubes you need for coil forms and other uses. *Hi-Dielectric. Hi-Strength.* Kraft, Fish Paper, Red Rope or any combination wound on automatic machines. Wide range of stock arbors. Special tubes made to your specifications or engineered for you.

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Stop wrestling with big irons. New HI-HEAT TIPS in your Ungar Electric Soldering Pencil produce a really versatile tool that'll perform on a par with the big, bulky 100-150 watt irons. If you can't get immediate delivery, please be patient, for production hasn't yet caught up with demand. Ask your supplier for No. 1236 Pyramid or No. 1239 Chisel. List price, \$1.25 each.

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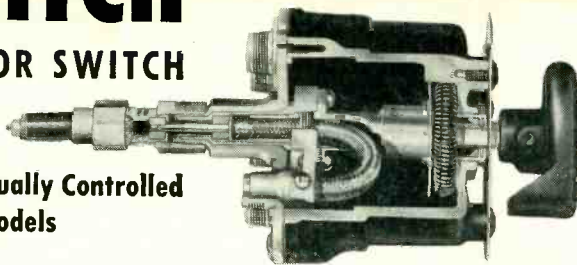
COAXSWITCH

COAXIAL SELECTOR SWITCH

50 Ohms—

Type N Connectors—Manually Controlled
Low VSWR—4 Models

CUT-A-WAY VIEW, MODEL 74



The COAXSWITCH is an RF switch for use in coaxial circuits where it is important that the 50 OHM impedance of the cables be maintained. In a circuit sense, this switch consists of two pairs of "N" connectors spaced 4½" apart using RG-8/U as the connecting link. The COAXSWITCH itself introduces no VSWR other than that of connectors. Characteristic impedance is maintained thru all switch details. Cut-

away view shows that shield as well as center conductor is switched. Beryllium copper contacts, on the gooseneck, mate directly with male "N" (Type UG-21B/U) connectors, which connect directly to back plate of switch. Since all connectors come out in line with axis of switch, right angle connectors are usually unnecessary.

Literature Gladly Sent

<p>MODEL 74 SINGLE COAXIAL CIRCUIT SIX POSITIONS (SELECTOR OR TAP SWITCH)</p>	<p>MODEL 718 SINGLE COAXIAL CIRCUIT EIGHT POSITIONS (SELECTOR OR TAP SWITCH)</p>	<p>MODEL 72-2 TWO COAXIAL CIRCUITS TWO POSITIONS (OPDT, etc.)</p>	<p>MODEL 72R TWO COAXIAL CIRCUITS REVERSING SWITCH (OPDT, etc.)</p>
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BIRD ELECTRONIC CORP.
Instrumentation for Coaxial Transmission
1800 East 38th Street • Cleveland 14, Ohio
West Coast Representative • NEELY ENTERPRISES • Hollywood 46, Calif.

cuse, N. Y., will be awarded the Morris Liebmann Memorial Prize for 1951 by the IRE for his contributions to the intercarrier sound system of television reception, wide-band phase-shift networks, and various simplifying innovations in f-m receiver circuits. The award will be presented at the Institute's annual banquet on March 21, 1951, at the Waldorf-Astoria Hotel in New York City.

Other 1951 awards which will be presented at that time are as follows:

Alan B. MacNee, assistant professor of electrical engineering at the University of Michigan, Ann Arbor, Mich., will receive the Browder J. Thompson Prize for his paper "An Electronic Differential Analyzer," which appeared in the November, 1949 issue of the *Proceedings of the IRE*. The award is given annually to the author under thirty years of age for that paper recently published by the Institute which constitutes the best combination of technical contribution to the field of radio and electronics and presentation of the subject.

The Harry Diamond Memorial Award, given only to persons in government service, will be bestowed on Marcel J. E. Golay, Signal Corps Engineering Laboratories, Fort Monmouth, N. J., for his contributions in the over-all Signal Corps research and development program, and particularly for his accomplishments leading toward a reduction in the infrared-radio gap.

Willis W. Harman, associate professor at the University of Florida, Gainesville, Fla., will receive the Editor's Award, established to stimulate the use of good English in technical writing, for his paper "Special Relativity and the Electron," which appeared in the November 1949 issue of the *Proceedings of the IRE*.

IRE-RTMA Fall Meeting

THE TWENTY-SECOND annual Fall Meeting of members of the IRE and the RTMA Engineering Department was held Oct. 30-Nov. 1 at the Hotel Syracuse in Syracuse, New York, with a total registration of over 600.

At the general session on Monday

INTERMODULATION METER Model 31



- Completely Self-Contained
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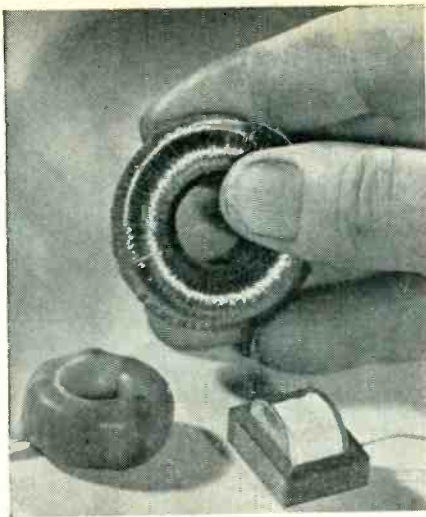
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HALF TRACK!

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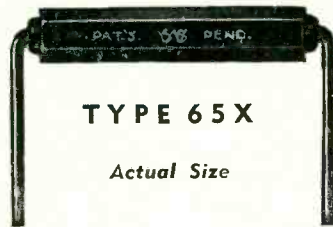
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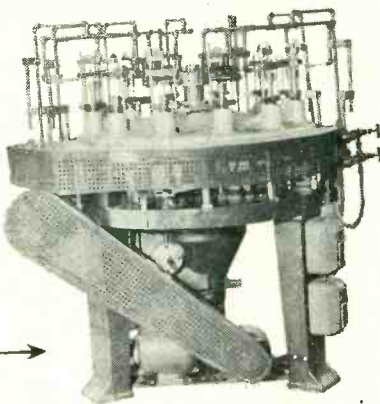
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DEPENDABLE
MODERATELY
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• **OUTPUT #1:** 200 to 325 VDC at 300 ma regulated

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PANEL SIZE
10 1/2" x 19"
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ISSUES YEARLY

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MID-JUNE

BUYERS' GUIDE

morning, papers presented included one on the use of the noise diode for determining amplifier sensitivity and another on wideband impedance matching between a resonant antenna and a line.

The Monday afternoon quality control session covered efficient use of data for quality control, the General Electric quality control indicator, the control of averages in radio tube manufacture, and the human aspect of engineering quality into a product.

At a joint session with the Technology Club of Syracuse on Monday evening, Dr. Allen B. Du Mont spoke on problems of the television industry, including the color tv controversy and the freeze on new tv station construction.

Both sessions on Tuesday were devoted to tv and much interest was shown in a paper titled, "An Analysis of Color Television," by A. V. Loughren of Hazeltine Electronics Corp. (Our cover last month showed four of the illustrations used in this presentation.) At the same session, two new tubes were described—the RCA low-noise double triode which is used as an r-f and i-f amplifier in tv receivers, and the GE miniature magnetron for use in the uhf tv band.

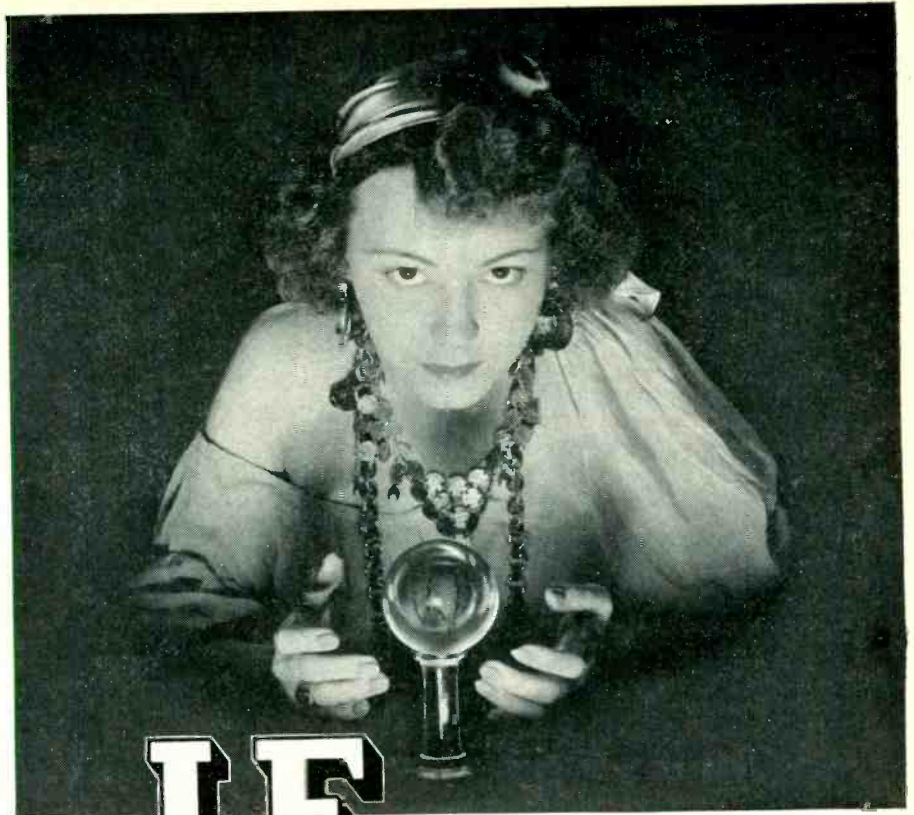
The RTMA award was presented posthumously to L. C. F. Horle at the Tuesday night banquet meeting. The late Mr. Horle was, until his recent retirement, RTMA's chief engineer.

The audio session on Wednesday morning consisted of papers on the mechanics of the phonograph pickup, a lightweight pickup and tone arm, sound pickup in high ambient noise, and the recently adopted RTMA standards for sound equipment.

It was announced that the Fall Meeting next year will be held in Toronto, Canada.

BUSINESS NEWS

ELECTRONIC CONTRACTORS INC., Philadelphia, Pa., is a new firm formed by John C. Merman and four other television service contractors for the purpose of entering into defense and private manu-



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If we could read the minds of engineers and scientists for a year ahead . . .

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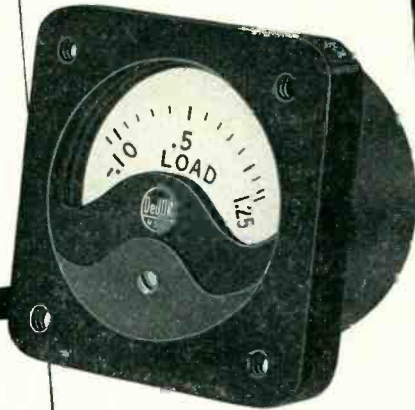
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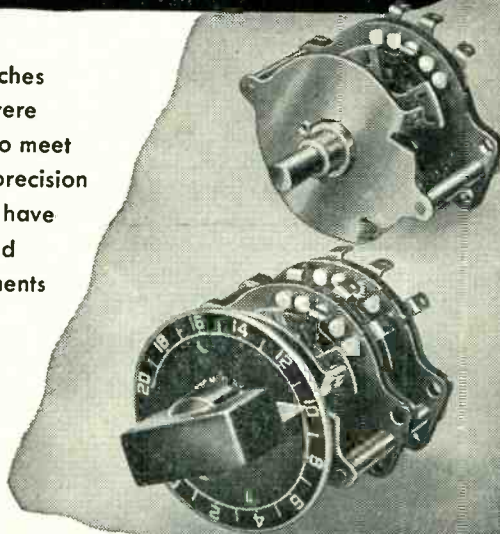
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HAVE A CONSTANT CONTACT RESISTANCE OF ONLY 1 or 2 MILLIOHMS!

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Write for Technical Bulletin No. 28.



TECH LABORATORIES

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facturing contracts that require electronics background and experience.

GENERAL ELECTRIC Co. will reopen a former radio tube plant in Utica, N. Y., and convert it for the manufacture of emergency radio communications equipment. The new plant is expected to be in full operation by June 1951, employing about 425 people.

ELECTRICAL REACTANCE CORP. recently dedicated its new 70,000-sq-ft plant in Olean, N. Y. The plant will be devoted to the manufacture of capacitors, resistors and choke coils.

RADIO RECEPTOR Co., INC., manufacturer of radio and electronic components and complete assemblies for industry and government, has purchased a 90,000-sq-ft factory in Brooklyn, N. Y., to house its expanding divisions.

SARKES TARZIAN, INC., has begun operation of its new 53,000-sq-ft plant in Batavia, Ill., to increase production of television picture tubes.

NATIONAL ELECTRONICS INC., Geneva, Ill., now has a new brick factory addition to its plant which increases total floor space by 80 percent and provides facilities for greater production of thyratrons, rectifiers and mercury pool tubes.

WESTERN ELECTRIC Co. has leased the Pomona Mills plant near Greensboro, N. C., to manufacture electronic equipment for the armed forces. Approximately 2,000 persons will be employed.

THE BARRY CORP., Cambridge, Mass., is erecting a new plant in Watertown, Mass., that will more than double its present floor space for production of shock mountings and vibration isolators.

NORTHWESTERN UNIVERSITY, Evanston, Ill., will build a 4½-million-volt electrostatic accelerator for nuclear research, to be used by staff members and graduate students doing research work, and in connection with special government projects. Cost of the project will be approxi-

The New STAYER MINI-SHIELD

TRADE MARK REG. AND PAT. PEND.

The shield
that fits all
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A flexible shield that snugly fits all miniature tubes because it compensates for all variations in tube dimensions. Mini-Shields are made for both T5 1/2 and T6 1/2 bulb tubes. Send for catalog sheet.



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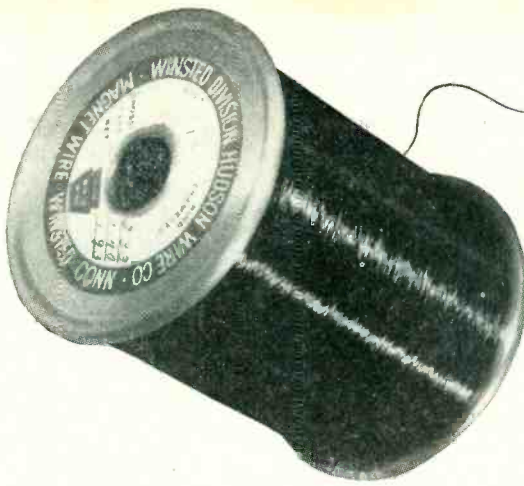


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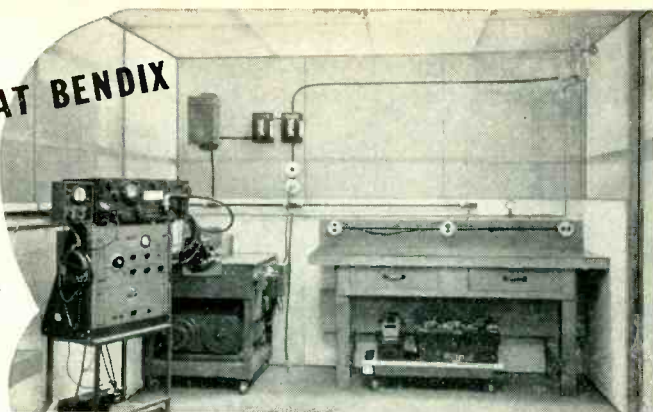
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ACE Screen Rooms provide attenuations of 100 db.—and higher—at frequencies as low as 0.15 and as high as 10,000 mc. Rooms are available for attenuations as high as 140 db. Ace shielding characteristics have been determined by reputable electronic laboratories. Write, wire or 'phone for descriptive bulletin.

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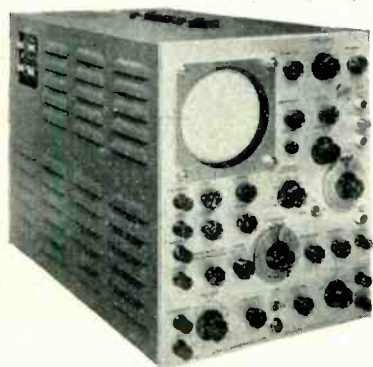
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REgent 9-1019



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Type 512 Oscilloscope

- **Band Pass—DC-2mc**
- **Sensitivity—5mv/cm maximum**
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Accurate observation and measurement of slowly recurring phenomena is difficult, if not impossible, by conventional oscilloscopic techniques. The Tektronix Type 512 Cathode Ray Oscilloscope, combining as it does direct-coupled amplifiers, slow sweeps and high accuracy, is recognized by a constantly increasing number of researchers as being an indispensable laboratory tool. New and fruitful approaches to the problems encountered in research are permitted by these features. \$950.00 f.o.b. Portland, Oregon.

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mately \$150,000 exclusive of the housing.

MINNEAPOLIS-HONEYWELL REGULATOR Co. recently launched a road show, called the Parade of Progress, which will cover more than 60 cities. Purpose of the traveling show is to demonstrate the latest electronic, electric and pneumatic control systems recently developed and now in production.

PEMCO CORP., Baltimore, Md., manufacturer of porcelain enamel finishes and ceramic chemicals, is expanding its plant by the addition of more than 30,000 sq ft of floor space to existing facilities.

AMERICAN ELECTRONEERING CORP., producers of aircraft instrument test equipment, power supply units and signal generators, have moved to new larger quarters at 5025 W. Jefferson Blvd., Los Angeles, Calif., to consolidate production facilities under one roof and make room for stepped up armed-service activities.

RADIO CRAFTSMEN, INC., Chicago, Ill., makers of custom-built tv and radio chassis and electronic equipment, have acquired 12,000 sq feet of space at 4401 North Ravenswood, Chicago, to be used in tv production.

PERSONNEL

VINCENT SALMON of Stanford Research Institute has been elected chairman of the San Francisco Section, Audio Engineering Society. Other officers are: Harold Lindsay of Ampex Electric Corp., vice-chairman; Frank Haylock, secretary; Myron J. Stolaroff of Ampex, treasurer; and Walter T. Selsted, Jack Hawkins and Ross Snyder, executive board members.

L. E. RECORD has been promoted from supervisor of the engineering development and testing laboratories to division engineer of the cathode-ray tube division of General Electric Co., Syracuse, N. Y.

JOHN T. WILNER, engineering director of stations WBAL and WBAL-TV, has been elected vice-president in charge of engineering

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LOCKHEED Aircraft Corporation
Burbank, California

ELECTRONICS — January, 1951

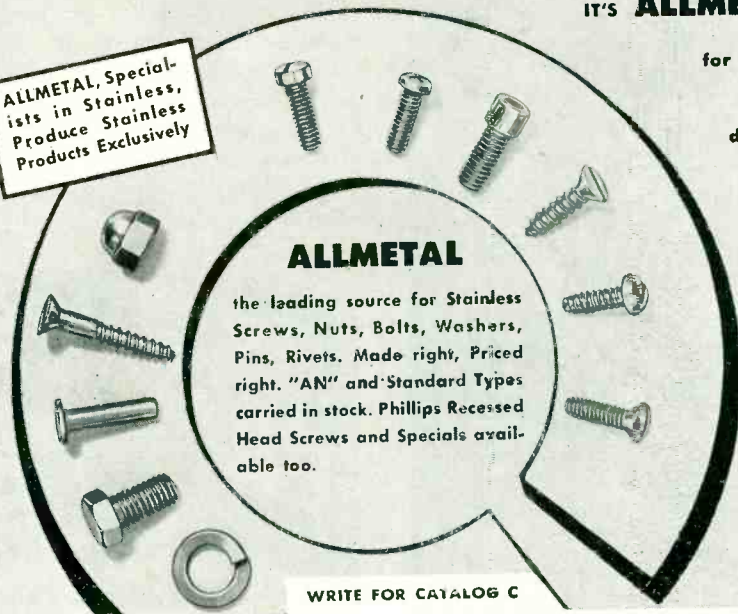
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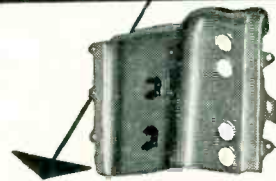
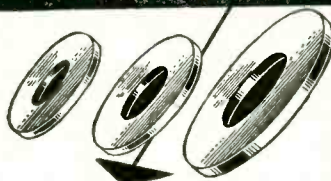
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of Hearst Radio, Inc., He was formerly engineer-in-charge of CBS television development.

CHARLES D. PERRINE, JR., formerly manager of the electronics department of Fairchild Engine and Airplane Corp.'s guided missiles division, has joined the electronics and guidance section in Consolidated Vultee's San Diego Division engineering department.



C. D. Perrine, Jr.

M. A. Acheson

M. A. ACHESON, formerly chief engineer of the radio tube division of Sylvania Electric Products Inc., Emporium, Pa., has been transferred to the staff of E. Finley Carter, vice-president in charge of engineering at Sylvania's New York office.

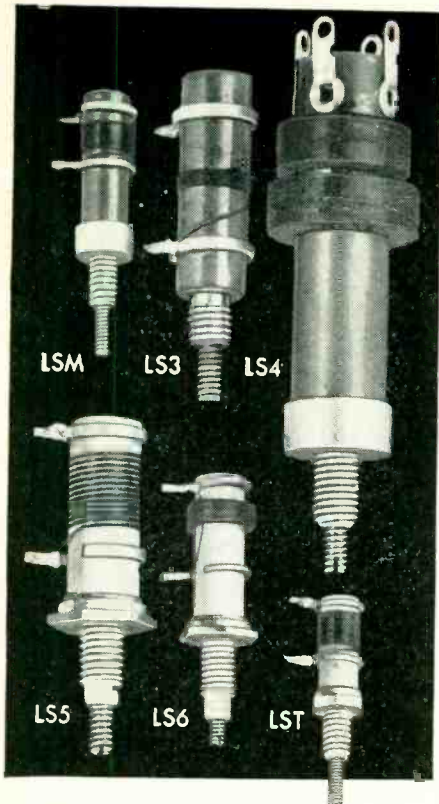
HARRY STOCKMAN, former consulting engineer to industrial firms in the Boston area, has been appointed director of research of the Tobe Deutschmann Corp., Norwood, Mass.

G. F. CALLAHAN, formerly division engineer of the cathode-ray tube division of General Electric Co., Syracuse, N. Y., has been appointed staff assistant to K. C. DeWalt, manager of the division.

LEIGH W. HAEFLE, with Air Reduction Co., New York, N. Y., since 1938, was recently appointed assistant chief engineer of the company's general engineering department.

DAVID S. RAU, formerly assistant to the vice-president in charge of engineering, is now assistant vice-president and chief engineer of RCA Communications, Inc.

JOHN F. BYRNE, formerly vice-president and chief engineer of Airborne Instruments Laboratory, Inc., Mineola, N. Y., has been ap-



Which Of These Coil Forms Best Fits YOUR Needs?

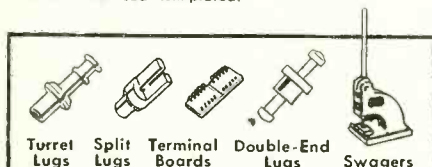
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LST	L-5 Ceramic	8-32	3/16"	1 9/32"
LS6	L-5 Ceramic	10-32*	1/4"	2 7/32"
LS5	L-5 Ceramic Paper	1/4-28*	3/8"	1 1/16"
LSM	Phenolic Paper	8-32	1/4"	2 7/32"
LS3	Phenolic Paper	1/4-28	3/8"	1 1/8"
LS4†	Phenolic	1/4-28	1/2"	2"

*These types only provided with spring locks for slugs.
†Fixed lugs. All others have adjustable ring terminals.
All ceramic forms are silicone impregnated. Mounting studs of all forms are cadmium plated.



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pointed associate director of research in the division of communications and electronics of Motorola, Inc., Chicago, Ill.

EDWIN LOCKWOOD, formerly senior research engineer for Electro-Mechanical Research, Inc., Ridgefield, Conn., has been appointed chief engineer of Price Electric Corp., Frederick, Maryland, manufacturers of electronic relays.



E. Lockwood

L. C. Smith

LESTER C. SMITH, formerly instructor in electrical communications at MIT, has been appointed chief engineer of Spencer-Kennedy Laboratories, Inc., Cambridge, Mass.

CHARLES N. KIMBALL, formerly technical director of Bendix Research Laboratories, Detroit, Mich., has been elected president of Midwest Research Institute, Kansas City, Mo.

CARL E. SCHOLZ, formerly vice-president and chief engineer in charge of Mackay Radio and Telegraph Company's engineering and plant department, was recently appointed vice-president and chief engineer of All America Cables and Radio, Inc., and The Commercial Cable Co.

ROBERT H. WEINMANN, formerly assistant vice-president of Geovision, Inc., New York City, and chief electronic engineer for the Rieber Research Laboratory of the same city, has been appointed chief engineer of Danco Instruments, Inc., Huntington Station, L. I., N. Y.

JAMES L. LAWSON, former head of the nuclear investigations division, has been named manager of the newly formed Electron Physics Divisions of the General Electric Research Laboratory, Schenectady, N. Y.

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ACTUAL SIZE



OF MAGNET

LIGHT WEIGHT
EAR PIECE

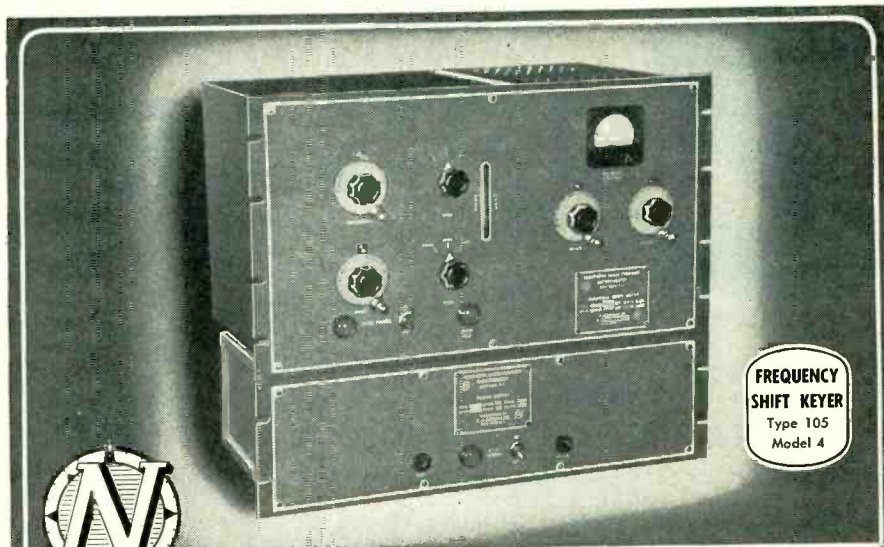
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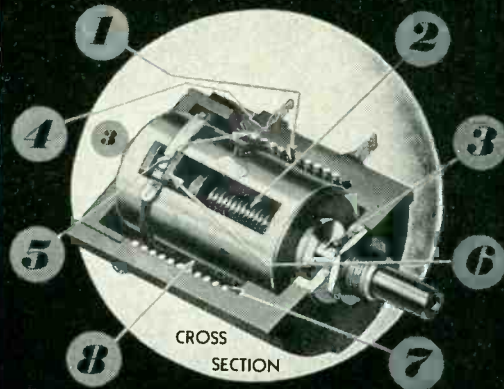
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in point, omits the best part of the story.

It is true, as you observe, that the Alpine tower was designed for the operation of a series of transmissions simultaneously arrayed between the arms. The attempt, however, to start such pioneering work at Alpine by Paul Godley with the installation of a second transmitter was promptly vetoed by the then engineering czar of the FCC, Mr. Andrew J. Ring.

Time passes. Mr. Ring leaves the Commission. He enters private practice. In due course, Mr. Ring advocates an arrangement among Washington f-m licensees and prospective licensees to locate all stations in two groups, the stations to be arranged as to frequencies and location to give maximum coverage and minimum interference to the people of Washington.

The world moves on. Now, twelve years after the disapproval of what was attempted at Alpine, the erection of at least a half dozen antennas atop the Empire State Building in New York City enters the realm of FCC standards of good engineering practice. The French have a word for it—"It is to laugh."

EDWIN H. ARMSTRONG
*Columbia University
New York, N. Y.*

Due Credit

DEAR SIRS:
YOUR article "Electrodynamic Ammeter for VHF" in *ELECTRONICS* (*Electron Art*, Sept. 1950) does not credit the development of the electrodynamic ammeter to those responsible for it.

In 1934, Professor H. M. Turner suggested to Dr. P. C. Michel, a graduate student at Yale University, that he examine the field of current measurement at high frequencies and try to make a contribution to the art in his doctorate thesis. Dr. Michel perceived that the attempt to operate a conventional pointer caused the poor performance of the electrodynamic ammeters previously developed and, by allowing the short-circuited ring to oscillate, invented an absolute standard of current at high frequencies. When Dr. Michel came

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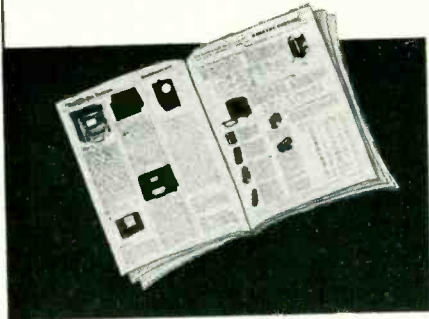
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MICRODIAL

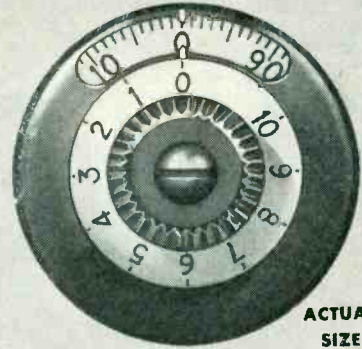
TEN TURN-COUNTING DIAL

Microdial is composed of two concentrically mounted dials... one for counting increments of each turn and the other for counting turns. The incremental dial has 100 equal divisions and is attached rigidly to the shaft so there is no backlash. Thus the contact position is indicated to an indexed accuracy of 1 part in 1000. Rotation is continuous in either direction. There are no stops on the Microdial assembly.

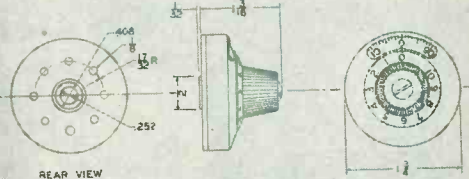
COMPACT... Microdial has same O.D. as Micropot... requires no more panel space.

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CONVENIENT... delivered completely assembled with dials synchronized. Easily mounted in a few seconds. All dials may be locked.



ACTUAL
SIZE



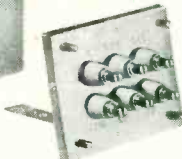
Microdial... turn-counting dial, primarily designed for use on Micropot ten turn linear potentiometers... use it on any multiturn device having ten turns or less.



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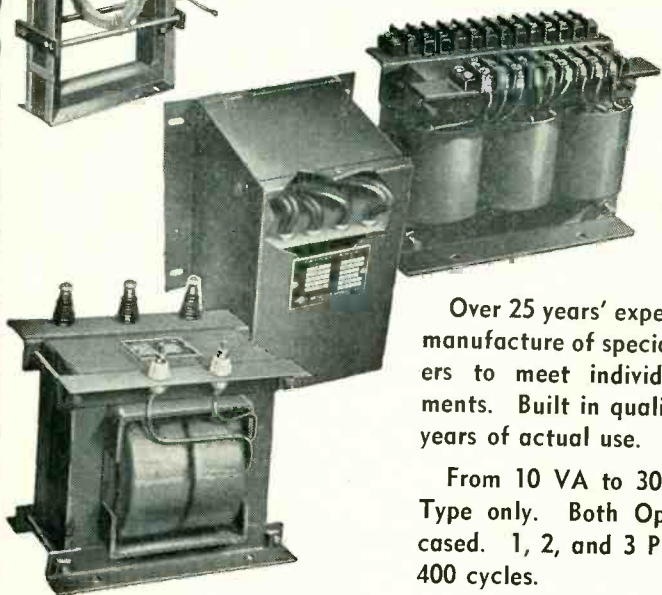
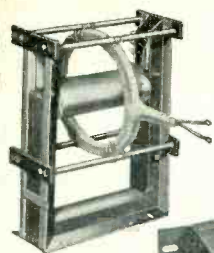
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to the General Engineering and Consulting Laboratory of the General Electric Co. at Schenectady, he was assigned to a group vitally concerned with such standards. The group continued the development of the electrodynamic ammeter, extending its frequency range up to 350 megacycles.

This new current standard provided new knowledge of the true frequency characteristics of thermocouple ammeters and led to the invention of an improved thermocouple, U. S. Patent 2,199,247—T. A. Rich, H. R. Meahl and P. C. Michel—1939, which was used in the General Electric Low-Impedance Thermocouple Ammeter.

One early application of these new thermocouple ammeters was the solving of a problem for the National Bureau of Standards which had resulted from attempts to measure r-f output of electrotherapy machines. When these were tested by measuring output current with then commercially available thermocouple ammeters, efficiencies greater than 100 percent were indicated.

The writer was asked by the Bureau if General Electric would supply a satisfactory ammeter and took several developmental samples of the ammeter to Washington, which solved the immediate problem. While there, the writer suggested that the Bureau might want an electrodynamic current standard. Later, a quotation was requested on an electrodynamic current standard and on a set of the Low-Impedance Thermocouple Ammeters. The Bureau purchased a set of these new thermocouple ammeters but at the time, showed no further interest in the accompanying quotation on an electrodynamic current standard.

Some time later, the Bureau asked for further information and Dr. Michel loaned them a copy of his unpublished thesis.

The only published data we have since seen on work on the Electrodynamic Ammeter at the Bureau of Standards is CRPL Preprint 50-15 by Max Solow. There is no attempt in that preprint to attribute full credit for this development to the Bureau; in fact, proper refer-

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ences are included, even the unpublished thesis.

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General Engineering and
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Schenectady, N. Y.

Maxson, Not Maxon

DEAR SIRs:

IN the October, 1950 edition of ELECTRONICS an article was written by Jack Kritz entitled "Precision Phase Meter for Audio Frequencies." In the by-line for this article the name of the company was misspelled. It would be appreciated if, in the next edition, you would print a correction notice calling attention to the proper spelling of the company name.

THE W. L. MAXSON CORPORATION
Contracts Department
Engineering Division

Electronics Quiz

THIS MONTH'S puzzle problem was submitted by Walther Richter, Consulting Electrical Engineer, Allis-Chalmers Manufacturing Company, Milwaukee, Wisconsin.

After having designed and constructed an entirely conventional full-wave rectifier circuit feeding a purely resistive load, the direct current through which is to be adjusted to exactly one ampere, the ham doing the work is suddenly seized by a spasm of caution (obviously a purely fictitious person) and decides to fuse the circuit. At first he decides to place a one-ampere fuse in the center leg, that is, between the load and the center tap of the transformer. But then he realizes that this might not prevent damage to the transformer from a short occurring from plate to plate. He wishes to employ the smallest fuses that are just able to carry the load current.

Assuming that fuses were available in any desired rating, and would blow at exactly this rating, would the

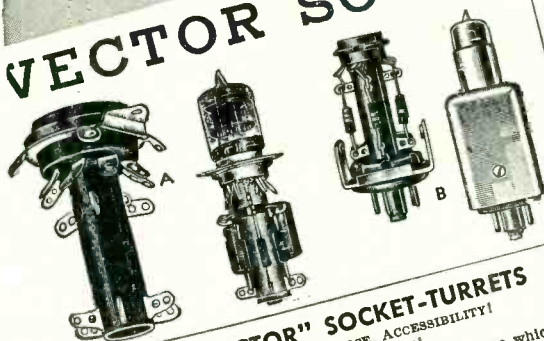
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SAVE SPACE, TIME, COSTS! IMPROVE HF PERFORMANCE, ACCESSIBILITY! MANUFACTURERS: WRITE US FOR QUANTITY PRICES!
These are unique new terminal structures which hold tubes and upon which assemblies may be quickly and neatly connected directly at the socket. They simplify job-assemblies with minimum connections, minimize number and length of leads, eliminate wire your circuits quickly without fuss and planning of mountings! Use sockets to reduce over-all chassis area! IMPORTANT: Several types may be included in quality for minimum prices: Impregnation of turret tubes for moisture and fungus damage on special order — add letter G to type number and add 5c to the catalog price. See drawing for sketch of socket-turret in use.

Octal Socket Turrets

Octal Socket, wrap-around contacts, steel saddle with 1 1/8" mtg. center hole. Turret 3/4" dia., 1/8" wall approx.; Grade XXXP natural phenolic adhesive bonded and bonded with phenolic adhesive. Set into recessed hole in socket and bonded with phenolic adhesive. Three near socket except in shortest type.

**Description
Terminals in 2 rings spaced 1 1/8"
Terminals in 2 rings spaced 1 1/8"
Terminals in 2 rings spaced 1 1/8"

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02-262	C10-O	2 1/2 x 2"	1.00
02-263	C12-O	3 x 2"	1.00

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02-266	B12-M	3 x 2"	1.00

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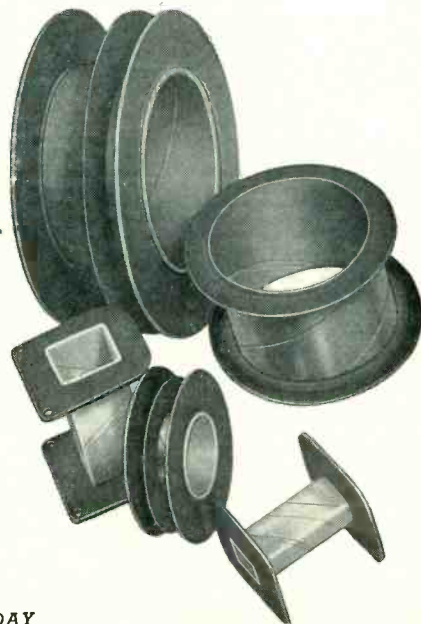
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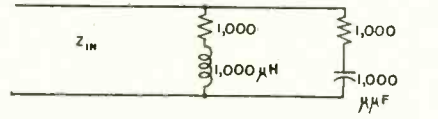
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choice of one ampere in the center, or presumably one-half ampere in series with each plate be correct?
The answer to this problem will appear in next month's *Backtalk* along with a new problem. Readers are encouraged to submit puzzle problems. A payment of five dollars will be paid for each acceptable entry (with solution).

Last Month's Solution
Last month's problem was:
What is the input impedance and the frequency for which the following circuit



has unity power factor (anti-resonance)?

Solution. The input impedance Z_{IN} is 1,000 ohms, and the anti-resonant frequency is indeterminate—that is, the circuit is resonant for all frequencies. The susceptance of the L branch is

$$\frac{\omega 10^{-3}}{10^6 + \omega^2 10^{-9}}$$

The susceptance of the C branch is

$$\frac{1}{10^6 + \frac{1}{\omega^2 10^{-18}}}$$

For unity power factor these two equations are equal

$$\frac{\omega 10^{-3}}{10^6 + \omega^2 10^{-9}} = \frac{1}{10^6 + \frac{1}{\omega^2 10^{-18}}}$$

$$\omega 10^3 + \frac{10^{18}}{\omega} = \frac{10^{18}}{\omega} + \omega 10^3$$

which is an identity satisfied for all values of ω .

The input impedance Z_{IN} is equal to the reciprocal of the sum of the conductances

$$\frac{1}{Z_{IN}} = \frac{10^3}{10^6 + \omega^2 10^{-9}} + \frac{10^3}{10^6 + \frac{1}{\omega^2 10^{-18}}}$$

$$= 10^{-3} \left[\frac{1}{1 + \omega^2 10^{-12}} + \frac{\omega^2 10^{-12}}{\omega^2 10^{-12} + 1} \right] = 10^{-3}$$

Thus $Z_{IN} = 1,000$ ohms.

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Teletypewriters complete, components or parts. Any quantity and condition.

W-6864, Electronics
330 W. 42nd St., New York 18, N. Y.

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For manufacturing radio tubes, electronic tubes, cathode-ray tubes, lamps. New and used. Reasonably priced, satisfaction guaranteed.

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Letters "J" "N" & "Q"\$80.00 ea.
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For INDUSTRIAL USE and PROJECTION
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Including plumbing, pulse transformers, thermistors, bolometers, cavities, test equipment, etc. Highest prices paid.
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AIRCRAFT EQUIPMENT
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AN Cams	COILS	RELAYS	LARGE STOCK
APC's	CPZ & BFI	RESISTORS	OF OTHER ITEMS
BINDING POSTS	CONTROLS	SHOCK WIRE	
CABLE	CRYSTALS	SOCKETS	LET US QUOTE
CAPACITORS	FILTERS	SOLENOIDS	YOUR NEEDS
CERAMICS	FUSES	SPACER'S	
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COLLINS ART-13 FREQ. MULT. UNIT
2-18 Mc for two 1625 Tubes. Comp. Assy less Tubes & Coils w/ ckt dia. **\$9.95**

EE89A Telephone Repeater
Used to extend range of field telephones. Simplex Teleg. and 20 cycle ringing possible over lines equipped with unit. Supplied w/ 305 tube. Phone supplied. (Foam-weight) \$9.49



ARC 5 MODULATOR
MD7/ARC5 w/ dynamotor complete w/ Tubes 1-12J5, 2-1625, 1-UR50. Good cond. Price \$8.95



MINICAP PIGTAIL

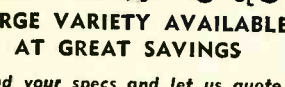
Mfd. Volt Price

2	50	.10
4	50	.10
4	100	.15
4	150	.18
4	200	.18
5	25	.10
5	50	.10
5	150	.10
8	150	.15
8	100	.18
8	150	.18
8	200	.20
10	50	.18
10	150	.20
12	450	.23
12	100	.20
16	150	.22
16	300	.30
16	450	.40
20	25	.10
20	50	.15
20	80	.18
20	350	.30
24	350	.30
25	25	.10
30	300	.25
30	450	.30
40	150	.20
40	450	.40
50	25	.22
50	50	.25
50	150	.30
100	50	.60
100	150	.50
100	50	.60
500	25	.75
1000	6	1.20
2000	6	1.35
1200	1.5	1.10
8-8	450	.60
8-16	450	.65
10-10	150	.50
10-10	450	.35
16-16	450	.70
20-20	150	.40
20-20	450	.50
40-20	450	.55
50-50	150	.35
50-30	150	.35
70-30	175	.85

Ceramic Case Mic

120MMF	
10KVF	\$19.00
30MMF	
10KVF	19.00
.05 MFD	10.00
.001	12.00
20KVF	24.00
.005	15.00
15KVF	21.00
.001 25K	35.00

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400 MA 12 Hm Choke 90 Ohms Herm. sealed. Special ...\$7.75

Choke Swinging
9/60Hv 400/.05 Amp 10000V Ins. Mfg. Super Elect.\$7.95



MS49 and MSSO Flashpole Antenna. 74" long. Both for 49¢

29¢ ea. 10 for \$2.75 MFD. VOLT

2x 8	450
2x 10	450
2x 15	450
2x 20	450
2x 25	450
2x 30	450
2x 35	450
2x 40	450
2x 45	450
2x 50	450
2x 60	450
2x 75	450
2x 90	450
2x 105	450
2x 120	450
2x 135	450
2x 150	450
2x 165	450
2x 180	450
2x 195	450
2x 210	450
2x 225	450
2x 240	450
2x 255	450
2x 270	450
2x 285	450
2x 300	450
2x 315	450
2x 330	450
2x 345	450
2x 360	450
2x 375	450
2x 390	450
2x 405	450
2x 420	450
2x 435	450
2x 450	450
2x 465	450
2x 480	450
2x 495	450
2x 510	450
2x 525	450
2x 540	450
2x 555	450
2x 570	450
2x 585	450
2x 600	450
2x 615	450
2x 630	450
2x 645	450
2x 660	450
2x 675	450
2x 690	450
2x 705	450
2x 720	450
2x 735	450
2x 750	450
2x 765	450
2x 780	450
2x 795	450
2x 810	450
2x 825	450
2x 840	450
2x 855	450
2x 870	450
2x 885	450
2x 900	450
2x 915	450
2x 930	450
2x 945	450
2x 960	450
2x 975	450
2x 990	450
2x 1005	450
2x 1020	450
2x 1035	450
2x 1050	450
2x 1065	450
2x 1080	450
2x 1095	450
2x 1110	450
2x 1125	450
2x 1140	450
2x 1155	450
2x 1170	450
2x 1185	450
2x 1200	450
2x 1215	450
2x 1230	450
2x 1245	450
2x 1260	450
2x 1275	450
2x 1290	450
2x 1305	450
2x 1320	450
2x 1335	450
2x 1350	450
2x 1365	450
2x 1380	450
2x 1395	450
2x 1410	450
2x 1425	450
2x 1440	450
2x 1455	450
2x 1470	450
2x 1485	450
2x 1500	450
2x 1515	450
2x 1530	450
2x 1545	450
2x 1560	450
2x 1575	450
2x 1590	450
2x 1605	450
2x 1620	450
2x 1635	450
2x 1650	450
2x 1665	450
2x 1680	450
2x 1695	450
2x 1710	450
2x 1725	450
2x 1740	450
2x 1755	450
2x 1770	450
2x 1785	450
2x 1800	450
2x 1815	450
2x 1830	450
2x 1845	450
2x 1860	450
2x 1875	450
2x 1890	450
2x 1905	450
2x 1920	450
2x 1935	450
2x 1950	450
2x 1965	450
2x 1980	450
2x 1995	450
2x 2010	450
2x 2025	450
2x 2040	450
2x 2055	450
2x 2070	450
2x 2085	450
2x 2100	450
2x 2115	450
2x 2130	450
2x 2145	450
2x 2160	450
2x 2175	450
2x 2190	450
2x 2205	450
2x 2220	450
2x 2235	450
2x 2250	450
2x 2265	450
2x 2280	450
2x 2295	450
2x 2310	450
2x 2325	450
2x 2340	450
2x 2355	450
2x 2370	450
2x 2385	450
2x 2400	450
2x 2415	450
2x 2430	450
2x 2445	450
2x 2460	450
2x 2475	450
2x 2490	450
2x 2505	450
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2x 2535	450
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2x 2580	450
2x 2595	450
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2x 2640	450
2x 2655	450
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2x 2805	450
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2x 2865	450
2x 2880	450
2x 2895	450
2x 2910	450
2x 2925	450
2x 2940	450
2x 2955	450
2x 2970	450
2x 2985	450
2x 3000	450
2x 3015	450
2x 3030	450
2x 3045	450
2x 3060	450
2x 3075	450
2x 3090	450
2x 3105	450
2x 3120	450
2x 3135	450
2x 3150	450
2x 3165	450
2x 3180	450
2x 3195	450
2x 3210	450
2x 3225	450
2x 3240	450
2x 3255	450
2x 3270	450
2x 3285	450
2x 3300	450
2x 3315	450
2x 3330	450
2x 3345	450
2x 3360	450
2x 3375	450
2x 3390	450
2x 3405	450
2x 3420	450
2x 3435	450
2x 3450	450
2x 3465	450
2x 3480	450
2x 3495	450
2x 3510	450
2x 3525	450
2x 3540	450
2x 3555	450
2x 3570	450
2x 3585	450
2x 3600	450
2x 3615	450
2x 3630	450
2x 3645	450
2x 3660	450
2x 3675	450
2x 3690	450
2x 3705	450
2x 3720	450
2x 3735	450
2x 3750	450
2x 3765	450
2x 3780	450
2x 3795	450
2x 3810	450
2x 3825	450
2x 3840	450
2x 3855	450
2x 3870	450
2x 3885	450
2x 3900	450
2x 3915	450
2x 3930	450
2x 3945	450
2x 3960	450
2x 3975	450
2x 3990	450
2x 4005	450
2x 4020	450
2x 4035	450
2x 4050	450
2x 4065	450
2x 4080	450
2x 4095	450
2x 4110	450
2x 4125	450
2x 4140	450
2x 4155	450
2x 4170	450
2x 4185	450
2x 4200	450
2x 4215	450
2x 4230	450
2x 4245	450
2x 4260	450
2x 4275	450
2x 4290	450
2x 4305	450
2x 4320	450
2x 4335	450
2x 4350	450
2x 4365	450
2x 4380	450
2x 4395	450
2x 4410	450
2x 4425	450
2x 4440	450
2x 4455	450
2x 4470	450
2x 4485	450
2x 4500	450

Carbon Pile Voltage Regulator
* Contract #NOAS-858 Bendix Aviation. MFRS Drawing 111144 w/mnt & pot.
* Type A, 105-115 amps 35°. 45° C. Ser. 28YK 809-JL. Reg. Volt. 80 Volts. Leland Electric. In enclosed base. Bendix Aviation.
* A-M Ref. #5U/1304 w/rect. & resist. in base. Type E 80V AC.
* Type C. Coll amps. 80 at 25C. Output volts 19. Ser. 3711-702. Spec. VR 9000-2C. Output amps 5.7. Input volt 22-30 w/resist. Leland Electric. These regulators are in brand new condition, priced at \$2.75 each.

BATHTUB CAPACITORS

Mfd	Volt	Type	Price
5	400	2BT	\$2.25
5	600	2TT	\$2.25
5	600	3TT	\$2.45
3x.1	600	3ST	\$4.35
3x.1	600	3ST	\$4.35
2x.1	400	3ST	\$2.25
2x.1	400	3ST	\$2.25
2x.1	600	3ST	\$2.65
2x.1	400	2TT	\$2.25
2x.1	200	2ST	\$2.20
2x.1	600	2BT	\$2.25
2x.1	600	3TT	\$2.25
1-1-1	400	3ST	\$2.25

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Our warehouses are full of surplus radio, radar, electronic equipment, for your needs, as a manufacturer, jobber, amateur, experimenter, engineer, everything at surplus prices. We own what we sell, phone or write us your needs and let us quote.
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ANTENNA MAST
Are you in a dead spot? If you can't get a good T.V. Picture here is a slgt. Corp. Ant. mast 30' high of rugged plywood construction to solve your problem. It telescopes into 3 ten feet. sec. for easy storage. Easy to Mim Comp. with stakes \$19.95 & rods. Each...

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SPST No closes at 85°. .69¢ ea
SPST No opens at 85°. .69¢ ea.
5 amp contacts
BC433 Mod or unmod CW Reception 200-1750KC in 3 bands 14 or 24V & 115V AC ADF Radio Compass As Is. Less Tubes Poor Condition \$10.49

DS FILTER CONDENSERS
40-20 135 10c
20-20 150 19c
2x30 150 29c
40x20 150 39c
2x40 150 39c
30x20 150 39c
2x50 150 39c
3x20 150 39c
3x30 150 39c
50/2x40 25/150 39c
2x40/12 150 39c
2x40/20 150 39c
3x20 150 39c
2x50/20 150/25 39c
2x50/10 150 39c
60-30/150 150/25 39c
80-40-30/150 150/25 39c
40-30 200 39c
20-16/10 200/25 39c
2x32 250 39c
2x32 350 39c
50x30 350 49c
16-8 450 49c
32x16 450 55c
2x3/25 450/75 49c
3x30/20 450/25 49c
Many Others

BC 221 Freq. Meters. Good condition complete w/calibration book tubes xtals & spare parts \$75.00 ea.
1 82A 5" 360° Comp. Insid. & Selsyn Receiver New ...\$4.95
BC 308A Ant. Tuning unit for BC 375 Excellent Cond. \$1.50 ea.
Motor Driven Yagi Switch 24V 1800 RPM. Price English Type ...\$3.95
BC434 Control Box Remote Control for 433 Radio Compass contains 0-5MA Meter. Dial Control \$3.95

Comb. Transformers—115V/50-60 cps. input

Item	H.V.	Amp	Filaments	Price
CT-861	2100VCT	.175	7.5VCT/4A, 2.5V/10A	\$7.29
CT-142	645VCT	.080	5V/2A, 6.3V/1.2A	4.25
CT-825	360VCT	.340	6.3VCT/3.6, 6.3VCT/3A	3.95
CT-076	600V	.100	2x12.6V/1.1	1.95
CT-626	1500V	.070	2.5/12, 30/100	9.95
CT-154	350VCT	.070	6.3/6, 6.3/1.8 lbs.	2.95
CT-071	110V	.200	33/200, 5V/10, 2.5/10	4.95
CT-378	2300V	4 MA	2.5/2	6.9
CT-367	580VCT	.050	5VCT/3A	2.25
CT-721	550VCT	.100	6.3/1, 2.5VCT/2	2.25
CT-99A	2x110VCT	.010	6.3/1A, 2.5VCT/7A	3.25
CT-91A	720V	.100	12.5/90/84MA, 6.3/5A	3.95
CT-080	700VCT	.205	5V/2A, 6.3V/2A	3.95
CT-328	110V	2.2	40V/2.2A, 115V/2.2A	4.49
CT-441	50V	.200	5V/2.4, 5V/1.2	2.2
CT-408	350VCT	.026MA	5V/3A	2.75
CT-26B	1100VCT	.250MA	6.3V/1.6, 400V B/9S.	6.25
CT-931	585VCT	.086	5V/3A, 6.3V/6A	4.25
CT-610	1250	.002MA	2.5V/2.1A, 2.5V/1.75A	4.9
CT-137	350VCT	.026MA	5V/3A	2.75
CT-102	1080VCT	.055	25V/3A, 6.3V/1.8A, 6.3V/1.2A	5.95
CT-866	330V	.065	6.3V/1.2, 6.3V/600MA	1.75
CT-319	330VCT	.085	5V/2, 6.3/7.5, 6.3/3	3.25
CT-526	510VCT	.025	12.5/90/84MA, 6.3/5A	1.95

Filament Transformers—115V/50-60 cps input

Item	Rating	Each
FT-852	23V	\$1.79
FT-30B	58V/2.2A	2.25
FT-589	78V/3.00, 6.3V/2A	1.95
FT-719	1.3V/6A	.79
FT-029	13.5V/1.1A	.79
FT-074	2.5V/10A, 6.3/9A	1.79
FT-23	6.3V/3A	1.1
FT-346	5VCT/13.5, 5VCT/6.75, 5VCT/6.75	5.95
FT-781	866 Trans. 2 x 2.5/5A	2.25
FT-364	6.3/2, 6.3/4.5	1.49
FT-511	3.4V/300A, 7 1/2" H x 10" x 5" 2/W	14.95
FTG-31	2.5V/2.5, 7V/7A (Tape @ 2.5V/2.5A), 16 lbs.	9.95
FT-674	8.1V/16A	1.10
FT-157	4V/16A, 2.5V/17.5A	2.95
FT-391	6.4V/3A	1.10
FT-736	2 x 6.3VCT/3.2-1.2A	1.49
FT-461	2 x 6.3VCT/1A	1.10
FT-899	2.5V/5.8A 29000 Rms.	15.95
FT-418	6.3VCT/1A, 6.3VCT/7A	1.95
FT-735	6.3VCT/5A, 6.3VCT/1A	1.79
FT-101	6V/25A	.79
FT-738	6.3VCT/1, 2.5V/2	1.69
FT-774	6.3V/16A	.79

Plate Transformers—115V/50-60 cps input

Item	Rating	Each
PT-976	Auto: 120VCT/10 MA	\$1.79
PT-31A	2 x 300V/5 MA	1.79
PT-46A	4030VCT N. L. 3% to 1 8" H x 6" W x 7" L 20 lbs.	29.95
PT-033	4150V/400 MA 1 1/2" x 9 1/4" W x 9" D 70 lbs.	49.95
PT-75	2 3/80/3446/3112VCT/77 MA	10.95
PT-28-1	4600VCT/.07	12.95
PT-403	Auto: 70V/1A	1.25
PT-160	120VCT/770 MA, 590VCT/82 MA, 25 lbs	24.95
PT-170	Auto: 156/146/137/138—71 MA	3.29
PT-848	3140VCT/750 MA for 68345, 5C1069A.	69.95
PT-139	42V/46V/50V/55V/15.2A 7 1/2" x 7" W x 6 1/2" H	10.95
PT-37	400V/20 MA	.99
PT-589	9V/1.6A	.49
PT-67-1	62VCT/3.5A	2.95
PT-12A	280VCT/1.2A	2.95
PT-10A	690V/450 MA	4.95
PT-054	980V/450 MA	5.29
PT-997	76V/.0075A KVA	1.49

SPECIAL TYPES

Item	Pri.	Output	Price
STF-946	210/220/230	25V/4A 3 1/2" H x 2 1/2" x 2 1/2" D	\$1.29
STF-443	220/440	11VCT 125A 6 1/2" L x 6 1/2" W x 1 1/2" H	15.95
STF-638	230	5V/9A 5 1/2" H x 4 1/2" x 3 3/4" D	1.25
STF-05A	115/230	2 x 5V/7.57" H x 7" x 5" D	4.25
STF-682	230	30-25-20V/1 MA	.69
STF-968	230	2.5V/6.5A	1.10
STF-105	230/115	5V/12.9A 2 1/2" x 2 1/2" x 2 1/2"	2.95
STF-370	220/440	3 x 2.5V/57, 2.5V/15A, 5 1/2" x 5 x 4 1/2"	5.25
STF-119	110/220	2.5V/500A, 7 x 5 1/2" x 5, 19.95	19.95
STF-61A	220	2 x 40V/.05/2 x 5V/6A, 12.6/1A	2.95
STF-631	230	2 x 5V/27A 2 x 5V/8A, 103/4H x 5 x 7.30 lbs	24.95
STF-96B	230	2.5V/6.5A	1.95
STF-608	220	24V/600, 5V/2A, 2 x 6.3V/1A	2.25
STF-45A	43/78/90	2 x 2.5/6.5, 6.3V/4	3.25
STF-306	115/180/230	5VCT 10 amp 10000 VT	19.95

SPECIAL PLATE TRANSFORMERS

Item	Pri.	Output	Price
STP-945	210/20/30	110VCT/300 5/4 x 4 x 3 1/2"	\$5.95
STP-444	230/480	230/105/115/125/15 lbs.	14.95
STP-643	230V	5 1/2" x 6 x 4 1/2"	1.29
STP-823	137V	222VCT/300 MA	2.95
STP-780	82V	400V/.002	1.29
STP-08B	50V	5 x 7.5V/10 MA	2.95
STP-311	30/35/40	95 NL-50VFL 1 Amp.	.59
STC-627	230V	1500/160, 110V/200, 3.3V/200, 5V/10, 2.5, 3.4/10	\$5.9
STC-611	230V	200V/200, 4 x 6.3V/3.	2.95
STC-16A	220V	260V/.03, 100V/1, 6.3V/4.2	2.95
STC-607	220V	700VCT/75 MA, 40VCT/100, 15/10/15V/100	3.95
STC-612	230V	400V/30, 190/30, 2, 5V/2.5 w/2-866 Socket	3.95

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Min. Order \$3.00
131 Liberty St., New York, N. Y. Dept. E-1

FILTER CHOKES

ITEM	RATINGS	PRICE
CH488	10 HY .030A	45¢
CH791	Dual 1. 65V-125 HY 100 MA	59¢
CH917	10HY .450A	12.95
CH10C	20HY .060A	1.10
CH86C	Dual .01-3.5HY 950-75MA	1.10
CH19-1	15HY .110A	1.59
CH921	20HY 80MA	1.49
CH22-1	7HY 900A	29.00
CH779	1HY 100A	49¢
CH25A	.6HY 490A	1.69
CH528	SW .09/.018HY 3/3A	1.69
CH922	200HY 100MA	2.75
CH043	1000HY 0MA	59¢
CH047	2 2HY 80MA	79¢
CHC29	2HY 200MA	3.25
CH867	SW15/29HY 150A	1.95
CH323	1.8HY 180A	1.25
CH360	2 1HY 200A	98¢
CH7A-1	15HY 15MA	1.79
CH791	1.75HY 100A	59¢
CH161	Dual 30HY .020A	1.35
CH373	11.5HY 90MA	1.95
CH21-A	.045HY 900A	1.35
CH045	5HY .040A	1.45
CH044	.01HY 2.5A	1.55
CH136	25HY 80MA	2.25
CH381	14HY 250A	9.95
CH702	6HY 150A	95¢
CH163	26HY .070A	1.39
CH116	.030HY 2A	12.95
CH152	10HY 600A	12.45
CH917	10HY 500A	79¢
CH756	30HY 25MA	79¢
CH67-1	.35HY 35A	2.95
CH38A	Dual 20HY 100A	8.95
CH064	3W/36HY 570/130A	7.95
CH084	20HY 300A	1.00
CH110	25HY .065	2.29
CH480	.333HY 1.12A	2.09
CH189	120HY 17MA	2.45
CH89A	Dual 1.52HY .167A	1.95
CH14A	100HY 1A	1.95
CH142	5HY 300A	1.45
CH382	5HY 150A	1.39
CH246	15HY 100A	1.10
CH141	Dual 7-11HY 75-60MA	1.75
CH961	Dual 22-44HY 6-4A	15.95
CH351	.033HY 7A	19.95
CH883	11HY 150A	7.95
CH1A1	5HY 100A	4.95
CH007	3.5HY .500A	.79

400 CYCLE CYCLER

Item	Rating	Price
6.3V/1.8A P/O APG2		\$1.49
6.4V/2.5 400VCT/35MA, 6.4/1.50A		3.49
6.4V/7.5, 6.4/3.8, 6.4/2.5A		2.49
6.4V/7.5, 6.4/3.2, 9.1/25/2A		1.95
6.4V/8A, 6.4V/1A		2.09
6.3V, 9.1A, 6.3VCT/6.5A, 2 x 2.5/3.5A		2.99
5V/2A, 6.3V/2A, 5V/2A, 6.3/5A		5.95
5V/15A, 5000V Ins.		6.00
6.3/2, 7.6, 3.8, 8.6, 6.3VCT/21A		6.00
760V, 6.9V, 6.3V, 5V, 320V, 6.3V/20A		6.00
6.4/7.5, 6.4/3.8, 6.4/2.5		2.95
592V/118MA, 6.3/8.1A, 5V/2 W.E.		4.95
6.3V/9.1, 6.3VCT/.65A, 2 x 2.5V/3.5A		2.95
6VCT .0006 KVA		1.49
6.4V/8A, 6.4/1A		1.49
1034VCT/111A, 6.9V/10, 2 x 6.3V/1.2A		6.49
5V2, 6.3/2.63/1		3.29
526VCT/.60A, 6.3VCT/2A, 5VCT/29		3.49
400VCT/35MA, 6.4/2.5, 6.4/1.5VCT		2.29
2300VCT Large Qty		1.49
600VCT/28MA		.00015
2.5V/7.5A, 6.3V/3A, 6.5V/6.5, 6.5/2A.		3.95
For SCR729		2.95
640V/500MA, 2.5V/1.75A P/O APS/15B		3.95
360VCT/20MA, 1500V/1MA, 2.5V, 6.3/2.5, 6.3V, 6A, P/O T29A		4.95
2x2.5V/15A, 2.5V/10A, P/O APT 4		
2x2.5V/2.5A, 6.3V/2.25A, 1200V		
Tap 1000V-750V		
P/O AN-APS-15		
742 5V, 50 MA, 709V, 47 MA,		
871V/45 MA		
600VCT/111A, 2 3/4 x 2 1/4 x 3 1/4		
1150-1150, 2 3/4 x 2 1/4 x 3 1/4		
640VCT/250 MA, 6.3V/.9, 6.3V/.6, 5V/6A		
6.3V/9.1A, 2.5V/3.5A, 6.3VCT/1.5A, 2.5V/1.5A		
9800V/2800V/32 MA		
592 VCT 120 MA, 6.3V/8A, 5V/2A		
4540 VCT/250 MA		
5V/3A, 6.3V 2A		
70 to 111V @ 247-822VA		
5000V/290 MA, 5V/10A		
2200V/350 MA		
2.5V/5, 5200V/2 MA		
13.5 KV/3.5 MA		
734VCT/.177A, 1710VCT/177A		
6.3V/9A, 7.7V/.365A		
2.5/20A, 6.3V/2A, 6.3V/1A, P/O AN/APQ-5		
6.4VCT/7.5, 6.4VCT/3.8, 6.4VCT/2.5A		
6.3V/2.7, 6.3V/.66A, 6.3VCT/21A		
6.5V/12A, 250V/100 MA, 5V/2A, P/O AN-APS-15		
400VCT/35 MA, 6.4/.15A, 6.4V/2.5A		
600VCT/50 MA, 6.3VCT/2A, 5VCT/2A, P/O R58/AR08		
2400CT/.5MA, 640V/.5MA, 2.5V/1.75A		
15.35VCT/1A		
59.2V/118.63V/8.1, 5V/2A, P/O APQ 13		
6.3/9, 6.3V, 6.5V/8, 640/200 MA		
2 x 14CV/00014A, 12CV/00012A, P/O APG2		
3640V/400 MA, P/O APT 4		
23.5V Tapped 22V/47 MA		
600VCT/36 MA		
780V, 27V/4.3, 6.3V/2.9, 1.25V/20A		
6.4V/11 Amp, P/O APQ7		
2 x 6.3V/1.25A, P/O APQ13		

80V 400 CYCLE INPUT

Item	Rating	Price
6.3V/1A, 2.5V/2A, P/O PE172A		3.95

CONDENSERS



MICA SOLAR XMB TAPPED HOLES

Mfd.	Price
2500 V Test	\$0.29
000025	.29
00003	.29
00005	.29
000075	.29</

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5071930, Delco, 115 V., 60 Cycle, 7000 r.p.m. Price \$4.50 each net.

36938-2, Haydon Timing Motor, 110 V., 60 cycle, 2.2 w., 4/5 r.p.m.

Price \$3.00 ea. net.



Type 1600 Haydon Timing Motor—110 V., 60 cycle, 3.2 w., 4 r.p.m., with brake Price \$4.00 each net.

Type 1600 Haydon Timing Motor—110 V., 60 cycle, 2.2 w., 1/240 r.p.m. Price \$3.00 each net.

Type 1600 Haydon Timing Motor 110 V., 60 cycle, 2.3 w., 1 r.p.m. Price \$2.70 each net.

Type 1600 Haydon Timing Motor, 110 V., 60 cycle, 2.2 w., 1 1/5 r.p.m. Price \$2.70 each net.

Type 1600 Haydon Timing Motor 110 V., 60 cycle, 3.5 w., 1 r.p.m. With shift unit for automatic engaging and disengaging of gears. Price \$3.30 each net.

Type 1600 Haydon Timing Motor, 110 V., 60 cycle, 2.2 w., 1/60 r.p.m. Price \$3.00 each net.

Eastern Air Devices Type J33 Synchronous Motor 115 V., 400 cycle, 3 phase, 8,000 r.p.m. Price \$8.50 each net

Telechron Synchronous Motor, Type B3, 115 V., 60 cycle, 2 r.p.m., 4 w. Price \$5.00 each net.

Barber-Colman Control Motor, Type AYLC 5091, reversible 24 volts D.C. .7 amps 1 R.P.M., Torque 500 in. lbs. Contains 2 adjustable limit switches with contacts for position indication. Ideal for use as a remote positioner or a beam or television antenna rotator, will operate on A.C. 60 cycle. Price \$6.50 each net

SERVO MOTORS

CK 1, Pioneer, 2 phase, 400 cycle. Price \$10.00 each net.

CK 2 Pioneer, 2 phase, 400 cycle. Price \$10.00 each net

10047-2-A Pioneer 2 phase, 400 cycle, with 40:1 reduction gear. Price \$10.00 each net

FPE-25-16 Diehl Low-Inertia 20 V., 60 cycle, 2 phase, 1600 r.p.m., 85 amps. Price \$10.00 each net.

CK2, Pioneer, 2 phase, 400 cycle, with 40:1 reduction gear. Price \$11.50 each net.

CK5 Pioneer, 2 phase, 400 cycle. Price \$20.00 ea. net.

MINNEAPOLIS-HONEYWELL TYPE B Part No. G303AY, 115 V., 400 cycle, 2 phase, built-in gear reduction, 50 lbs. in torque. Price \$10.00 each net.

Kollsman Type 776-01 400 cycle 2 phase drag-up type, fix phase voltage 29, variable phase 35V. maximum, frequency 400 cycle.

Price \$10.50 each net.

**REMOTE INDICATING
MAGNESYN COMPASS SET**

Pioneer Type AN5730-2 Indicator and AN5730-3 Transmitter 26 V., 400 cycle.

Price \$40.00 per set new sealed boxes.



Kollsman Remote Indicating Compass Set Transmitter part No. 679-01, indicator part No. 680k-03, 26 V., 400 cycle. Price \$12.50 each net.

GYROS

Schwein Free & Rate Gyro type 46800. Consists of two 28 V. D.C. constant speed gyros. Size 8" x 4.25" x 4.25". Price \$15.00 ea. net.



Sperry A5 Directional Gyro, Part No. 656029, 115 volts, 400 cycle, 3 phase. Price \$20.00 each net.



Sperry A5 Vertical Gyro, Part No. 644841, 115 V., 400 cycle, 3 phase. Price \$20.00 each net.

Sperry A5 Amplifier Rack Part No. 644890. Contains Weston Frequency Meter. 350 to 450 cycle and 400 cycle, 0 to 130 voltmeter. Price \$15.00 each net.

Sperry A5 Control Unit Part No. 644836. Price \$7.50 each net.

Sperry A5 Azimuth Follow-Up Amplifier Part No. 656030. With tube. Price \$5.50 each net.

Sperry A5 Autopilot Indicator: contains Pioneer AY20 Autosyn 26 V., 400 cycle. Price \$9.50 ea. net.

Pioneer Type 12800-1-D Gyro Servo Unit. 115 V., 400 cycle, 3 phase. Price \$15.00 each net.

Norden Type M7 Vertical Gyro. 26 V., D.C. Price \$19.00 each net.

Allen Calculator, Type C1 Bank and Turn Indicator, Part No. 21500, 28 V. D.C. Contains 28 V. D.C. constant speed gyro. Price \$10.00 each net.

Type C1 auto-pilot formation stick, part No. G1080A3. Price \$15.00 each net.

GOVERNMENT approved instrument repair station No. 3564.

D.C. MOTORS

5069625, Delco Constant Speed, 27 V., 120 r.p.m. Built-in reduction gears and governor. Price \$7.50 each net.

C-28P-1A, John Oster Series Motor, 27 V., 0.7 amps., 7000 r.p.m., 1/100 h.p. Price \$4.50 each net.

Jaeger Watch Co. Type 44-K-2 Contactor Motor, Operates on 3 to 4.5 volts D.C. Makes one contact per second. Price \$2.00 each net.

General Electric Type 5BA10AJ52C, 27 V. D.C., 0.65 amps., 14 oz. n. torque, 145 r.p.m. Shunt Wound, 4 lead reversible. Price \$6.50 each net.

General Electric Type 5BA10AJ37C, 27 V.D.C., 0.5 amps., 8 oz., in. torque, 250 r.p.m. Shunt Wound, 4 leads reversible. Price \$6.50 each net.

General Electric Type 5BA10J18D, 27 V. 0.7 amps. 110 R.P.M. 1 oz. ft. torque. Price \$6.50 ea. net.

D.C. ALNICO FIELD MOTORS

S. S. FD6-16, Diehl, 27 V., 10,000 r.p.m. Price \$6.50 each net.

S. S. FD6-18, Diehl, 27 V., 10,000 r.p.m. Price \$6.50 each net.

S. S. FD6-21, Diehl, 27 V., 10,000 r.p.m. Price \$6.50 each net.

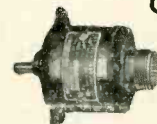
5069466 Delco 27.5 V. 10,000 R.P.M. Price \$10.00 ea. net

706343 Delco 27.5 V. 10,000 R.P.M. Shaft 0.5 in. long. Price \$7.50 ea. net.

5068571 Delco 27.5 V. 10,000 R.P.M. with blower assembly. Price \$10.00 ea. net.

5071895 Delco 27.5 V. 250 R.P.M. Price \$10.00 ea. net.

5072400 Delco 27.5 V. 10,000 R.P.M. Shaft 0.5 in. long with worm gear. Price \$6.75 ea. net.

**GENERAL ELECTRIC
D. C. SELSYNS**

8TJ9-PAB Transmitter, 24 V. Price \$3.75 each net.

8DJ11-PCY Indicator, 24 V. Dial marked -10° to +65°. Price \$4.50 each net.

8DJ11-PCY Indicator, 24 V. Dial Marked 0 to 360°. Price \$7.50 each net.

AMPLIFIER

Pioneer Gyro Flux Gate Amplifier, Type 12076-1-A. Price \$17.50 ea. net, with tubes.

G. E. Servo Amplifier Type 2CV2A1, 115 V. 400 cycle. Price \$10.00 ea. net.

Minneapolis Honeywell Amplifier Type G403, 115 V. 400 cycle. Price \$8.00

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SUPPLIER OF ELECTRONIC & AIRCRAFT EQUIPMENT**IMMEDIATE
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Wincharger Corp. Inverter PU/16 type MG 750, Input 24 V.D.C., 60 amps. Output 115 V, 400 cycle, 1 phase, 6.5 amps. **Price \$60.00 each net.**

Leland type 10285, Input 28 V. D.C. at 60 amps. Output 115 V. 3 phase at 750 V.A., 26 V., 400 cycle, single phase at 50 V.A.

Price \$100.00 each net

149H, Holtzer Cabot. Input 28 V. at 44 amps. Output 26 V. at 250 V.A., 400 cycle and 115 V. at 500 V.A., 400 cycle. **Price \$40.00 each net.**

149F, Holtzer Cabot. Input 28 V. at 36 amps. Output 26 V. at 250 V.A., 400 cycle and 115 V. at 500 V.A., 400 cycle. **Price \$40.00 each net.**

12117, Pioneer. Input 12 V.D.C. Output 26 V., 400 cycle, 6 V.A. **Price \$22.50 each net.**

12117-2 Pioneer. Input 24 V.D.C. Output 26 V. 400 cycle, 6 V.A. **Price \$20.00 each net.**

12116-2-A Pioneer. Input 24 volts D.C., 5 amps. Output 115 volts 400 cycle single phase 45 watts. **Price \$100.00 each net.**

5D21NJ3A General Electric. Input 24 V.D.C. Output 115 V., 400 cycle at 485 V.A. **Price \$25.00 each net.**

PE 218, Ballentine. Input 28 V.D.C. at 90 amps. Output 115 V., 400 cycle at 1.5 K.V.A. **Price \$50.00 each net.**

ACTUATORS

White Rodgers Electric Co. type 6905, number 3, 12 V., D.C., 1.3 amps., 1½ RPM, torque 75" in lbs., contains adjustable limit switches. **Price \$10.50 each net**

METERS

Weston Frequency Meter, Model 637, 350 to 450 cycles, 115 volts. **Price \$10.00 each net.**

Weston Voltmeter. Model 833, 0 to 130 volts, 400 cycle. **Price \$4.00 each net.**

Weston Voltmeter. Model 606, Type 204 P, 0 to 30 volts D. C. **Price \$4.25 each net.**

Weston Ammeter. Model 506, Type S-61209, 20-0 100 amps. D. C. **Price \$7.50 each net with ext. shunt.**

Weston Ammeter. Type F1, Dwg. No. 116465, 0 to 150 amps. D. C. **Price \$6.00 each net.**
With ext. shunt \$9.00 each net.

Westinghouse Ammeter. Type 1090-D-120, 120-0-120 amp. D. C. **Price \$4.50 each net.**

Weston Model 545. Type 82PE Indicator. Calibrated 0 to 3000 RPM. 2¾" size. Has built-in rectifier, 270° meter movement. **Price \$15.00 each net.**

Westinghouse Ammeter, type E1, part No. 1162965, range 0-300 amps. D.C. **Price \$7.50 each net.**

Weston Voltammeter, type 201-P, Mod. 606, range 0-30 volts D.C. and 0-30 amps. with shunt. **Price \$12.50 each net.**

RECTIFIER POWER SUPPLY

General Electric, Input 230 V. 60 cycle 3 phase. Output 130 amps. at 28 V. D.C. Continuous duty, fan cooled, has adjustable input taps. G.E. model No. 6RC146F. Size: Height 46", width 28", depth 17½". **Price \$225.00 each net.** New

PIONEER AUTOSYNS

AY1, 26 V., 400 cycle. **Price \$7.50 each net.**

AY14D, 26 V., 400 cycle, new with calibration curve. **Price \$15.00 each net.**

AY20, 26 V., 400 cycle. **Price \$7.50 each net.**



AY5, 26V., 400 cycle. Has hollow shaft. **Price \$7.50 ea. net.**

AY54D, 26 V., 400 cycle, with pointer for I 81 & I 82 Indicator. **Price \$10.50 each net**

PRECISION AUTOSYNS

AY131D, new with calibration curve. **Price \$35.00 each net.**

AY201-2-A. **Price \$35.00 each net.**

**PIONEER AUTOSYN
POSITION INDICATORS**

Type 5907-17. Dial graduated 0 to 360°, 26 V., 400 cycle. **Price \$20.00 each net.**

Type 6007-39. Dual, Dial graduated 0 to 360°, 26 V., 400 cycle. **Price \$30.00 each net.**

PIONEER TORQUE UNIT

Type 12606-1-A. **Price \$40.00 each net.**

**MAGNETIC AMPLIFIER
ASSEMBLY**

Pioneer Magnetic Amplifier Assembly Saturable Reactor type output transformer. Designed to supply one phase of 400 cycle servo motor. **Price \$12.50 each net.**

**PIONEER TORQUE UNIT
AMPLIFIER**

Type 12073-1-A, 5 tube amplifier, Mag-nesyne input, 115 V., 400 cycle. **Price \$17.50 each net with tubes.**

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MX-215/APG**

John Oster, 28 V.D.C., 7000 r.p.m. 1/100 h.p. **Price \$5.00 each net.**

Westinghouse Type FL Blower, 115 V., 400 cycle, 6700 r.p.m., Airflow 17 C.F.M. **Price \$5.00 each net.**

RATE GENERATORS

F16, Electric Indicator Co., two-phase, 22 V. per phase at 1800 r.p.m. **Price \$12.00 each net.**

J36A, Eastern Air Devices, .02 V. per r.p.m. **Price \$9.00 each net.**

B-68, Electric Indicator Co., Rotation Indicator, 110 V., 60 cycle, 1 phase. **Price \$14.00 each net.**

PM-1-M Electric Indicator Co. Same as type B35. 2 V. per 100 R.P.M. Max speed 5,000 R.P.M. Can be used as D.C. motor, 1/77 H.P. 115 V. D.C. **Price \$14.00 ea. net.**

SINE-COSINE GENERATORS

(Resolvers)

FPE 43-1, Diehl, 115 V., 400 cycle. **Price \$20.00 each net.**

SYNCHROS

1F Special Repeater, 115 V., 400 cycle. Will operate on 60 cycle at reduced voltage.



Price \$15.00 each net.

2J1F3 Selsyn Generator 115 volts, 400 cycle. **Price \$5.50 each net.**

2J1G1 Control Transformer, 57.5/57.5 V., 400 cycle. **Price \$1.90 each net.**

2J1H1 Selsyn Differential Generator, 57.5/57.5 V., 400 cycle. **Price \$3.25 each net.**

W. E. KS-5950-L2, Size 5 Generator 115 V., 400 cycle. **Price \$10.00 each net.**

1G Generator 115 V., 60 cycle. **Price \$40.00 each net**

5G Generator 115 volts, 60 cycle. **Price \$50.00 each net**

2J1F1 Selsyn Generator, 115 V., 400 cycle. **Price \$3.50 each net.**

5SDG Differential Generator 90/90 V., 400 cycle. **Price \$15.00 each net.**

1CT Control Transformer, 90/55 volts, 60 cycle. **Price \$40.00 each net.**

POSITION TRANSMITTER

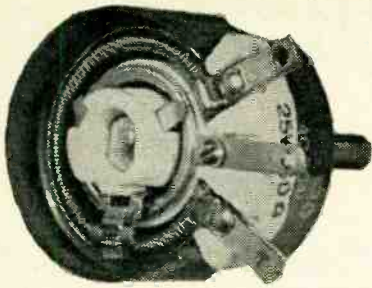
Pioneer Type 4550-2-A Position Transmitter, 26 volts 400 cycle, gear ratio 2:1. **Price \$15.00 each net.**

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ASSOCIATES**

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Ohm	Watt	Bush ing	Shaft	Cat. No.	Stock No.	Quan.	List Price	Ohm	Watt	Bush ing	Shaft	Type	Body Dia.	Stock No.	Quan.	List Price
2	25	5/8S	1/8SD	O-H	8A-1	523	\$5.20	6	4	3/8	7/16	CTS	1 9/16	P-68	77	\$2.25
3-3 (Dual)	25	1/2	1/2	J	8A-2	1339	5.20	10	2	3/8	1 5/8	---	1 5/16	P-64	112	1.75
15	25	3/8	1"	C	8A-3	175	5.20	20	2	3/8	2"	C	1 1/8	P-1	48	1.75
15	25	3/8	1 1/8	D-245	8A-4	213	5.20	20	2	1/2	1/8SD	CTS	1 1/4	4A-57	26	2.25
20	25	1/2	1 1/4	I	8A-5	10	5.20	20	4	3/8	3/8FD	M	1 5/8	P-3	78	2.25
25	25	1/2	1 1/2F	D-245	8A-6	377	5.20	30	4	3/8	1/4SD	CTS	1 9/16	P-4	8	2.25
25	25	3/8	1"	D-245	8A-7	31	5.20	50	2	3/8	7/8F	CTS	1 1/4	P-69	80	2.25
25	25	1/2	3/8S	I	8A-8	512	5.20	50	4	3/8	1 1/16	CTS	1 9/16	P-70	10	2.25
30	25	3/8	7/16	C	8A-9	7	5.20	50	4	3/8	5/16F	CTS	1 9/16	P-71	21	2.25
50	25	3/8	1"	D-245	8A-10	101	5.20	75	2	3/8	3/8SD	M	1 1/16	P-5	226	2.25
50	25	5/8	1 1/8	O-H	8A-11	5569	5.20	100	2	5/8	3/8F	---	1 5/16	P-32	270	2.00
75	25	1/2	1/8SD	O-H	8A-12	1051	5.20	100	4	3/8	5/16	CTS	1 9/16	P-6	352	2.25
100	25	3/8	7/16	D-245	P-54	79	5.20	100	4	3/8	5/16	CTS	1 9/16	4A-58	31	2.00
100	25	1/2	1/2	H	8A-13	148	5.20	100	4	3/8	1/2	C	1 1/8	P-22	38	2.25
225	50	3/8	11/16	O-H	8A-14	52	5.20	200	2	1/2	7/8	CTS	1 1/4	P-83	100	2.25
350	25	3/8	11/8	D-241	8A-15	132	5.85	255	2	1/2	1/8SD	CTS	1 1/4	P-73	12	2.25
350RHO	25	3/8	1 1/8	O-H	8A-16	892	5.20	300	2	3/8	1	CTS	1 1/4	P-7	31	2.25
500	25	3/8	1 1/16	H	8A-17	369	5.20	300	4	3/8	3/8	M	1 5/8	P-8	31	2.25
800	50	3/8	7/16F	D-245	8A-18	419	5.20	350	2	3/8	1 1/8	---	1 1/4	P-63	38	1.75
1K	25	1/2	1/2	O-H	8A-19	148	5.85	350	2	3/8	1/2	CTS	1 1/4	P-23	56	2.25
3K	25	3/8	1 3/16	D-245	8A-20	256	6.18	500	4	3/8	1 1/2	CTS	1 1/4	P-24	100	2.25
5K	25	1/2	1/8SD	O-H	8A-21	31	6.18	1K	2	3/8	3/8SD	CTS	1 9/16	P-10	90	2.25
5K	25	3/8	7/8FS	D-245	8A-22	7660	6.18	2K	2	1/2	5/8F	CTS	1 1/4	P-25	7	2.25
5K	50	3/8	1/8SD	O-J	8A-23	7660	6.18	2K	2	1/2	1/8SD	CTS	1 1/4	P-26	70	2.25
20K	25	1/2	1/8SD	D-245	8A-24	6901	7.00	2K	4	3/8	1/8SD	CTS	1 9/16	P-81	44	2.25
				D-245	8A-25			3K	4	3/8	1/2	C	1 5/8	8A-38	16	2.25
				D-245	8A-26			3K	4	3/8	1/2	CTS	1 9/16	P-82	100	2.25
								3K	4	3/8	1/2	CTS	1 9/16	P-13	37	2.25
								4K	4	3/8	1/2	CTS	1 1/4	P-28	244	2.25
								4K	4	3/8	1/2SD	CTS	1 5/8	8A-40	190	2.25
								5K	2	3/8	7/16SD	CTS	1 5/8	8A-39	2344	2.25
								5K	4	1/2	17/8	T	1 5/8	P-17	31	2.25
								7.5K	4	7/16	1/2SD	CTS	1 9/16	P-75	219	2.25
								10K	2	3/8	3/8SD	CTS	1 1/4	P-29	266	2.25
								10K	2	3/8	1 15/16	CTS	1 5/16	P-49	10	1.75
								10K	2	3/8	1 4SD	---	1 1/4	P-57	29	1.75
								10K	2	3/8	3/8F	---	1 1/4	P-42	880	2.25
								10K	4	1/2	5/8	T	1 5/8	8A-42	880	2.25
								10K	4	3/8	3/8	CTS	1 9/16	P-16	27	2.25
								10K	4	3/8	3/8	CTS	1 9/16	P-76	31	2.25
								15K	4	3/8	1/2SD	CTS	1 9/16	P-17	146	2.25
								20K	4	5/8	2 3/4	CTS	1 9/16	P-77	20	2.25
								20K	6	3/8	1 3/16	CTS	1 5/8	P-78	8	2.25
								40K	4	3/8	3/8SD	M	1 5/8	P-51	66	2.25

PRECISION POTENTIOMETERS

Ohm	Watt	Cat. No.	Stock No.	Quan.	List Price
10	6	D-292	8A-27	23	\$6.00
12	6	M-314AS	8A-28	14	6.00
5K	6	D-260D	8A-30	76	8.50
10K	6	D-271	8A-31	2	17.50
10K	12	371A	8A-32	2	15.00
10K	6	D5083-G2	8A-33	70	6.00
20K	6	D-260	8A-34	101	6.00
20K	6	M-314A	8A-35	757	8.50
20K	6	D-501	8A-36	14	8.50
100K	25			14	32.50
100K	25			2	32.50

WIRE WOUND POTENTIOMETER—
 DISCOUNT SCHEDULE

1 to 49... 80% off list price
 50 to 199... 80 & 10% off list
 200 and up... 80 & 10 & 10% off list

Different items may NOT be mixed for discount. Quantity discount allowed only to quantity shown. NEDA members write.

COMPOSITION POTENTIOMETERS

Ohm	Taper	Bushing	Shaft	Type	Stock No.	Quan.	Net Price
75	Lin.	3/8	3/8	J	P-34	65	\$1.00
200	Lin.	1/4	9/32	J	P-62	59	.75
1K	Lin.	1/2S	1/2	J	P-61	6	1.50
1.5K	Lin.	3/8	3/8SD	J	P-36	75	.35
2K	Lin.	1/2S	1/8SD	J	P-60	80	.75
5K	Lin.	5/16	1/8	J	P-35	90	.65
10K	Lin.	3/8	1/2	J	P-40	46	.75
10K	Lin.	1/2S	3/16SD	J	P-39	72	.75
10K	Lin.	3/8	3/8	J	4A-61	45	.75
50K	Lin.	3/8	1/2	J	P-58	26	1.00
75K	Lin.	3/8	3/8	CTS	P-41	8	.70
10-75K	Lin.	3/8	3/8F	CTS	P-46	28	.40
100K	Lin.	3/8	3/8	J	P-43	35	.70
100K	Lin.	3/8	7/16	J	4A-60	48	1.00
300K	Lin.	3/8	2 1/4S	J	P-56	117	1.25
25-400K	Lin.	1/4	1/8SD	J	P-35	115	.75
500K	Tap.	3/8	5/16	J	P-42	79	.70
1Meg.	Tap.	3/8	7/8	CTS	P-40	153	.40
1Meg.	Lin.	1/4	3/8	---	P-45	55	.70
2Meg.	Lin.	3/8	3/8	---	P-55	45	.40
2Meg.	Lin.	3/8	3/8F	CTS	P-48	79	.40
2Meg.	Lin.	1/2	1 9/16	CTS	P-49	208	1.00
10Meg.	Lin.	3/8	7/16F	J	P-49	27	.49

Write for our Unique Flyers. Complete Stocks of AN Connectors, Turret Sockets, Turret Lugs, Mounting Boards, Tube Sockets, Glass to Metal Seals, Stand-off Insulators, Etc.

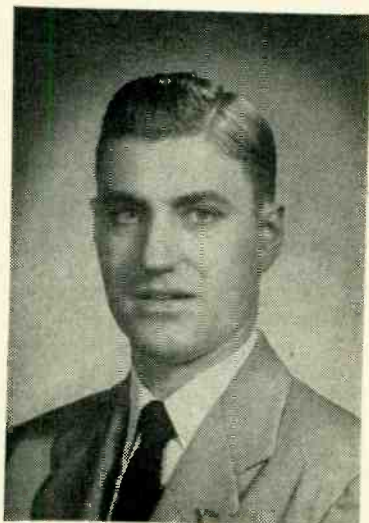
Widely Known for Fair Dealing and Good Service.

HAROLD H. POWELL

632 Arch Street

Philadelphia 6, Pa.

MARKet 7-5650



AN CONNECTORS

FAST SERVICE - LOW COST

Insert					Insert					Insert							
	3100	Shell & Price	3106	3108	3101		3100	Shell & Price	3106	3108	3101		3100	Shell & Price	3106	3108	3101
8S-1S	\$1.60	\$1.05	\$1.60	\$1.83	\$1.76	20-11S	1.60	1.05	1.60	1.83	1.76	24-10S	2.22	1.50	2.54	2.74	2.19
8S-1P	.62	.48	.64	1.02	.65	20-11P	1.60	1.00	1.67	1.83	1.68	24-10P	2.18	1.46	2.50	2.67	2.16
10S-2S	.59	.43	.56	.99		20-12S	1.42	.87	1.77	1.80	1.44	24-11S	2.42	1.70	2.75	2.87	2.37
10S-2P	.57	.43	.60	1.00		20-12P	1.35	.81	1.52	1.74	1.38	24-11P	1.95	1.43	2.27	2.60	2.12
10SL-3S			.79	1.03		20-14S	1.76	1.25	2.23	2.16	1.77	24-12S	2.02	1.90	2.31	2.80	2.34
10SL-3P	.69	.57			.71	20-14P	1.56	1.17	1.66	2.12	1.77	24-12P	1.85	1.23	2.16	2.39	1.92
10SL-4S			.61	1.10		20-15S	1.82	1.28	2.08	2.21	1.88	24-14S	2.00	1.28	2.33	2.45	2.00
10SL-4P	.64	.48			.65	20-15P	1.58	1.04	1.96	1.97	1.64	24-14P	1.60	1.09	1.92	2.25	1.70
12S-3S	.65	.48	.77	1.10	.69	20-16S	1.82	1.32	1.66	2.12	1.88	24-15S	2.21	1.55	2.63	2.77	2.25
12S-3P	.89	.50	.79	1.15	.68	20-16P	1.77	1.24	1.95	2.17	1.80	24-15P	1.87	1.76	2.16	2.67	2.17
12S-4S	.55	.41	.64	1.09	.62	20-17S	1.77	1.24	2.24	2.17	1.82	24-16S	2.11	1.38	1.87	2.37	2.07
12S-4P	.56	.41	.64	1.10	.62	20-17P	1.68	1.13	1.84	2.07	1.72	24-16P	1.68	1.12	1.68	2.02	1.82
12-5S	.64	.56	.79	1.20	.77	20-18S	1.93	1.37	2.33	2.33	1.97	24-17S	2.03	1.23	2.27	2.75	2.25
12-5P	.61	.50	.77	1.13	.69	20-18P	1.70	1.12	2.17	2.09	1.72	24-17P	1.52	1.00	1.83	2.17	1.62
14S-1S	.71	.53	.95	1.27	.81	20-19S	1.68	1.12	2.16	2.07	1.70	24-19S	2.24	1.52	2.20	2.69	2.20
14S-1P	.71	.53	.96	1.27	.81	20-19P	1.56	1.08	1.68	2.01	1.66	24-19P	1.82	1.32	2.13	2.51	2.02
14S-2S	.75	.87	.96	1.30	.79	20-20S	1.70	1.12	1.76	2.10	1.72	24-20S	2.25	1.52	2.38	2.89	2.26
14S-2P	.83	.65	.95	1.40	.87	20-20P	1.52	.96	1.76	1.91	1.56	24-20P	2.45	1.77	2.65	2.82	2.43
14-3S	.81	.57	.87	1.66	.83	20-21S	1.84	1.30	1.97	2.25	1.90	24-21S	1.93	1.46	2.27	2.30	1.86
14-3P	.83	.57	1.02	1.58	.85	20-21P	1.77	1.25	2.17	2.17	1.77	24-21P	1.84	1.25	2.02	2.55	1.82
14S-4S	.68	.57	.91	1.26	.68	20-22S	1.77	1.25	2.18	2.18	1.82	24-28S	2.92	2.25	3.23	3.30	2.90
14S-4P	.56	.43	.77	1.13	.59	20-22P	1.70	1.15	1.82	2.10	1.74	24-28P	3.72	3.03	3.80	4.08	3.67
14S-5S	.85	.63	.98	1.49	.93	20-23S	1.48	.93	1.85	1.88	1.52	28-2S	2.24	1.63	2.47	3.06	2.57
14S-5P	.85	.64	1.14	1.49	.95	20-23P	1.35	.81	1.52	1.74	1.38	28-2P	2.10	1.42	2.36	2.82	2.33
14S-6S	1.03	.86	1.23	1.68	.98	20-24S	1.57	1.03	1.68	1.88	1.60	28-3S	2.22	1.36	2.63	2.79	2.30
14S-6P	1.05	.84	1.19	1.65	1.04	20-24P	1.48	.93	1.64	1.87	1.52	28-3P	1.74	1.01	2.16	2.41	1.85
14S-7S	.89	.65	1.10	1.50	.89	20-26S	1.38	.99	2.02	1.93	1.56	28-4S	2.03	1.42	2.35	2.70	2.43
14S-7P	.79	.57	.90	1.26	.78	20-26P	1.38	.89	1.52	1.82	1.48	28-4P	1.74	1.17	2.17	2.50	2.10
14S-9S	.83	.60	.95	1.43	.83	20-27S	1.79	1.44	1.90	2.37	2.02	28-5S	2.36	1.44	2.33	2.86	2.36
14S-9P	.93	.67	.88	1.34	.77	20-27P	.25	1.84	2.37	2.77	2.42	28-5P	1.95	1.16	2.35	2.62	2.08
16S-1S	1.05	.89	1.29	1.54	1.15	20-28S	.79	1.44	1.90	2.24	2.02	28-6P	1.90	1.23	2.17	2.63	2.02
16S-1P	1.16	.75	1.29	1.76	1.15	20-28P	2.25	1.78	2.37	2.67	2.38	28-7S	2.13	1.20	2.47	2.62	2.13
16-2S	.91	.67	1.09	1.43	.93	20-29S	3.40	3.40	4.50	5.62	4.50	28-7P	1.70	1.03	2.10	2.49	1.80
16-2P	.83	.59	.99	1.43	.85	20-29P	3.40	3.40	4.50	5.62	4.50	28-8S	1.80	1.60	3.04	3.04	2.39
16S-3S	.73	.50	.89	1.36	.77	22-1S	1.41	.81	1.70	2.02	1.48	28-8P	2.05	1.46	2.89	2.89	2.43
16S-3P	.73	.50	.89	1.36	.77	22-1P	1.36	.75	1.60	1.92	1.37	28-9S	2.53	2.17	2.89	3.47	2.90
16S-4S	.77	.56	.93	1.17	.81	22-2S	1.72	1.15	2.10	2.25	1.74	28-9P	2.16	1.48	2.50	2.89	2.54
16S-4P	.77	.55	.93	1.42	.81	22-2P	1.58	1.02	1.76	2.13	1.60	28-10S	2.59	1.98	2.97	3.10	2.59
16S-5S	.87	.69	1.10	1.43	.95	22-3S	1.49	.92	1.92	2.01	1.50	28-10P	2.39	1.52	2.79	2.95	2.43
16S-5P	.87	.63	1.06	1.50	.90	22-3P	1.34	.79	1.58	1.90	1.34	28-11S	2.97	2.33	2.70	3.75	3.25
16S-6S	.85	.61	1.06	1.57	.95	22-4S	1.60	1.00	1.82	2.36	1.64	28-11P	2.90	2.38	2.81	3.40	2.89
16S-6P	.85	.61	1.01	1.49	.87	22-4P	1.48	.95	1.64	2.02	1.56	28-12S	2.63	2.38	2.98	3.53	3.00
16-7S	1.07	.83	1.04	1.66	1.09	22-5S	1.56	1.03	1.66	2.13	1.58	28-12P	2.63	2.19	3.02	3.62	3.10
16-7P	.95	.93	1.12	1.56	1.01	22-5P	1.48	1.48	1.56	2.04	1.48	28-15S	1.84	2.19	3.02	3.62	3.10
16S-8S	.95	.83	1.23	1.46	1.09	22-6S	1.52	.95	2.02	2.08	1.53	28-15P	3.42	2.86	4.08	4.30	3.50
16S-8P	1.05	.77	1.15	1.49	.99	22-6P	1.43	.85	1.72	1.43	1.43	28-16S	2.75	2.50	3.10	3.23	2.75
16-9S	1.09	.85	1.30	1.72	1.15	22-7S	1.54	.99	1.90	2.10	1.54	28-16P	2.03	1.77	2.39	2.97	2.35
16-9P	1.03	.81	1.20	1.62	1.07	22-7P	1.36	.81	1.60	1.92	1.36	28-17S	2.18	1.56	2.47	2.47	2.46
16-10S	1.05	.85	1.25	1.63	1.11	22-8S	1.49	1.00	1.66	2.19	1.56	28-17P	2.18	1.56	2.47	2.47	2.46
16-10P	.91	.69	1.09	1.54	.95	22-8P	1.18	.50	1.36	1.77	1.25	28-18S	2.45	1.82	2.83	3.25	2.65
16-11S	.95	.73	.99	1.57	1.01	22-9S	1.48	.90	1.97	2.02	1.50	28-18P	2.24	1.48	2.62	2.89	2.35
16-11P	.91	.64	1.09	1.52	.95	22-9P	1.28	.76	1.60	1.66	1.30	28-19S	2.14	1.54	2.45	2.83	2.45
16-12S	1.05	.81	1.23	1.65	1.09	22-10S	1.23	.87	1.42	1.94	1.35	28-19P	1.85	1.24	2.24	2.65	2.10
16-12P	.95	.71	1.11	1.54	.98	22-10P	1.35	.81	1.56	1.92	1.37	28-20S	2.52	1.99	2.84	3.20	2.90
18-1S	1.46	1.15	1.57	2.07	1.52	22-11S	1.38	.85	1.64	1.93	1.43	28-20P	2.52	1.60	2.50	3.03	2.53
18-1P	1.60	1.25	1.79	2.29	1.66	22-11P	1.16	.78	1.30	1.80	1.51	28-22S	2.73	1.80	3.06	3.22	2.73
18-2S	.90	.85	1.45	1.82	1.19	22-12S	1.68	1.10	1.92	2.22	1.48	28-22P	2.55	1.50	2.79	2.90	2.39
18-2P	.90	.83	1.45	1.82	1.19	22-12P	1.54	.99	1.84	2.10	1.57	32-1S	2.65	1.76	3.10	3.35	2.74
18-3S	1.11	.65	1.46	1.78	1.01	22-13S	1.72	1.15	2.14	2.25	1.72	32-1P	2.34	1.56	2.73	3.11	2.53
18-3P	1.09	.59	1.19	1.70	.99	22-13P	1.44	1.03	1.62	2.11	1.60	32-6S	4.30	3.38	4.70	4.96	4.32
18-4S	1.15	.73	1.25	1.58	1.17	22-14S	2.09	1.85	2.21	2.72	2.40	32-6P	3.75	2.82	3.74	4.39	3.79
18-4P	1.23	.80	1.26	1.82	1.18	22-14P	2.35	1.77	2.82	2.89	2.35	32-7S	4.25	3.32	4.73	4.98	4.28
18-5S	1.11	.73	1.26	1.78	1.10	22-15S	2.08	1.50	2.55	2.61	2.10	32-7P	3.90	2.88	3.78	4.58	3.94
18-5P	1.19	.67	1.19	1.77	1.07	22-15P	1.58	1.07	1.74	2.16	1.64	32-8S	3.89	2.98	4.30	4.60	3.96
18-6S	1.15	.73	1.32	1.76	1.17	22-16S	1.97	1.40	2.44	2.53	2.00	32-8P	3.60	2.37	4.05	4.26	3.65
18-6P	1.10	.69	1.16	1.70	1.13	22-16P	1.74	1.20	2.24	2.30	1.76	32-9S	3.36	2.65	3.75	4.20	3.45
18-7S	1.34	.81	1.44	1.85	1.25	22-17S	1.65	1.32	1.85	2.35	1.70	32-9P	2.98	2.04	3.40	3.63	3.03
18-7P	1.15	.83	1.17	1.82	1.07	22-17P	1.77	1.23	2.04	2.33	1.80	32-10S	3.12	2.29	3.48	3.87	3.25
18-8S	1.48	1.18	1.60	2.00	1.60	22-18S	1.64	1.15	1.82	2.25	1.74	32-10P	2.49	1.14	2.84	3.23	2.69
18-8P	1.44	1.05	1.48	1.97	1.46	22-18P	1.57	1.00	2.10	2.11	1.56	32-16S	4.36	3.40	4.70	5.00	4.35
18-9S	1.60	1.37	1.95	2.76	1.43	22-19S	1.80	1.60	1.96	2.47	2.10	32-16P	3.77	2.84	4.24	4.40	3.83
18-9P	1.64	1.18	1.74	2.39	1.68	22-19P	1.66	1.38	2.44	2.50	1.97	32-20S	3.98	3.40	4.60	4.60	4.35
18-10S	1.60	.95	1.93	2.10	1.48	20-20S	1.54	1.23	1.70								

Reliance Specials

CAPACITORS POSTAGE STAMP MICAS

MMF	MMF	MMF	MMF	MMF	MFD	MFD
8.2	43	100	250	580	.0013	.0051
10	47	110	300	600	.00136	.006
15	50	120	330	620	.0015	.0062
20	51	125	350	680	.001625	.0065
22	56	130	370	750	.002	.0068
24	60	150	390	800	.0025	.007
25	62	160	400	820	.0026	.0075
30	75	175	430	910	.0027	.008
35	82	180	470	MFD	.003	.0082
39	85	200	500	.001	.0033	.01
40	90	220	510	.0011	.0047	
		240	560	.0012	.005	

Price Schedule
8.2 MMF to .0011 MFD 5¢
.0012 MFD to .002 MFD 7¢
.0023 MFD to .0082 MFD 12¢
.01 MFD 18¢

SILVER MICAS

MMF	MMF	MMF	MMF	MMF	MFD	MFD
10	51	120	270	470	815	.00282
18	60	125	325	488	820	.002826
22	62	130	330	500	875	.003
23	66	150	360	510	MFD	.0033
24	68	180	370	525	.001	.0039
30	75	200	390	560	.001625	.005
39	82	208	400	660	.0022	.0051
40	100	225	410	700	.0023	.0056
50	110	240	430	750	.0024	.006
	115	260	446		.0028	.0082

Price Schedule
10MMF to .0011MFD 10¢
.001625MFD to .0024MFD 12¢
.00282MFD to .0082MFD 50¢

OIL FILLED

MFD	V. D. C.	Price	MFD	V. D. C.	Price
.25	20,000	\$15.75	8	1,000	\$1.35
.03	16,000	1.95	4	1,000	1.15
.375 @	18,000 and	5.95	1	1,000	.80
.75 @	8,000	1.95	2	1,000	.85
.1	7,500	1.55	1	800	.39
.1-1	7,000	1.55	10	600	1.35
.01	6,000	.95	8	600	1.15
.03-.03	6,000	1.25	4	600	.79
.02-.02	7,000	1.25	2	600	.39
1	6,000	5.25			
2	5,000	3.95			
2	4,000	2.50			
2	3,000	2.15			
.25	3,000	1.10			
2	750 AC	.49			
8	2,000	3.95			
2	2,000	3.65			
2	2,500	1.95			
1	2,000	.95			

2 mfd
4,000
V.D.C.
G.E.
SPECIAL \$2.50

JONES BARRIER STRIPS

Type	Price	Type	Price	Type	Price
2-140Y	\$0.16	5-141 1/2 W	.30	3-142	.17
3-140 1/2 W	.17	6-141 Y	.30	3-142 Y	.23
5-140	.17	7-141	.29	6-142	.26
6-140	.20	7-141 1/2 W	.41	5-142 1/2 W	.67
9-140 1/2 W	.40	8-141 1/2 W	.47	10-142 1/2 W	.71
10-140 1/2 W	.44	9-141 Y	.52	11-142 Y	.78
2-141	.19	10-141 Y	.58	2-150 1/2 W	.38
3-141 1/2 W	.19	10-141 Y	.58	3-150	.44
3-141 W	.19	13-141 1/2 W	.74	4-150	.57
4-141 W	.25	17-141 Y	.96		
4-141 1/2 W	.25				
5-141	.22				

METERS

	Price
0-1 Amp. R.F.	3.29
0-300 V.D.C.	3.50
0-80 Amp. D.C.	2.25
0-7.5 V. A. C.	3.46

VERNIER DRUM (From BC-221)

0-50 in 180°. Black with silver marks. \$85¢

VERNIER DIAL (From BC-221)

2 5/8" Dia. 0-100 in 360°. Black with silver marks. Has thumblock. \$85¢

BLOWER & MOTOR

Blower #12, motor 27 1/2" V.D.C., 1/100 H.P., 8,500 R.P.M. Continuous duty. Has mounting brackets. Navy inspected. \$3.50

GEAR ASSORTMENT

100 small assorted gears. Most are stainless steel or brass. Experimenters dream! Only \$6.50

WIRE WOUND PRECISION RESISTORS 1% OR BETTER

1/4 WATT—25c		1/2 WATT—25c		1 WATT—30c	
6.68Ω	12.32Ω	16.37Ω	125Ω	414.3Ω	9,000Ω
10.48	13.02	62.54	147.5	705	14,825
10.84	13.52	79.81	220.4	2193	600,000Ω
11.25	13.89	105.8	301.8	59,148	700,000Ω
11.74	14.98	123.8	366.6	100,000	700,000Ω

1 WATT—40c		1 Megohm—1 Watt 1%—65c; 5%—40c	
100,000Ω	128,000Ω	320,000Ω	600,000Ω
120,000Ω	130,000Ω	522,000Ω	700,000Ω

Orders for 100 precision resistors—10% Discount



UNIVERSAL JOINT
3/16" hole x 3/8" O.D.
1 1/8" long
Steel or Aluminum
50¢

FILAMENT TRANSFORMERS

Pri. 115 V., 60 Cyc.—Sec. 5V., 115A. 6000 volt insulation to 9250 core. \$9.95 each
Pri., 115V., 60 Cyc.—Secondary: 6 V. @ 35 A.
12 V. @ 18 A. \$5.95
24 V. @ 9 A.

PULSE TRANSFORMERS

X 124 T2. UTAH, marked 9262, 9340, small gray case. Ratio 1:1:1; hypersil core. \$2.75
D161310, 50 Kc to 4 Mc. 1 1/2" dia. x 1 1/2" high. 120 to 2350 ohms. \$1.50
352-7178—Spec. 10, 111 Chicago Trans. equivalent to 9250 (above). \$1.50
RS9802, Ratio, 1:1:1, 2:1, Freq. range 380 to 520 C.P.S. \$1.50
D106173. W.E. Freq. resp. 10Kc to 2 MC. \$3.50
800 KVA G.E. #2731, 25,000 Volt peak output. \$9.80
Bifilar: one microsecond pulse width. \$28.50

PRECISION CONTROLS

6 WATT	4 WATT		
20,000Ω Muter 314A	1.70	500Ω Centralab 48-501	\$1.00
6,000Ω De jur 260	1.70	200Ω GR 301	1.25
6,000Ω Muter 314A	1.70	20Ω De jur 292	1.00
5,000Ω Muter 314A	2.50	12Ω GR 301	1.10
2,000Ω De jur 260	1.70	12Ω De jur 292	1.00
10,000Ω De jur 271T	\$2.00	2Ω GR 301	1.25
10,000Ω Muter 471A	2.00		
5,000Ω De jur 271T	2.00		

PRECISION CAPACITOR—W.E.

D-161270. 1 mfd @ 200 VDC; -40° to +65°C. \$8.50

SELENIUM RECTIFIERS

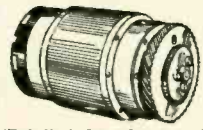
Full Wave—200 ma., 115 V. \$1.57
Half Wave—100 ma., 115 V. .72

TIME DELAY RELAY

Raytheon CPX 24166 KS 10193-60 Sec. • 115 V., 60 Cycle • Adj. 50-70 Seconds • 2 1/2 second recycling time—spring return • Micro-switch contact, 10A • Holds ON as long as power is applied • Fully cased • ONLY \$6.50

SELSYNS


115 V., 60 Cyc.
#C78248
3 3/8" dia. x 5 1/2" long
\$8.95 pair



Mounting Brackets — (Bakelite) for selsyns, and differentials shown above. 35¢ pair

DIFFERENTIAL

115 V., 60 Cyc.
#C78249
3 3/8" dia. x 5 1/2" long
\$2.95 ea.



Used between two #C78248's as dampener. Can be converted to 3600 RPM Motor in 10 minutes. Conversion sheet supplied. (Converted) \$3.50


COAXIAL CABLES

GUARANTEED!! NEW!!

	Price per Ohms, 1,000 ft		Price per Ohms, 1,000 ft
RG-5/U	53.5	RG-29/U*	53.5
RG-6/U	76	RG-34/U	71
RG-7/U*	97.5	RG-35/U	71
RG-9/U*	51	RG-37/U	55
RG-10/U	52	RG-39/U	72.5
RG-13/U*	74	RG-41/U	67.5
RG-15/U	76	RG-54/U	58
RG-18/U	62	RG-56/AU	54
RG-21/U	53	RG-56/U	53.5
RG-22/U*	95	RG-57/U*	95
RG-24/U	125	RG-58/U	53.5
RG-25/U	48	RG-74/U	52
RG-26/U	48	RG-77/U*	48
RG-27/U	48	RG-78/U	48
RG-28/U	160		80

*No minimum order—others 250' minimum
Add 25% for orders less than 1,000 feet

COAXIAL CABLE CONNECTORS



Angle Adapter 15¢
M-359 83-IAP

Plug 40¢
PL-259A 83-ISP

Socket 35¢
SO-239 83-IR

Hood 9¢
83-IH

Adapter for PL-259 A for use on small coax. \$10.00 per 100
12¢ each

83-1AC	\$0.42	UG-19/U	.73	UG-85/U	.88
83-1F	1.12	UG-21/U	.67	UG-87/U	.79
83-1P	.80	UG-22/U	1.10	UG-103/U	.48
83-1SP	.45	UG-23/U	.85	UG-104/U	.85
83-1T	1.12	UG-24/U	.67	UG-167/U	2.00
83-22AP	1.10	UG-25/U	.60	UG-167/U	1.33
83-22F	1.48	UG-27/U	.68	UG-175/U	.15
83-22R	.48	UG-28/U	.83	UG-176/U	.15
83-168	.15	UG-30/U	1.20	UG-197/U	1.33
83-186	.15	UG-31/U	14.80	UG-206/U	.63
UG-7/AP	2.14	UG-34/U	12.80	UG-255/U	1.22
UG-12/U	.63	UG-36/U	12.80	UG-284/U	1.74
UG-13/U	.63	UG-37/U	12.80	UG-281/U	.60
UG-18/U	.63	UG-58/U	.63		

SOUND POWERED HANDSET

Brand New!
Includes 6 ft. cord. No batteries or external power source used.
\$8.92 ea. \$17.60 pr.

CERAMICONS

2 NMF	30 MMF	500 VOLT CERAMIC CONDENSERS			
5.6	35	MNF	MMF	MMF	MMF
10	35	2	35	56	150
12	45	2	34.4	62	180
15	62	4.7	27	68	200
20	82	8	30	82	220
22	150	12	33	91	270
	200	15	40	100	300
		16	47	140	1000

\$6.50 per hundred \$5.50 per hundred

2J1G1 SELSYNS

BRAND NEW
400 Cycle
Can be used on 60 cycle
\$1.85



3AG FUSES

AMP	Per 100	AMP	Per 100	AMP	Per 100
1/8	\$4.00	1 1/2	\$3.00	5	\$3.00
1/4	4.00	2	3.00	10	3.00
3/8	4.00	3	3.00	15	3.00
1/2	4.00	4	3.00	20	3.00

Fuse Holder—for 3AG Fuse. (Littlefuse or Buss) .25¢

4AG FUSES

AMP	Per 100	AMP	Per 100	AMP	Per 100
1/10	\$4.00	2	\$2.00	10	\$2.50
1/4	3.50	3	2.00	15	2.50
1/2	3.50	4	2.00	20	2.50
1	2.00	5	2.00	25	2.50

Fuse Holder—for 4AG Fuse. (Littlefuse or Buss) .18¢

Wrapped—BALL BEARINGS—New

Mfg	ID	OD	Width	Price
Fafnir 33K5	3/16"	1/2"	5/32"	\$0.25
MRC 205R	63/64"	2 3/64"	19/32"	1.10
N.D. 5202C13M	1/2"	1 3/8"	1 1/8"	1.00
Fafnir 7308W	1 37/64"	3 9/16"	5/16"	2.00
SKF466430	6"	8"	1"	5.00
TIMKEN	4 5/16"	6 1/4"	29/32"	4.25

NEEDLE BEARINGS

B108 1/2" wide	5/8"	13/16"	30¢
GB34X 1/4" wide	3/16"	11/32"	25¢

ALLEN SET SCREWS

4-40 x 1/8	8-32 x 1/8	8-32 x 5/16
4-40 x 3/16		8-32 x 3/8
ALL SIZES		\$1.50 per 100

HAYDON TIMING MOTOR

4 R.P.M., 115 V., 60 Cycle. \$1.79



DELAY NETWORK—ALL 1400Ω

T 113—Approx. 1.2 micro sec. delay 85¢
T 114—Approx. 2.2 micro. sec. delay 85¢
T 115—Similar to T 114 with tap brought out. 85¢

CHOKES

30 Hy., 8 ma. \$1.29
6 Hy., 8 ma. \$1.29

Get On Our Mailing List! Minimum Orders \$3. All orders f.o.b. PHILA. PA.

RELIANCE MERCHANDIZING CO.

Arch St. Cor. Croskey Phila. 3, Pa. Telephone RIttenhouse 6-4927

1000 KC crystal BT cut.....\$3.95
3" scope shield..... 1.29
2 speed dial drive for 1/4" shaft ratios 5:1 1 to 1 .39
ATC 100 mmdf air trimmer screwdriver shaft..... .29
Sigma 8em. Relay 8000 ohms..... 1.98
Centralab 850 S 50MMF 5KV BUTON COND..... .39
500 watt 12.5 ohm power rheostat..... 3.49



50 mmdf 5 KV vacuum condenser.....\$1.49
6v, 12v vibrators any type..... .98
Rotary switch Mycalex, 2 deck SP3T..... .39
1 mfd 5000v oil condenser..... 2.98
2 mfd 3000v oil condenser..... 3.25
3 mfd 4000v oil condenser..... 3.95
24 mfd 1500v DC 3KV flash. Excellent for speed lamp..... 3.95

TUBES!! BRAND NEW! STANDARD BRANDS! NO SECONDS! COMPARE! TUBES!!

Table listing various vacuum tube types and their prices, including categories like 6X4, 6X5, 6X6, etc.

SELENIUM RECTIFIERS FULL WAVE BRIDGE TYPE

Table of selenium rectifier specifications including input/output voltage, current, and price.

CENTER TAPPED RECTIFIERS Single Phase Full Wave Bridge

Table of center tapped rectifier specifications including input/output voltage, current, and price.

TRANSFORMERS—115V 60 CY HI-VOLTAGE INSULATION

Table of transformer specifications for 115V 60 cycle, including primary/secondary voltages and current ratings.

TRANSFORMERS—220v 60 Cyc

Table of transformer specifications for 220V 60 cycle, including primary/secondary voltages and current ratings.

EQUIPMENT SPECIALS

Table of equipment specials including ATR Inverter, AN/CRW-2 UHF Receiver, BC433 Receiver, etc.

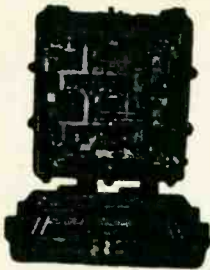
FILTER CHOKES HI V INS

Table of filter choke specifications including inductance, voltage, and price.

RADIO HAM SHACK Inc. 189 GREENWICH STREET, NEW YORK, N. Y. Includes contact information and a note about price changes.

IMMEDIATE DELIVERY • LOW PRICES • FULLY GUARANTEED

BROWN TELEPLOTTER RECEIVER



Model 791X1R
115 volt 60 cycles

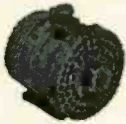
Contains a pen driven by two balancing motors which writes on rear of a translucent chart. Pen arm position is in terms of two coordinates supplied balancing motors thru two amplifiers. Originally intended for recording plotted or written data from central plotting board. Writes at one half scale on 18 in. chart. Discriminator input circuit designed to operate unit as function of two varying R.F. frequencies varying about mean of approx. 430 KC. Further data on request. (Shipping weight 435 lbs.)

Price \$375.00



Aircraft Generator Eclipse NEA-3

Output 115 VAC; 10.4 amps 800 cycles at 2400 rpm. Also 30 VDC at 6 amps. Stock #SA-306. Price \$39.50 each.



400 Cycle Generator

G. E. 5ASBS1JJ3. 400 cycles out at 115 volts 7.2 amps, ideal for lab. 6" lg. x 6" diam. 8000 rpm. Stock #SA-292. Price \$79.50 ea.



A-5 Autopilot Indicator

Autosyn Type Pilot Indicator for A-5 Autopilot. 26 v. 400 cycles. Stock #SA-299. Price \$12.50 each.



Pioneer Servo Motor

Type 10047-2A. 2 ϕ 400 cycle low inertia. 26 v fixed phase. 45 v. max. variable phase. Stock #SA-90. Price \$12.50 each.



PRECISION AUTOSYN

Pioneer Type AY-150 Control Autosyn. Precision type. 26 v. 400 cycle. Stock #SA-297. Special low price \$14.50 each.

SYNCHROS

Navy Types

1G, 1CT, 5G, 5CT, 5DG, 5HCT, 5SF, 5HSF, 5SDG, 6DG, 7G, etc.

Prices on Request



Prices F.O.B. Paterson
Phone ARmory 4-3366
WRITE FOR LISTING



Compass Indicator
I-82F Compass Indicator. 0-360°-5 in. dial. 26 v. 400 cy. 8-12 v. 60 cy. Ideal position indicator. Stock #SA-284. Price \$6.50 each



SWEEP GENERATOR CAPACITOR

Hi-speed bearings. Split stator. Silver-plated coaxial type. 5-10 mmf.

Stock #SA-167

Price \$2.75 each

ALSO IN STOCK

C-1 AUTOPILOT COMPONENTS
A-5 AUTOPILOT GYROS
GENERAL ELECTRIC D-C SELSYNS
AC and DC RATE GENERATORS

400 CYCLE AC BLOWERS

E. A. D. J-151—115 v. 400 cy. 22 c.f.m.
Westinghouse Type FI—115 v. 400 cy. 17 c.f.m.

DC MOTORS

Haydon-0666, 1/2 rpm. 29 v. d-c, 100 ma.
Delco 5069625—120 rpm. Gov. cont. 27 v. field. Arm. v. 60. Amplyduty controlled.
Delco-A-7165—1/30 hp. 3600 rpm. Gov. cont.

W. E. KS-5603-LO2—1/100 hp. 4 lead shunt.
National Mineral—90600. 1 hp. Int. duty. Fan cooled.

Diehl FDE-53-5—3600 rpm. Gov. cont. 1/30 hp.
G. E. 5BA25MJ409—24 v. 7500 rpm. Cont. duty.

Airsearch—Actuator—25800-24. 2" travel.
Barber—Colman—Actuator—YLc-2066-2. 200 in/lb. 135 degrees in 45 seconds.
Airsearch—Actuator (Manual Flap) 25080.
Airsearch—Actuator—(Automatic Flap) 25040.

Holtzer Cabot—RBD-2220—1/2 hp. 27 v. 3600 rpm.
Arma Latitude Motor — 8413-30 (Step motor)

Ellnco B-64—1/165 hp. 3100 rpm. 27 v. f. 80 v. armature. (Thyratron control)
John Oster—A-21E-12R—Split field series reversible. 28 v. 0.4 amps. 2 watts output.
General Electric 5PS56HC18 — Split field series rev. 60 v. 1.4 A. 5500 rpm.

AC SERVO MOTORS

Kollsman—776-01—400 cy. 2 ϕ drag cup type.

Diehl FP-25-3—2 ϕ 60 cy. 20 v. 2.5 watts out.

Pioneer CK-2—2 ϕ 400 cy. 1.05 in/oz. stall.

Pioneer CK-17—2 ϕ 400 cy.

Minneapolis Honeywell G303AY2CA4. Built in gear reduction. 2 ϕ 400 cy.

AUTOSYNS (Pioneer)

B-9A—Dual Oil Pressure Indicator (6007-4F-7A)

B-9A—Oil Pressure Transmitter, (4150-3B3)

Pioneer Types—AY-1, AY-14, AY-54, 2320, etc.

C-14A—Fuel Pressure Transmitter.
Pioneer I-81A and I-82A Compass Indicators.

Subfractional Horsepower AC Motors

Eastern Air Devices—J-72B—115 v. 400 cy. 1/50 hp. Cont. duty. 4700 rpm.

E. A. D. J-49B—115 v. 400 cy. 1/250 hp.

E. A. D. J-33—115 v. 3 ϕ 400 cy. Int. duty.

Diehl FBF-24-1—115 v. 400 cy. 1/100 hp.

Synchro-600—110 v. 60 cy. 1 rpm.

Haydon 36228—115 v. 60 cy. 1 rpm.

MAGNESYNS

Pioneer Type CL-3, 6 power.

Pioneer 1006-1E-B1 Indicator. AN-5730-2.

INVERTERS



Wincharger PU-7/AP
Input 28 VDC at 160 amps. Output 115 v. 400 cy. 1 ϕ at 2500 VA. Voltage and frequency regulated. Cont. duty. Stock #SA-164. Price \$89.50 each.



G.E. 5AS181N3 (FE-118)
Input 28 VDC at 100 amps. Output 115 v. 400 cy. 1 ϕ at 1500 VA. PF 0.8 W.E. Spec. K6-5601L1. Stock #SA-286. Price \$29.50 ea.



FE-218E Inverters

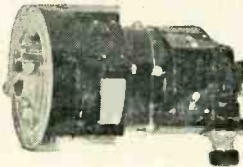
Russel Electric and Leland. Input 28 VDC at 93 amp. Output 115 v. 400 cycles at 1500 VA. PF 0.9. Stock #SA-112A. Price \$49.50 each.



Pioneer 12130-4-B

Input 28 VDC at 14 amps. Output 120 v. 400 cy. Single Phase at 1.15 amps. (140 VA.) Voltage and frequency regulated. Made 1948. Stock #SA-304. Price \$89.50 each.

JACK AND HEINTZ STARTER



Dwg. 6-950-E Aircraft engine starter. 28 VDC. Stock #SA-305. Price \$19.50 each

DC SERVO MOTOR



Ellnco Type B-64. 1/165 hp at 3100 rpm. Field volts 27.5 Max. armature voltage 80. Ideal for thyratron servo control. Stock #SA-211. Price \$12.50 each.

MAGNETIC AMPLIFIER ASSEMBLY

Sperry 661824. Saturable reactor type output transformer. Designed to supply one phase of 400 cycle servo motor. Stock #SA-266. Price \$6.75 each

FORD INS'T SERVO MOTOR



115 volt 60 cycle two phase low inertia motor. 15 watts output. BuOrd. 207927. Stock #SA-291. Price \$49.50 each.

Servo-Tek products co.
4 Godwin Ave. Paterson, N. J.

SPECIALISTS IN FRACTIONAL HORSE POWER MOTOR SPEED CONTROL

MICROWAVE RECEIVERS

AN/APR-1 Receivers and tuning units TN-1 (38 to 95 MC) TN-2 (76-300 MC) TN-3 (300-1000 MC)
 AN/APR-4 Receivers and tuning units TN-16 (38-95 MC) TN-17 (76-300 MC) TN-18 (300-1000MC)
 AN/APR-5A Receivers. 1000 to 6000 MC Range.

**U. S. NAVY
 SOUND POWERED BATTLE
 PHONES**

Western Electric No. D173312, Type O. Combination headset and chest microphone. Brand new including 20 ft. of rubber covered cable.....\$17.50
 Automatic Elec. Co. No. G1A43A0. Similar to above but including Throat microphone in addition to chest microphone. Brand new with 20 ft. rubber covered cable.....\$13.50
 U. S. Instrument Co. Navy Type M. Dr. No. A-260 A.I.T. 1. Complete with 20' cable and navy plug. Brand new.....\$17.50

G. E. SERVO AMPLIFIER

Type 2CV1C1 Aircraft Amplidyne control amplifier. 115 volts—400 cycles. Dual channel. Employs 2-6SN7GT and 4-6V6GT tubes. Supplied less tubes. New.....\$22.50

400 CYCLE TRANSFORMERS

AUTO. 400 cy. G.E. Cat No. 80G184
 KVA .945S—520P. Volts 460/345/230/115. New \$4.95
 FILAMENT. 400/2600 cy. Input: 0/75/80/85/105/115/125V. Output: 5V3A/5V3A/5V3A/5V3A/5V6A/5V8A/6.3V6A/6.35A. New.....\$2.95
 THYRATRON POWER. 400/1600 cy. Raytheon UX-8876. 400/1600 cy. Pri: 115. Sec: 50-0-50V at 0.5A, 6.3V at 1.2A. Test r.m.s. 1780. New.....\$2.75
 PLATE WECO KS9560. 400/800 cy. Pri: 115V. Sec: 1350-0-1350 at .057A (2700 V Total). Elestat shided. Wt. 2.3 lbs. New.....\$2.95
 SCOPE PL. & FIL. WECO 9556. 400/2400 cy. Pri: 115. HV. Wdg. 1125V at .008A. Fil. Wdgs. 6.4V4A/2.5V1.75A/6.4V.6A. Elestat shided. Wt. 1.4 lbs. New.....\$2.75
 FILAMENT. 400/2400 cps. WECO KS9553. Pri: 115V. Sec: 8.2V1.25A/6.35V1.5A Elestat shided. Wt. 0.5 lbs. New.....\$1.95
 PLATE & FIL. 400/2600 cy. Pri: 0/80/115V. Sec #1=1200VDC at 1.5MA, Sec #2=400VDC at 130MA. Fil. Sec: 6.4V4.3A/6.35V0.8A. (Ins. 1500V)/5V2A/5V2A. New.....\$4.95
 RETARD. 400 cy. WECO KS9598. 4 Henry 100MA \$1.75

60 CYCLE TRANSFORMERS

50KVA STEPDOWN. Standard Trans Corp. Navy type MD. Pri: 450V111A. Sec: 117V427A. Navy type. Ambient temp. 50 Deg. C.....\$125.00
 FILAMENT. Raytheon Hypersil Core. Pri: 115V. Sec: 6.3V22A/6.3V2.4A/6.3V2.25A/6.3V0.6A Ins. for 1700V.....\$5.95
 Plate. Thordarson #T46889. 1650 VA. Pri: 105-120V. 60 cy. 1 PH. Sec: 5600V. Center tapped. 7.5kV insulation. Brand new.....\$49.50
 High Reactance Trans. G. E. type Y-3502A.—60 cy. Voltage 11200-135. Inductance H.V. Windings 135 Henries. Output Peak Voltage 22.8KV. Cat. 83180C5G1. New.....\$89.50

PULSE TRANSFORMERS

PULSE. WECO KS-9563. Supplies voltage peaks of 3500V from 807 tube. Tested at 2000 Pulses/sec and 5000V peak. Wdg. 1-2=18 ohms. Wdg. 1-3=72 ohms. 1. of Wdg. 1-3=.073-.0821 at 100 cps.....\$5.50
 PULSE. WECO KS-161310. 80 KC. to 4MC. 1 1/2" Dia. x 1 7/8" high. 120 to 2350 ohms. New.....\$3.95

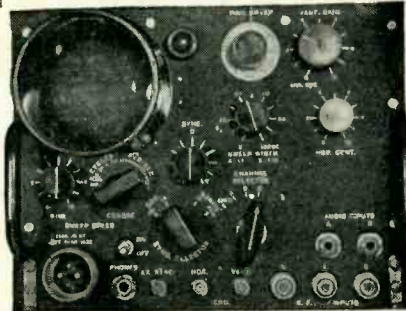
HIGH VOLTAGE CAPACITORS

.25 MFD., 20KV.....\$17.75
 .25 MFD., 15KV.....15.75
 .5 MFD., 25KV.....\$26.50
 1 MFD., 15KV.....\$18.50
 1 MFD., 7.5KV.....\$ 7.95

All brand new. Made by prominent manufacturers.

All prices indicated are F O B Bronxville, New York. Shipments will be made via Railway Express unless other instructions issued.

**MODEL AN/APA-10
 PANORAMIC ADAPTER**



Provides 4 Types of Presentations:
 (1) Panoramic (2) Aural
 (3) Oscillographic (4) Oscilloscopic

Designed for use with receiving equipment AN/ARR-7, AN/ARR-5, AN/APR-4, SCR-587 or any receiver with I. F. of 455kc. 5.2mc. or 30mc.

SUMMARY OF CHARACTERISTICS:

SENSITIVITY: "A" channel, 400 microvolts or less per 1/4" beam deflection. "B" channel, 400 microvolts or less per 1/4" beam deflection. "C" channel, 1 volt or less per 1/4" beam deflection.
 RESOLUTION: 12 kilocycles at 3 db down from peak. sweep control at maximum, using CW signal.
 PRESENTATION: Panoramic ("A" & "B" channels); Oscillographic, "C" channel.
 SWEEP WIDTH: Channel A, ± 50kc (100 kc overall) Channel B, ± 500 kc (1 Mc overall) Channel C, ± 1 Mc (2 Mc overall)
 CATHODE RAY SWEEP: Oscillatory or non-oscillatory (Servo) Variable Sawtooth Generator, 35 to 40,000 cycles per second.
 AUDIO OUTPUT: 50 milliwatts into 600 or 800 ohm load.
 VERTICAL AMPLIFIER: Single stage, ± 2db from 30 cycles to 100 kc or higher. Amplifier out position permits direct connection to one vertical plate through coupling capacitor.
 HORIZONTAL AMPLIFIER: Single stage, ± 2db from 30 cycles to 100 kc. No provision for direct connection to deflection plates.
 CATHODE RAY TUBE VOLTAGE: Cathode to accelerating anode; 1200V DC for 115V A.C. input.
 SENSITIVITY OF CATHODE RAY OSCILLOSCOPE: Maximum through Amplifier. Horizontal: 10 volts peak to peak per inch. Vertical: 1.5 volts peak to peak per inch.
 DIRECT TO VERTICAL PLATE: 150 volts peak to peak per inch.
 NOISE: No disturbance in excess of 25,000 microvolts between 200kc to 200Mc generated by equipment. Overall Dimensions: 19-9/16" x 10 1/4" x 7 7/8" Weight: 40 lbs.
 Power Requirements: 115V. A.C. 60 cycles, 1 phase. With 21 tubes including 3" scope tube, for operation on 115 V. 60 cycle source. PRICE.....\$245.00
 AN/APA-10 80 Page Tech Manual.....\$2.75



**LINEAR SAWTOOTH
 POTENTIOMETER
 W.E. KS-15138**

Has continuous resistance winding to which 24 volts D.C. is fed to two fixed taps 180° apart. Two rotating brushes 180° apart take off linear sawtooth wave voltage at output.
 Brand New \$5.50

**LAVOIE FREQ. METER
 375 to 725 MCS**

Model TS-127/U is a compact, self-contained, precision (± 1 MC) frequency meter which provides quick, accurate readings. Requires a standard 1.5V "A" and 45V "B" battery. Has 0-15 minute time switch. Contains sturdily constructed HI-"Q" resonator with average "Q" of 3000 working directly into detector tube. Uses 957, L56 and 3S4 Tubes. Complete, new with inst. book, probe and spare kit of tubes. Less batteries. Write for descriptive circular.....\$69.50

PLEASE NOTE OUR
 NEW ADDRESS



PARABOLOIDS

Spun Magnesium dishes 17 1/2" dia., 4" deep. Mounting brackets for elevation and azimuth control on rear. 1 1/2" x 1 3/8" opening in center for dipole. Brand new per pair.....\$8.75

SWEEP GENERATOR CAPACITOR

High speed ball bearings. Split stator silver plated coaxial type 5/10 mmfd. Brand new.....\$2.50

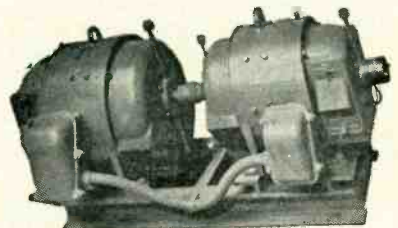
RAYTHEON VOLTAGE REGULATOR

Adj. input taps 95-130V., 60 cy. 1 1/2" Output: 115V., 60 Watts, 1/2 of 1% Reg. Wt. 20 lbs. 6 3/4" H x 8 3/4" L x 4 3/4" W. Overload protected. Sturdily constructed. Tropicalized. Special.....\$14.75

**Synchro Differential
 Generator**

Ford Inst. Co. Type 5SDG. Brand New.....\$22.50

**MOTOR GENERATORS
 DYNAMOTORS, INVERTERS, ETC.**



2.5 KVA MG SET. Diehl Elec. Co. 120V DC to 120V AC, 60 cy. 1 Ph. Complete with Magnetic Controller, 2 Field Rheos and Full Set of Spare Parts including Spare Armatures for Generator and Motor. Full specs. on request. New.....\$285.00

2 KVA MG SET. O'Keefe and Merrill. 115V DC to 120V AC, 50 cy. Idles as 3 Ph. synch motor on 208V, 50 cy. New. Export crated...\$165.00
 MG SET FOR NAVY TBS TRANSMITTER. Type CG-21302. 440V AC, 60 cy. 3 Ph. 1500 VA to 875V DC and 300V DC. New.....\$69.50

DYNAMOTOR. Navy Type CAJO-211444. 105/130V-DC to 13V DC at 46A or 26V DC at 20A. Radio filtered. Complete with Line Switch. New.....\$69.50

DYNAMOTOR. Eacor. 32V DC to 110V AC, 60 cy. 1 Ph. 2.04 Amps. New.....\$24.50
 Also available for 64 volts input. Same price.

DYNAMOTOR. Eacor. 32V DC to 110V AC, 60 cy. 1 Ph. 0.43 Amps. New.....\$17.50

AMPLIDYNE—G. E. Model 5AM31N19A. 530 Watts. 7500 R.P.M. Input: 27V DC. Output: 60V. DC. Weight 3 1/2 lbs. New.....\$16.50

AMPLIDYNE—G. E. Model 5AM21J7. 4600 R.P.M. Motor Compound wound. 150 Watts. Input: 27V. DC. Output: 60V. DC Sig. Corps. U. S. Army MG-27-B. New.....\$26.50

AMPLIDYNE—Edison type 5AM31N18A. Input: 27 volts 44 Amps., 8300 RPM. Output: 60V DC at 8.8 amps. 530 Watts. New.....\$26.50

INVERTER—Leland Elec. Co. Model PE206A. Input: 28V. DC, 38 Amps. Output: 80V., 800 cy. 485 VA. New.....\$17.50

INVERTER—G. E. Model 5D-21N33A. Input: 24V. DC. Output: 115V. 400 cy. 485 Va. New.....\$24.50

PE 218 INVERTER—G. E. J8169172. Input: 28V. DC. Output: 115V, 400 cycles at 1.5 KVA.....\$50.00

D. C. MOTOR—G. E. Model 5BA 50LJ2A 0.5 HP. Armature 27V. at 8.3 Amps. Field: 60V. at 2.3 Amps. R.P.M. 400. New.....\$16.75

DYNAMOTOR—Type PE94C. For use with SCR522 Transmitter-Receiver. Brand new in export cases.....\$9.50

Radar Antennas in stock. Types SO-1, SO-3, SO-13. Brand New.

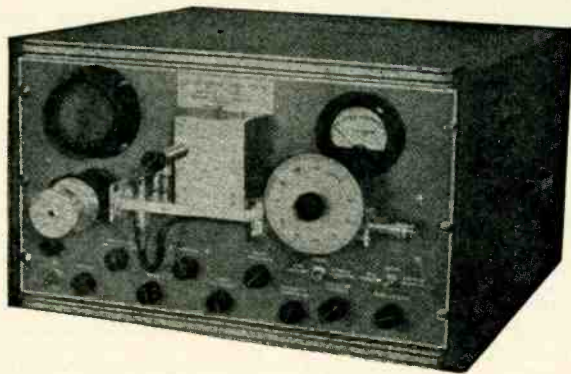
**ELECTRONICRAFT
 INC.**

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 PHONE: BRONXVILLE 2-0044

All merchandise guaranteed. Immediate delivery, subject to prior sale.

All Prices Subject to Change Without Notice

TEST EQUIPMENT



- X Band Spectrum Analyzer 8500-9600 Mc., calibrated linear below cut-off attenuator, calibrated frequency meter, tuned mixer, 4 i.f. stages, 3 video stages overall gain 125 db., regulated power supply.
- S Band Spectrum Analyzer 2700-3900 Mc., similar to above.
- X Band Test Load low power low power \$20.00
- X Band Below Cut-Off Wave Guide Attenuator, with calibrated dial, type N input connector, output connects to 1/2" x 1" wave guide.....\$55.00
- X Band Test Load, low power....\$15.00
- TS-62 X Band Echo Box with r.f. cable and pick-up antenna.
- TS-33 X Band Frequency Meter, 8500-9600 Mcs. Crystal detector and 50 micro-amp. meter. Indicates Resonance. Connection for scope available.
- TS-45A-APM-3 Signal Generator, 8700-9500 mc., 110 V. 60-800 cps.
- TS-35/AP X Band Signal Generator, pulsed, calibrated power meter, frequency meter, 8700-9500 mc.
- 30 MC I.F. STRIP, VIDEO, and AUDIO AMPLIFIER AND 110 Volt 60-2600 cps POWER SUPPLY, Bandwidth 10 mc, new, part of SPR-2 Receiver.
- AMPLIFIER STRIP AM-SSA/SPR-2 contains I. F. amplifier, detector, video amplifier, pulse stretcher and audio amplifier and Rectifier Power Unit PP-155A/SPR-2 bandwidth 10 mc, center frequency 30 mc, sensitivity 50 microvolts for 10 milliwatts output. Power supply 80/115 V ac, 60-2600 cps 1.3 amps.\$65.00 less tubes
- X Band Test Load, 50 watts, average power 1/2" x 1" waveguide. Sand load TS 108.....\$35.00
- HI POWER X BAND TEST LOAD, dissipates 280 watts of average power for 3/8" x 1/4" waveguide, VSWR less than 1.15 between 7 and 10 KMC \$150.00
- S Band Signal Generator Cavity With Cut-Off Attenuator, 2300-2950 mc., 2C40 tube, with modulator chassis \$30.00
- High Pass Filter F-29/SPR-2, cuts off at 1000 mc. and below; used for receivers above 1000 mc.....\$12.00
- UPN-1 S Band Beacon Receiver-Transmitter\$75.00
- S Band Test Load TPS-55P/BT, 50 ohms \$12.00
- High Pass Filter F-29/SPR-2, cuts off at 1000 mc and below; used for receivers above 1000 mc.....\$12.00
- TS-125 CALIBRATED S BAND POWER METER with attenuator.
- TS-155 S BAND SIGNAL GENERATOR and Power Meter.
- S Band Mixer, tunable by means of slider, type N connector for the R. F. and local oscillator input, U.H.F. connector for the I.F. output, variable oscillator injection\$30.00
- TS-110 S Band Echo Box 2400-2700 mc, portable\$110.00
- HI POWER S BAND TEST LOAD, dissipates 1000 watts of average power, for 1 1/2" x 3" waveguide. Range 2500 to 3700 MC.
- X Band Thermistor Mounts, VSWR less than 1.4 8500-9600 MC Fixed triple tuned, 1/2"x1" waveguide.....\$40.00
Fixed triple tuned 3/8"x1 1/4" waveguide\$50.00
- Frequency Meter, 8500-9600, variable, absorption type for either 1/2"x1" or 3/8"x1 1/4" waveguide, with calibration, ± 4 MC, precision ground thread.\$150.00
- X Band Crystal Mount, 1/2"x1" waveguide\$25.00
- X Band Attenuator, double van type, VSWR less than 1.4, 8500-9600 MC 0-30db, calibrated for 1 1/4"x3/8" waveguide\$80.00
1/2"x1" to 3/8"x1 1/4" adapter, UG80/U \$5.00
- TS-203/AP CALIBRATED SELSYN..\$10.00
- GENERAL RADIO PRECISION WAVE-METER TYPE 724A, range 16 kc to 50 mc, 0.25% accuracy, V.T.V.M. reso-

- nance indicator, complete with accessories and carrying case NEW...\$175.00
- HEWLETT-PACKARD-AUDIO SIGNAL GENERATOR 205A.....\$230.00
- RADIO RECEIVER BC-967T2, 18-160 mc, 3 bands FM/AM, 110 V, 60 cps.\$200.00
- RADIO RECEIVER BC-969-B, 15-150 kc. \$150.00
- RADAR RECEIVER BC-1068A, 150-210 mc., individual tuning for r.f. stages, bandwidth 4 mc., 115 v. 60 cy.....\$30.00
- MEASUREMENTS 78E, 50-75 mc, calibrated output.....\$100.00
- ESTERLINE Angus recording Milliammeter 60 cycles, AC.....\$150.00
- FERRIS MODEL, 10B SIGNAL GENERATOR, 85 kc to 25 mc, calibrated output, good working order.....\$100.00
- TS-184 Echo Box and Attenuator for APS-13.
- TS-226 Peak Power Meter for APS-13.
- TS-89 Voltage Divider for measuring high video pulses, ratios 1:10 and 1:100 transmission flat within 2 db 150 c.p.s. to 5 mc., with cable for attaching to syndroscope.
- Waveguide Below Cut-off Attenuator L 101-A U.H.F. Connectors at each end calibration 30-100 db.....\$10.00
- FIXED ATTENUATOR PADS, 20 db ±0.2 db DC-1200 mc, 50 ohms, VSWR 1.3 or less, 2 watts average power...\$30.00
- WAVEGUIDE BELOW CUT-OFF ATTENUATOR same as above except input is matched in range of 2200-3300 mc. VSWR less than 1.2.....\$54.00
- PULSE TRANSFORMER 132-AWP...\$8.00
- PULSE TRANSFORMER GE 69G, 828 G-1 \$6.00
- HYPERSIL CORE CHOKE, 1 Henry, Westinghouse L-422031 or L 422-32....\$3.00
- PULSE FORMING NETWORK, 20 kv., .92 micro-second, 50 ohms, 800 p.p.s.\$40.00
- PULSE INPUT TRANSFORMER, permalloy core, 50 to 4000 kc., WE-D161310, impedance ratio 120 to 2350 ohms..\$3.00
- TRANSFORMERS, 115 volts, 60 cps primaries:
1. 6250, 3250 and 200 volts, tapped primary voltage doubler, 12.5 kv. ins.\$14.00
 2. 6250 volts 60 ma. G.E. voltage doubler, 12.5 kv. ins.....\$12.00
 3. 2 secondaries at 500 volts 5 amps each, at 210 pounds.....\$50.00
- SD-3 SHIPBOARD RADAR, New and complete with test equipment....\$1050.00
- SQ RADAR, used but in good working order, complete with antenna, control unit\$650.00
- SN RADAR, used, good working order, complete\$550.00
- UG-27/U TYPE N RIGHT ANGLE ADAPTERS 10 for \$5.00; 1000 for \$250.00
- U.H.F. RIGHT ANGLE ADAPTER 10 for \$2.50; 1000 for \$125.00

ELECTRO IMPULSE LABORATORY

P. O. Box 250

Eatontown 3-0007

Red Bank, N. J.

ARROW "The Home of Values!"

BC 906—Frequency Meter

Range 150-225 MC with modifications possible for lower frequencies of TV, etc. Contains 0-500 DC microammeter and uses Battery pack of 1.5 V and 45 VDC.
Like New—Less Batteries **\$10.95**

CONDENSERS

1 mfd 6000 VDC, OIL FILLED	Each	\$1.98
.00025 mfd. 25000 VDC OIL FILLED		2.95
1 mfd. 600 VDC, OIL FILLED		.24
	5 for	1.00
50 mmfd—5KV—5 Amp. Vacuum Cond.		1.19

AS-138/ARN—10 inch streamline loop as used with direction finding receivers. Fixed position. It is ideal for planes, boats, automobiles. New **\$1.95**

IS-185 Weston Voltmeter Model 433—0 to 150 VAC 25 to 2400 cycles. New **\$24.95**

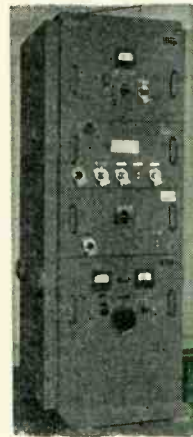
TUBE SPECIALS!

211	\$.39
307A	5.50
703A	1.89
723A/B	12.95
724B	1.89
803	2.89
805	3.29
807	1.89
813	6.95
832	2.95
832A	7.95
837	1.19
84149
860	4.95
86424

DYNAMOTORS

DM 32A	PE 73
DY2/ARR2	PE 94
DA 1A	PE 86
DM 34	DM 28
DM 35	DM 33
DM 36	PE 208
DM 37	PE 101
DM 40	DM 53A
DY 12	PE 218
DY 17	MG 149
BD 77	

Many other types are also in stock. Your inquiry is invited. Prices upon request.



RADIO EQUIPMENT

RC 100 B

This equipment made by General Electric, was designed for ground use as an identification of friendly aircraft.

CABINET CH-118 is of the Standard 19 inch rack type structural steel frame with runner angles for each of the units. A full length access door with safety interlocks forms the rear of the cabinet. \$34.95
TRANSMITTER BC-769 is designed to transmit RF pulsed signals at 470 megacycles with the use of the two type 15E Tubes operating in push-pull with resonant grid, plate and filament lines — Less tubes \$19.95

KEYING UNIT BC-770 furnishes the pulse of the Transmitter— Less tubes \$14.95

RECEIVER BC-768 was used to detect the 493.5 megacycle reply pulses from the interrogated station and to sufficiently amplify these signals for oscilloscope observation. Less tubes \$19.95

RECTIFIER RA-52 produces the high voltage. An 0-15 kilowatt DC Meter is connected across the output of the filter to measure the voltage fed to transmitter BC-769, while an 0-20 milliammeter is connected to ground return to measure the average current drawn— With tubes \$74.50

AIR COMPRESSOR M-349 together with 12 feet of 3/4 inch soft copper tubing and necessary hardware is used to fill and maintain transmission lines with dry air under pressure. Operation is direct from 110 V AC 60 cycles \$42.50

OVEN M-348 is furnished for removal of moisture from the dehydrating cylinders of the compressor. It too operates from 110 V AC 60 cycles \$29.50

FREQUENCY METER BC-771 is used for frequency checking and for tuning operations on Radio Transmitter BC-769 and Radio Receiver BC-768. It is a separate unit mechanically and has its own power supply, which requires a 110 to 120 Volt, 50 to 60 cycle source \$49.50

TECHNICAL MANUAL TM11-1113B covering entire equipment \$5.00

COMPLETE UNITS are available at amazing low price . . . WRITE TODAY!

BC-604 TRANSMITTER FM 20-28 MC

11 and 15 meters. Can be operated on 10 meters—10 channel push button crystal. With all tubes and meter but less dynamotor. Excellent Condition

\$19.95

Crystals — Set of 80

\$19.95

BC 603

Receiver—Good. Used.

\$24.95

Complete SCR-508 Installation available—price and information upon request.

MISCELLANEOUS SPECIALS!

	Used	New
ASB 7 Indicator Scope	\$12.95	
MN 26 C	17.50	\$24.95
RA 10 DA Receiver	17.50	24.95
RT/APN1 Transceiver	6.95	9.95
APN 1 Complete		24.50
BC 347 Interphone Amplifier		.89
I-70 Tuning Meter		.59
BC 401 Veeder Root Counter		1.49
BC 442 Less Condenser		.98
AFS 13 UHF Antenna, Pair		2.95
FL 8 Filter		3.95
I-97 Bias Meter		4.95
RM 29 Remote Telephone Control	7.95	9.95
RL 42 Antenna Gearbox Motor and Reel	4.95	7.50
TS 10—Sound powered phones	6.50	
BC 1066 B—150 to 225 MC Portable Receiver adaptable to many amateur uses. In Canvas Carrying Bag. Used		\$5.95
Tuning Units for BC 375		Presently most numbers are available in excellent condition with case at \$2.95 ea.
One Tube Interphone Amplifier—Small compact aluminum case fully enclosed. 2 1/4" x 3 3/4" x 5 3/4". Less Tube	 79c
96Q1 Complete Autotune assembly with motor and frame as used in ARC-1 Transmitter. New	 \$35.00
BC 709 Battery operated lightweight interphone amplifier. Complete with tube and shock mount, but less battery. New	 \$3.95
SCR 183 Complete	 New \$49.50
250 MA Circuit Breaker	 New .59
Collins VFO Dial—5 calibrated ham bands from 3.2 Mc to 32 Mc; complete with pointer, gears, logging dial and flywheel. Scale 6" on 8" plate. New	 each .95
C-18—Antenna coil assembly slug tuned used in BC 603 receiver. Frequency range 20-27.9 Mc.—fully shielded. New. 10 for \$1.95		
I 82 F—Five Inch 360 degree compass indicator and Selsyn receiver. New	 \$4.95
Indicator	 \$2.45
A-81-2 Transmitter selsyn for 182 indicator	 \$2.45
(Both I82F & Trans. Selsyn for \$7.00)		
MC 385A—Headset Adapter. New	 49c
Information and Prices on Request		
RTA 1B Transceiver		
TA 2J24 Transmitter and MP 10G Power Pack		
SCR 2'9 Compass Installation		
R 5/ARN 7 Compass Installation		
MN 26 Compass Installation		
ASB7 Complete Radar Installation		

IDG/APN4 Scope unit complete with 5CP1 cathode ray tube and shield and all parts except smaller tubes and crystal. Used \$9.95 ea.

BC 620

Receiver-Transmitter—2 crystal channels—20 to 27.8 MC FM—13 tubes. Metered, Plate and Filament Used \$9.95
PE-97 or PE 117 or PE 120 Power Supply for above 6-12 volt vibrator type. Used less tubes, vib. & con. \$2.95
Used, complete \$6.95
FT 250 Mount for both BC 620 and PE 97 New \$1.50

BC 223

Brand new Transmitter with all three tuning units, two tuning unit cases, spare tube carrying case, shock mount and brace; **\$29.95** but less tubes at new low price of \$3.95
Set of 5 tubes \$3.95
Tuning units are available separately at Ea. \$2.50
PE 125—12-volt Vibrator Pack. New \$12.95 Used 8.95

SURPRISE PACKAGE

20 lbs. Ass't radio parts. **\$1.95**
A \$25.00 value for only

TEST EQUIPMENT

EV-10 Precision Vacuum Tube Test Set	used	\$28.00
No. 772 Weston Multi Tester	used	40.00
No. 492 Radio City Products. Volt-Ohm Meter	used	25.00
No. 471 Radio City Products Output Meter	used	10.00
No. 803 Radio City Products Tube Tester & Set Tester	used	35.00
No. 777 Weston Tube Checker	used	29.00
No. E 200 Precision Signal Generator	used	25.00
No. M-652 Jackson Audio Oscillator	used	30.00
No. 224 A Dumont Oscilloscope	used	80.00
No. 185 A RCA Oscilloscope	used	90.00
No. M-840 Triumph Oscilloscope	used	75.00
BC-1287 Oscilloscope	used	75.00
BC-231 Frequency Meter	Like New	90.00
Others as Low as		49.50

PRICES UPON REQUEST

I-98-A	TS10A/APN
I-114 P/O RC-68	TS16/APN
I-135 P/O IE-17	TS19/APQ5
I-167 Weston Anal. #772	TS27/TSM-1
I-183 Freq. Meter	TS36/AP
I-185 Oscillator	TS47/AP
I-187 Synchronizer	TS59/APN-1
I-189 Calibrator	TS62/AP
IE-19	TS102A/AP
IS-185 Voltmeter	TS126/AP
TS3/AP	TS-251 Less Xtal

COMMAND (SCR 274 N) EQUIPMENT

	Used	New
BC-453	\$12.95	
BC-454	5.95	
BC-455	7.95	\$9.95
BC-456		2.95
BC-457	5.95	
BC-458	5.95	8.95
BC-696	14.95	24.95
BC-450—3 Receiver Remote Control	.89	1.95
BC-442		2.95
3 Receiver Rack		1.95
2 Transmitter Rack		1.50
Complete Command set as removed from aircraft—3 receivers—2 transmitters—Relay unit control boxes—mounting racks—plugs—modulator and dynamotors—crated		Set \$34.50

R C—150 RADIO EQUIPMENT

BC 1161 A Receiver is a 14 tube superhet all ready for 110 V 60 cycle operation. Frequency coverage is from 157 to 187 MC, but may be trimmed to cover the two meter ham band. The IF transformers are stagger tuned to provide a 4 MC band pass, but they may be retuned to a sharp center frequency of 11MC with no wiring changes. All RF and IF tuning is done by observing a magic eye indicator tube from the front panel. Brand New—Complete \$34.95

BC 1160 A Transmitter also covers a frequency of from 157 to 187 MC and is also ready for 110 V 60 cycle operation using a transtat for regulated control and a meter for indication. Output is pulsed, reaching a peak of one kilowatt. Tube complement as follows: 1-6SN7; 1-9002; 1-9006; 1-6J5; 1-807; 1-2X2; 2-326; 2-5V4G. Brand New—Complete \$34.95

BC 1162 A Interconnector and wavemeter units. These are contained in one housing but may be separated without interfering with the separate circuit wiring. Primary purpose is to control operation of transmitter and receiver units for correlation with radar screen, and to provide means of measuring their frequencies by means of cavity resonator. New, complete except tubes. \$14.95

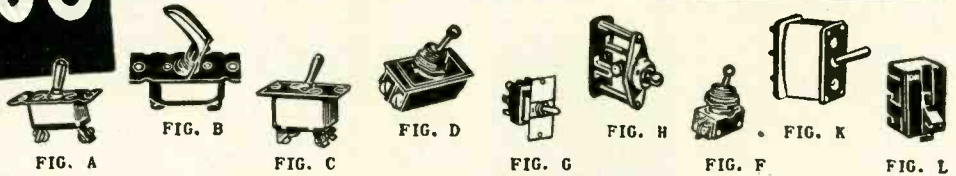
All shipments FOB warehouse. 20% Deposit required on all orders. Minimum order accepted—\$5.00. Illinois residents, please add regular sales tax to your remittance.

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FINEST QUALITY

**Immediate Delivery from Our Huge Stock...
All New and Unconditionally Guaranteed!**

Switches

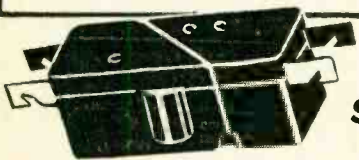


**WIDE SELECTION
OF ELECTRONIC
COMPONENTS AT
WELLS**

- Tubes • Resistors
- Condensers
- Wire and Cable
- Volume Controls
- Co-ax Connectors
- Relays • Rectifiers
- Transformers • Chokes
- Micro Switches, Toggles
- Antennas, Accessories
- Electronic Assemblies
- Dial Light Assemblies

TOGGLE SWITCHES

STOCK NUMBER	FIG.	CONTACT ARRANGEMENT	MANUFACTURER & NUMBER	PRICE EACH
PH-500	A	SPDT.	B1B.	\$0.35
PH-503	A	SPDT Center Off Mom Each Side.	B11.	.32
PH-505A	A	SPDT Momentary.	B21.	.30
PH-505	A	SPST.	AN-3022-2B.	.30
PH-506	A	SPDT Center Off.	AN-3022-1.	.35
PH-507	A	SPDT Center Off Mom Each Side.	AN-3022-7B.	.32
PH-513	A	SPDT Center Off.	Cutler Hammer AN-3022-1B.	.38
PH-514	A	SPST.	Cutler Hammer B-5A.	.35
PH-516	A	SPST.	B5.	.35
LT-104	A	SPDT One Side Momentary.	Cutler Hammer 8905K568.	.35
309-168	A	SPST.	168553.	.30
309-178	A	SPDT Momentary.	AN-3022-11B.	.35
309-181	A	SPST Momentary.	Cutler Hammer 8211K6.	.35
305-172	A Spcl.	SPST Momentary.	Cutler Hammer 8905K531.	.35
305-182	A Spcl.	SPST Momentary.	Cutler Hammer 8905K630.	.45
370-14	A	SPDT Center Off 1 Side Mom.	Cutler Hammer B-7A.	.30
370-4	A	SPDT Center Off.	Cutler Hammer B-9A.	.35
370-25	A	SPST Momentary.	Cutler Hammer B-6B.	.25
309-169	B	SPST Momentary.	Cutler Hammer B-19	.35
PH-509	C	DPST.	AN-3023-2B.	.45
PH-510	C	DPDT Momentary.	Cutler Hammer 8715K2.	.50
PH-511	C	DPDT Momentary.	Cutler Hammer 8715K3.	.50
PH-512	C	DPST Center Off.	Cutler Hammer 8720K1.	.55
303-65	C	DPST.	Cutler Hammer AN-3023-2.	.45
309-163	C	DPDT Center Off Momentary.	Cutler Hammer C-11.	.55
309-162	C	DPST.	Cutler Hammer C-1.	.45
309-164	C	DPST Momentary.	Cutler Hammer 8711K3.	.40
305-87	D	1 Side DPST Mom, 1 Side SPST.	AH & H	.95
LT-100	F	SPST.	Cutler Hammer.	.22
LT-101	F	SPST Momentary.	AH & H. W/Leads.	.20
301-51	G	4PDT Momentary.	Cutler Hammer 8905K12.	.75
305-140	H	DT No Make Each Side.	Open Frame.	.25
309-161	K	SPST.	Cutler Hammer 8781K3.	1.95
309-170	K	SPST.	Cutler Hammer 8905K656.	2.25
301-41	L	DPST.	AH & H	.75
305-76	L	DPST.	AH & H—Open Frame.	.75
319-50	L	SPST.	Allied Elec. Mfg. Corp.	.28
305-170	Spcl.	SPST.	Cutler Hammer Type B13.	.40



SWITCHETTES

STOCK NUMBER	MANUFACTURER'S TYPE NUMBER	CONTACTS	TERMINAL LOCATION	UNIT PRICE
303-20	CR1070C103-A3	N.C.	Side	\$0.47
301-29	CR1070C103-B3	N.O.	End	.47
303-34	CR1070C103-C3	1-N.O. 1-N.C.	End	.47
303-18	CR1070C103-F3	1-N.O. 1-N.C.	Side	.47
303-19	CR1070C103-E3	N.O.	Side	.47
303-43	CR1070C123-B3	N.O.	End	.47
303-23	CR1070C123-C3	1-N.O. 1-N.C.	End	.47
305-83	CR1070C123-J2	SPDT	End	.47
303-22	CR1070C123-J4	SPDT	End	.47
303-17	CR1070C124-M4	SPDT	Side	.47
303-16	CR1070C128-C3	1-N.O. 1-N.C.	End	.47

LEAF SPRING SWITCHES

STOCK NUMBER	CONTACT ARRANGEMENT	SPEC. INFORMATION	BACK OF PANEL DIM.	PRICE EACH
302-96	HPDT One Side.		3 1/4 x 1 3/4 x 3/4	\$1.65
311-58	1A Momentary & 1A.	W/Escutcheon Plate	3 1/4 x 3/4 x 3/4	1.35
309-167	2C One Side.		3 x 1/2 x 1 1/16	1.25
305-183	3A Momentary & 3A Momentary.		3 1/2 x 1 1/2 x 3/4	1.50
319-43	DPDT Center Off.	Mossman.	3 7/8 x 2 x 1 3/8	.85
319-42	4PDT Center Off Mom One Side.	Mossman.	3 7/8 x 2 x 1 3/8	.95
309-159	3B.	Mossman.	3 7/8 x 2 x 1 1/4	.85
309-158	2D.	Mossman.	3 7/8 x 2 1/4 x 1 3/8	.85
309-165	1A.	Mossman.	3 7/8 x 1 3/4 x 1 1/4	.75
311-96	4PDT.	Bakelite Actuator.	3 1/2 x 1 3/8 x 7/8	.85
305-164	3A.		3 1/2 x 1 1/2 x 1 1/16	1.25
319-43A	DPDT Center Off Mom Each Side.	Mossman.	3 7/8 x 1 3/8 x 2	.95
305-165	3A & 3A.	Switchboard Type.	4 3/4 x 1 1/2 x 3/4	.95

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Order From Your Parts Jobber or Directly From Wells.

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World's Largest Display of Radio and Electronic Components. 9000 Square Feet of Display All on One Floor.



320 N. LA SALLE ST. DEPT. SL, CHICAGO 10, ILL.

RCA HI-VOLTAGE TRANSFORMER

Pri—115/230V. 60Cy
Sec—6000V—80 MA

\$11.80

Insulated for
Voltage Doubler Use



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LOW INERTIA SERVO MOTORS

Type 937-0240—85/68 Volts—100 Cycles
2 Phase—5 Watts—2650 RPM
Will Operate Satisfactorily at 60 Cycles
Original Price \$34.50—Our Price—\$8.22 ea.

\$7.50 EACH—Lots of 10

COAXIAL CONNECTORS



83-LAC	.42 UG-12/U	.63 UG-86/U	1.22
83-LAP	.15 UG-21/U	.67 UG-87/U	.79
83-IF	1.12 UG-22/U	.86 UG-171/U	1.33
83-IH	.10 UG-23/U	.85 UG-175/U	.15
83-IJ	.80 UG-24/U	.67 UG-176/U	.15
83-IR	.40 UG-27/U	.68 UG-181A/U	7.83
83-ISB	.45 UG-29/U	.83 UG-191/AP	.63
83-ISPN	.40 UG-30/U	1.20 MX-195/U	.41
83-IT	1.12 UG-34/U	12.80 UG-197/U	1.33
85-22AP	1.10 UG-36/U	12.80 UG-206/U	.63
83-22F	1.48 UG-37/U	12.80 UG-255/U	1.22
83-22R	.88 UG-58/U	.63 UG-264/U	1.74
83-22SP	.45 UG-85/U	.88 UG-290/U	.85

FULL LINE OF JAN APPROVED COAXIAL CONNECTORS IN STOCK

WESTINGHOUSE HYPERSIL TRANSFORMER



PRI-115V. 60CY 1/4 KVA
SEC #1 - 240V - 1.56A
SEC #2 - 240V - 1.56A
WT. 30 LBS.

\$11.50 EACH

GENERATORS

• Eclipse-Plioneer type 716-3A (Navy Model NEA-3A)
Output—AC 115V 10.4A 800 to 1400 cy. 1 φ; DC 30
Volts 60 Amps. Brand New—Original Packing \$38.50

• Eclipse-Plioneer type 1235-1A. Output—30 Volts
DC 15 Amps. Brand New—Original Packing... \$9.50

STANDARD BRANDS ONLY

TUBE SPECIALS

BRAND NEW FIRST QUALITY

COMPLETE STOCK OF RECEIVING, TRANSMITTING, CATHODE RAY, THYRATRON, IGNITRON, MAGNETRON, KLYSTRON, PHOTOCCELL, T-R & ATR TUBES.
QUOTATIONS UPON REQUEST

PULSE TRANSFORMERS

UTAH 9262 and 9340	\$2.75
UTAH 9278	2.75
G. E. 68G-627	4.75
AN/APN-9 (901756-501)	1.50
AN/APN-9 (901756-502)	1.25
AN/APN-4 Block, Osc.	1.50
Philco 352-7149—Modulator to 50 ohm line. 115 KW peak power	\$9.95
Philco 352-7150—50 ohm line to magnetron. 115 KW peak power	\$9.95

SPRAGUE PULSE NETWORKS

7.5 E3-1-200-67P. 7.5 KV. "E" Circuit 1 microsec.	\$4.30
200 PPS, 67 ohms Imped. 3 sections.	
7.5 E3-3-200-67P. 7.5 KV. "E" Circuit 3 microsec.	\$6.75
200 PPS, 67 ohms Imped. 3 sections.	
7.5 E4-16-67P. 7.5 KV. "E" Circuit 4 sections.	\$8.25
16 microsec. 60 PPS, 67 ohms Imped.	
15-E4-15-600-50P. 15 KV. "E" Circuit 1.5 microsec.	\$12.00
600 PPS, 50 ohms Imped. 4 sections.	
15-E6-180-50P. 15 KV. "E" Circuit 5 microsec.	\$25.00
180 PPS, 50 ohms Imped. 6 sections.	

MISCELLANEOUS EQUIPMENT

ID-6/APN-4 Indicator	\$29.50
R-7/APS-2 Receiver	49.50
R-7/APS-15 Receiver	49.50
SCR-522 Transceiver	36.95
RT-7/APN-1 Transceiver—less tubes.	6.95
FL-8 1020 cycle filter.	1.37
RM-29 remote control unit.	8.95
RM-14 remote control unit.	8.95
RTA-1B 1/2 24 V dynamotor.	30.00
BC-1206-C-2 Receiver	7.95
CY-230/MFG-1 Radar Console.	575.00
G.E. Type JP-1 portable current transformer.	32.50
ASB-4 Radar equilb. Complete.	69.75
AN/APS-13 less tubes.	12.95
T-9/APQ-2 less tubes.	16.50
BC-645A complete	18.95
RCA AVR-15 Beacon Recvr.	15.00
TBY Trans-Recvr	29.95
T-47/ART-13 Transmitter	165.00
T-47A/ART-13 Transmitter	165.00
G.E. 2CV2A1 Servo Amplifier	6.95
Sperry A-3 Hydraulic Servos	3.95
ETMAC 35 TG Ionization Gauge.	5.95
CP-11/APS-15 Range Unit less tubes.	32.50
ATR Inverters 6VDC to 110 VAC 60 cy 75W—Orig. Cartons	19.95
Pioneer Type 800-1B Inverters—28VDC to 120V 300 cy 7 amp AC (used)	22.65
G.E. Inverter—28VDC to 120VAC 800 cy 750VA 1 φ (new)	39.50

SOUND POWERED TELEPHONES

• U. S. INSTRUMENT Type A-260
• WESTERN ELECTRIC Type D-173013
• AUTOMATIC ELECTRIC Type GL-832BAO
U. S. NAVY TYPE M HEAD AND CHEST SETS
These are high quality heavy-duty units not to be confused with cheaper units now available. Designed to withstand exacting shock, vibration, salt water corrosion, temperature and pressure tests. ANY TYPE \$14.88 ea., \$28.00 per pair.
TS-10 HANDSETS \$8.92 each

METERS

500 Microamps, DC—2 1/2" round—Sun	\$4.30
1 ma, DC 3/4" R. (4 KV scale)—Roller Smith	4.17
1 ma, DC Fan type—4" scale (rem. from equlpt)	3.95
500 ma, DC 2 1/2" R.—General Electric	2.95
3 amp, RF 3 1/2" R.—Weston	4.95
2 amp, RF 2 1/2" Sq.—Simpson	3.15
5 amp, AC 4 1/2" R.—JBT	4.11
1 ma, DC 4 1/2" R.—General Electric	6.95
50 VAC 3/4" R.—General Electric	4.11
58-62 Cycles (115 V.) 3 1/2" R.—JBT	6.45
10 amp, RF 3 1/2" R.—Simpson	4.95

MAGNETRONS

2J21A	\$8.95	2J38	12.70	700C	16.50
2J22	8.95	2J41	132.50	700E	16.90
2J26	7.26	2J48	14.95	706AY	45.00
2J27	13.70	2J49	39.50	706BY	45.00
2J31	9.60	2J61	36.20	706CY	17.95
2J32	14.45	4J50	197.00	706FY	45.00
2J33	19.90	4J52	197.00	706GY	45.00
2J34	19.90	5J23	14.20	714AY	6.95
2J36	85.00	5J29	14.20	735A	8.95
2J37	13.70	700B	16.90	730A	10.95

KLYSTRONS

2K23	\$23.95	2K33	295.00	707B	12.95
2K25	23.50	2K54	135.00	723A	6.95
2K26	75.00	2K55	135.00	726A	11.95
2K28	23.50	417A	10.65	726A	14.50
2K29	29.95	707A	6.95	726B	29.50

TYPE "J" POTENTIOMETERS
75¢ each

Resis.	Shaft	Resis.	Shaft
100	SS 10K	SS 100K	5/16"
500	SS 15K	SS 100K	7/16"
500	1/2" 15K	SS 100K	7/16"
650	1/2" 20K	SS 100K	SS"
5000	1/2" 25K	1 1/2" 150K	1/2"
6500	SS 25	SS 200K	SS"
10K	1/2" 30K	1 1/2" 250K	SS"
10K	1/2" 50K	SS 1 MEG	SS"

Deal "JJ" Potentiometers—\$1.30 each
50-50 Ω SS 100-100 Ω SS 250-250 Ω SS
Triple "JJ" Potentiometers—1/2" shaft. \$1.67
All shaft lengths beyond bushing—SS (screw slot)

TEST EQUIPMENT

• A.W. Barber Lays. VM-25 VTVM \$86.00
• TS-10A/APN Delay Line Test Set \$25.00
• TS-19/APQ-5 Calibrator \$75.00
• AT-48/UP "X" Band Horn \$39.95
• REL W-1158 Frequency Meter 160-220 MC. \$32.95
• CWL-60AAG Range Calibrator for ASB, ASE, ASV and ASVC Radars. \$39.95
• CRV-14AAS Phantom Antenna for Transmitters up to 400 MC. \$11.75
• TS-146/AP X-Band Test Set. Price on request.
• TS-184/AP \$1.35 Price on request.
• CPR-60AAJ and CPR-60AAK—IFF Test Sets. (pair) \$16.95
AN/APA-23 Recorder \$147.50
TN-1B/APR-1 Tuning Unit \$95.00
C-D Quietone Filter Type IF-16 110/220 V AC/DC 20 Amps \$9.00
• TS-127/V Freq. Meter w/spares \$69.50
• TS-143/CPN Oscilloscope \$95.00
• Dumont 175A Oscilloscope \$225.00
• Telrad 18 A Frequency Std. \$29.50
• LM-20 Frequency Meter 49.50
• Gen. Radio 757-PI Power Supply \$38.00
• Gen. Radio 670-F Decade \$27.00
• I-130 A Signal Generator \$70.00
• TS-6/AP Frequency Meter \$42.00
• L & N KS-9470 Null Volt Test Set \$60.00
• Measurements 79B Pulse Generator \$200.00
• MIT TTX-10RH 3 cm FM Test Set \$325.00
All Items New Except Where Noted (Exc. Used Condition)

SYNCHROS

General Electric 2J1G1 pair \$2.95
Caps for connecting to above. pair 1.00
G. E. 2J1F Generators. ea. 2.85
C-78248 Transmitters—110V 60 cy. pair 8.95
C-78411 Transmitters—50V 50 cy. pair 8.25
C-78249 Differentials—110V 60 cy. ea. 2.95
C-78410 Repeaters—110V 60 cy. ea. 6.75
C-69406-1 Repeaters—110V 60 cy. ea. 12.00
Many additional types in stock including:
Types B, M, N, X, F, J, E, 43-1
Sizes 5CT, 5D, 5DG, 5F, 5G, 5SF, 6G, 7DG

CONSTANT VOLT. TRANSFORMERS

Federal Constant Voltage Transformer Input 95-135V
60cy Output 115V 210W \$34.00
Sola Constant Voltage Transformer Input 95-126V
60cy-Output 15.8V 285VA \$24.70
Sola Constant Voltage Transformer Input 105-125V
60cy-Output 115V 80VA \$15.95

SELENIUM RECTIFIER STACKS
FULL WAVE BRIDGE

MAXIMUM RATINGS AC VOLTS INPUT - 18 DC VOLTS OUT - 14.5	MAXIMUM RATINGS AC VOLTS INPUT - 40 DC VOLTS OUT - 34
1.2 Amps..... \$2.64	0.6 Amps..... \$3.00
2.4..... 3.07	1.2..... 3.44
6.4..... 4.99	3.2..... 5.15
13.0..... 7.67	6.0..... 9.32
17.5..... 8.69	9.0..... 10.05
26..... 15.33	12..... 18.64
39..... 23.00	18..... 20.12
52..... 30.67	24..... 35.96
65..... 38.33	36..... 41.24

W. E. MERCURY CONTACT RELAYS

Glass sealed mercury wetted SPDT contact assemblies. Magnetically operated. Used In Western Electric D-168479 high speed plug in relays. Supply your own coil \$2.00 each

PIONEER SERVO SYSTEM UNITS

• Type 12073-1A Torque Amplifier, Input 115 V 400 cy. Complete with Tubes \$14.95
• Magnetic Amplifier Assy. Saturable Reactor Type to supply one phase of 400 cycle Servo Motor \$5.95

OIL FILLED CONDENSERS

MFD	VDC	Price	MFD	VDC	Price
2	600	\$.45	2	2000	\$2.70
4	600	.95	4	2000	3.95
4	600 (R'd)	.05	1	2500	.49
4	600 (R'd)	1.05	1-1	2500	3.85
8	600 (R'd)	1.39	32	2500	12.80
10	600	.95	1	5000	4.88
10	600 (R'd)	1.52	.01-.03	6000	1.65
8-8	600	1.49	1	7000	1.79
1	1000	.62	2	12500	23.95
2	1000	.89	.045	16K	4.70
3.5-.5	1000	1.35	.05	16K	4.95
1	1500	.89	.075	16K	8.95
4	1500	2.95	50	220VAC	3.95
1-.5	2000	.87	60	330VAC	5.75
.5	2000	.95	7	660VAC	3.35
1	2000	1.50			

ANTENNAS

AT-38A/APT (70 to 400MC)	\$13.70
AT-49/APR-4 (300 to 3500MC)	13.70
AT-48/UP 3 cm horn antenna	4.95
DZ-2 Loop antenna with pedestal	14.50
AN-74B (125 to 150MC)	1.65
AN-65A (P/O SCR-521)	.95
AN-66A (P/O SCR-521)	1.15
A1A—3CM conical scan	125.00
ASB Yagi—5 element 450 to 560MC	7.00
ASB Yagi—Double stacked 6 element	12.70
ASA Yagi—Double stacked 370 to 430MC	29.40

COMPONENT SPECIALS

FUSES	4AG	10 Amp.	\$3.00/c
	4AG	20 Amp.	\$3.00/c
MOLDED PAPER CONDENSERS—			
.02 MFD	200 VDC	.04 1/2 Ea.	\$3.00 per 100
.05	200	.04 1/2	3.00
.1	200	.04 1/2	3.00
.25	200	.06	4.00
.1	400	.09	6.00
.005	600	.04 1/2	3.00
.01	600	.07	4.75
.05	600	.08	5.50

CRYSTAL DIODES—

1N21	.79	1N23	1.19	1N45	.94
1N21A	1.19	1N23A	1.55	1N52	1.05
1N21B	2.75	1N27	1.09	1N63	1.39
1N22	.89	1N34	.79		

PHASE SHIFT CAPACITOR—Type D—150734—4 stator single rotor. \$2.69

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SELENIUM RECTIFIERS and ASSOCIATED COMPONENTS

SINGLE PHASE

Full Wave Bridge

Input: 0-18 VAC		Output: 0-12 VDC	
Type No.	Current		Price
B1-250	250 Ma.		\$.98
B1-1	1.0 Amp.		2.49
B1-1X5	1.5 Amp.		2.95
B1-3X5	3.5 Amp.		4.50
B1-5	5.0 Amp.		5.95
B1-10	10.0 Amp.		9.95
B1-20	20.0 Amp.		15.95
B1-30	30.0 Amp.		24.95
B1-40	40.0 Amp.		27.95
B1-50	50.0 Amp.		32.95

Input: 0-36 VAC		Output: 0-26 VDC	
Type No.	Current		Price
B2-150	150 Ma.		\$.98
B2-250	250 Ma.		1.25
B2-300	300 Ma.		1.50
B2-2	2.0 Amp.		4.95
B2-3X5	3.5 Amp.		6.95
B2-5	5.0 Amp.		9.95
B2-10	10.0 Amp.		15.95
B2-20	20.0 Amp.		27.95
B2-30	30.0 Amp.		36.95
B2-40	40.0 Amp.		44.95

Input: 0-115 VAC		Output: 0-90 VDC	
Type No.	Current		Price
B6-250	250 Ma.		\$2.95
B6-600	600 Ma.		5.95
B6-750	750 Ma.		6.95
B6-1X5	1.5 Amp.		10.95
B6-3X5	3.5 Amp.		18.95
B6-5	5.0 Amp.		24.95
B6-10	10.0 Amp.		36.95
B6-15	15.0 Amp.		44.95

Full Wave Center Tap

Input: 10-0-10 VAC		Output: 0-8 VDC	
Type No.	Current		Price
C1-10	10.0 Amp.		\$6.95
C1-20	20.0 Amp.		10.95
C1-30	30.0 Amp.		14.95
C1-40	40.0 Amp.		17.95
C1-50	50.0 Amp.		20.95

THREE PHASE

Full Wave Bridge

Input: 0-234 VAC		Output: 0-250 VDC	
Type No.	Current		Price
3B13-1	1.0 Amp.		\$22.00
3B13-2	2.0 Amp.		32.00
3B13-4	4.0 Amp.		56.00
3B13-6	6.0 Amp.		81.50
3B13-10	10.0 Amp.		105.00
3B13-15	15.0 Amp.		120.00

RECTIFIER MOUNTING BRACKETS

For Types B1 through B6, and Type C1 \$.35 per set
For Types 3B 1.05 per set

D-C PANEL METERS

Attractive, rugged, and reasonably priced. Moving vane solenoid type with accuracy within 5%. Square case.

0-6 Amperes DC
0-12 Amperes DC
0-15 Volts DC

Any range \$2.49 each

ATTENTION MANUFACTURERS!

We are now in a position to furnish Selenium Rectifiers, in quantity, to specifications. Excellent delivery, prompt quotations.

Minimum Order \$5.

All prices FOB our NYC warehouse. Send check or money order. We will ship transportation charges collect. Rated concerns send P.O., Terms Net 10 days.

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GENERAL PURPOSE Low voltage DC power supplies, with variable outputs. Rugged—Dependable—precision control.

Features

- ✓ Long life Full Wave Selenium Rectifiers
- ✓ Output Voltage Continuously Adjustable from Zero to Maximum
- ✓ 3" Voltmeter and Ammeter 2% acc'y.
- ✓ Stepless Control
- ✓ Instant Power—No Warm-Up Period
- ✓ Assembled and Ready to Operate
- ✓ For 115 VAC 60 Cycles
- ✓ Dimensions 8 1/2" x 16 3/4" x 8"

Write for descriptive bulletin GPA

Model	Voltage	Current	Price
GPA810	0-8 VDC	10 Amps.	\$69.50
GPA1210	0-12 VDC	10 Amps.	75.00
GPA2810	0-28 VDC	10 Amps.	85.00

RECTIFIER CAPACITORS

Model	Value	Voltage	Price
CF-1	1000 MFD	15 VDC	\$.98
CF-20	2500 MFD	15 VDC	1.95
CF-6	4000 MFD	30 VDC	3.25
CF-19	500 MFD	50 VDC	1.95
CF-18	2000 MFD	50 VDC	3.25
CF-21	1200 MFD	90 VDC	3.25
CF-2	200 MFD	150 VDC	1.69
CF-10	500 MFD	200 VDC	3.25

Mounting clamps for above capacitors 15c ea.

RECTIFIER TRANSFORMERS

All Primaries 115 VAC 50 60 Cycles				
Type No.	Volts	Amps	Shpg. wt.	Price
XF15-12	15	12	7 lbs.	\$ 3.95
TXF36-2	36	2	6 lbs.	4.95
TXF36-5	36	5	8 lbs.	6.50
TXF36-10	36	10	12 lbs.	9.95
TXF36-15	36	15	20 lbs.	11.95
TXF36-20	36	20	25 lbs.	17.95
XF18-14	18 VCT	14	10 lbs.	6.95

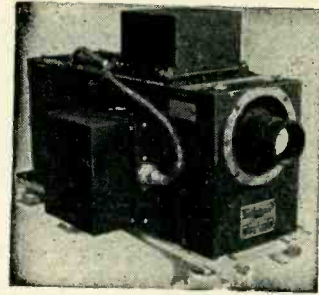
All TXF Types are Tapped to Deliver 32, 34, 36 volts. XFC Type is Tapped to Deliver 16, 17, 18 Volts Center-tapped.

RECTIFIER CHOKES

Type No.	Hy.	Amps	DC Res	Price
HY5A	.028	5	.20	\$5.25
HY10A	.014	10	.04	9.95
HY20A	.007	20	.02	13.95

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3350 line resolution. Easily converted to present RMA standards. Circuits available with camera. Complete, like new.

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APS-4 RADAR

APS-6 RADAR

MARK-16 RADAR COMPLETE

MARINE RADIO UNIT FT 102

(167BY Transmitter) 200 W. 4 bands covering range of 2-24 mc. NEW.

BC-1100-A TRANSMITTER with remote control. 125 W. 115 VDC or AC.

BC-452 TRANSMITTER

300 W. 1.5-7.0 mc. Point-to-point and air warning. A1, A2 and A3 emission. 115 and 230 V.

RC-184 IFF EQUIPMENT

Brand new. Complete.

COMPLETE LINE OF TEST EQUIPMENT SUCH AS:

TS-36/AP TS-117 WAVE METER

TS-35/AP TS-102A/AP

TS-108 TS-12/AP (Units 1 & 2)

1-177 HICKOK TUBE CHECKER

TS-184A/AP

WE ARE LOOKING FOR: ALL TYPES OF RADAR, GROUND and AIRCRAFT RADIO EQUIP.

We Want: BC-348 ART-13
ARC-1 RTA-1B
MN 62 R5A/ARN7
BC-1000

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2E22.....	1.00	12A6.....	.35	616G.....	1.25
2J21.....	5.00	12H6.....	.60	616GT.....	1.25
2J21A.....	5.00	12K8.....	.60	617.....	.75
2J22.....	5.00	12SH7.....	.50	617.....	.75
2J28.....	5.00	12SJ7.....	.50	68A7.....	.75
2J27.....	5.00	12SR7.....	.50	68F7.....	.90
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OA4G	1.35	3B24	3.50	307A	4.95	801A	1.00
OB2	3.00	3B24W	5.50	310A	7.95	802	3.60
OC3	1.08	3C23	2.95	311A	7.95	803	2.95
OD3	1.08	3C23	49.50	312A	3.95	804	6.95
1A3	1.00	3C24	2.50	327A	2.95	805	2.95
CI1A	4.95	3C24	5.95	337A	3.95	806	12.00
CI1B	4.95	3C45	11.45	350A	3.95	807	1.69
1B21A	2.75	3DP1/A	2.95	350B	2.95	808	.95
1B22	3.95	3E29	12.50	357A	37.50	809	2.45
1B23	7.95	SN4	5.50	368AS	2.95	810	11.00
1B24	7.95	4A1	3.75	371B	.95	812	2.95
1B26	1.95	4C27	10.80	385A	4.95	958A	.49
1B27	7.95	4J25	99.00	388A	2.95	959	.69
1B32	1.75	4J26	99.00	393A	5.95	975A	12.95
1B38	33.00	4J31	220.00	394A	5.95	991	.45
1B42	5.95	4J37	99.00	417A	7.95	1280	1.95
1B56	49.95	4J38	89.00	446A	1.95	1611	1.95
1H60	4.95	4J39	99.00	446B	2.95	1613	1.08
1N21	1.35	4J57	99.00	450TL	35.00	1616	1.95
1N21A	1.75	4J62	99.00	464A	6.95	1619	.35
1N22	1.75	5J23	2.95	471A	2.75	1620	4.95
1N23	2.00	5J29	15.00	527	35.00	1622	2.75
1N23A	2.75	5J31	45.00	527	35.00	1624	1.00
1N23B	5.00	5J32	9.95	527	35.00	1625	.45
1N26	5.00	5J32	9.95	527	35.00	1851	1.95
1N27	5.00	5J32	9.95	527	35.00	8012	1.25
1N48	1.00	5J32	9.95	527	35.00	8013	6.95
1S21	3.95	5J32	9.95	527	35.00	8014A	24.95
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2C34	.35	5J32	9.95	527	35.00	9001	1.75
2C40	5.75	5J32	9.95	527	35.00	9002	1.50
2C43	21.00	5J32	9.95	527	35.00	9003	1.75
2C44	.90	5J32	9.95	527	35.00	9004	.75
2C51	5.95	5J32	9.95	527	35.00	9005	1.90
2D21	1.75	5J32	9.95	527	35.00	9006	.35
2E22	3.75	5J32	9.95	527	35.00		
2E30	4.00	5J32	9.95	527	35.00		
2F21	40.00	5J32	9.95	527	35.00		
2G21A	9.95	5J32	9.95	527	35.00		
2C22	9.95	5J32	9.95	527	35.00		
2D26	7.75	5J32	9.95	527	35.00		
2J27	12.50	5J32	9.95	527	35.00		
2J31	19.95	5J32	9.95	527	35.00		
2J32	19.95	5J32	9.95	527	35.00		
2J36	105.00	5J32	9.95	527	35.00		
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2J49	69.00	5J32	9.95	527	35.00		
2J50	39.50	5J32	9.95	527	35.00		
2J61	45.00	5J32	9.95	527	35.00		
2J62	45.00	5J32	9.95	527	35.00		
2K25	27.50	5J32	9.95	527	35.00		
2K28	27.50	5J32	9.95	527	35.00		
2K29	27.50	5J32	9.95	527	35.00		
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TS 12 Unit 2 Plumbing for above TS13	
TS16AA VSWR Measuring Amplifier Navy type TS9	
12 Unit 1	
TAA-11BL VSWR Measuring Amplifier, Browning	
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TS 35 X Band Pulsed Signal Generator	
TS 36 X Band Power Meter	
TS 45 X Band Signal Generator	
TS 146 X Band Signal Generator	
TS 263 Navy Version of TS 146	
TS 108	
X Band Magic T Plumbing	
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S Band	
TS3A/AP S Band Power and Frequency Meter	
RF 4 Electrically Tuned S Band Echo Box	
BC 1277/60ABQ S Band Pulsed Signal Generator	
PE 102 High Power S Band Signal Generator	
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Hazeltine 1060 Signal Generator 145 to 235 Megacycles	
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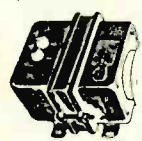
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MA. 3 filament	MA. 3 filament	MA. 3 filament
windings. 6.3-6A.	windings. 6.3-6A.	windings. 6.3-6A.
5A, 3-5A, 5-3A, 6.3-1.5A, 5-2A, 6.3-4A, 5-3 A.		
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This unit is designed primarily for aircraft installation, 24-28 volts D.C. but it can be readily adapted for a 115 or 230 volt 60 cycle power supply by use of a transformer and rectifier. Simple circuit diagram for adaption to 115 or 230 volts 60 cycle use supplied with each unit. Can be used on 32 volt farm or boat systems as is without the installation of additional transformers, etc. Power consumption approximately 75 to 100 watts.

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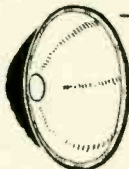
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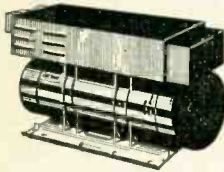
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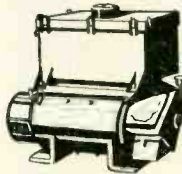
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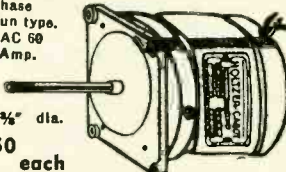
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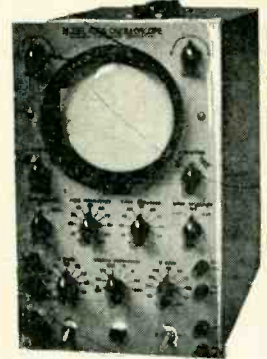
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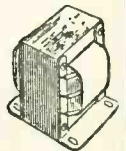
Pri. 115 v. 60 cy. Sec. #1: 125 v. @ 90 mls; #2: 135 v. @ 90 mls; #3: 6.3 v. @ 1.5 amps. Upright mt. Ea. **\$1.95**

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13.52	330	4	1155	2463	9445	33000	230000
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14.25	350	4	1200	2490	9710	37000	240000
14.5	360	4	1225	2500	9800	38140	240000
15	366	6	1250	2525	9900	38500	245000
16	370	4	1260	2600	9902	39000	250000
17	375	4	1300	2625	10000	39500	265000
19	380	4	1350	2635	10430	40000	268000
19.2	389	4	1355	2700	10500	42000	270000
20	390	4	1400	2750	10600	43000	275000
22	400	4	1488	2850	10900	45000	294000
23	410	4	1495	2860	10936	47000	300000
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25	418	3	1510	2900	11400	48000	311000
26	425	4	1518	3000	11500	48660	314000
28	426	9	1600	3100	11690	49000	316000
30	427	4	1640	3163	12000	50000	325000
31.5	440	4	1646	3259	12500	52000	330000
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45	457	4	1670	3333	13000	56000	333500
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49	460	4	1710	3500	13500	58333	353500
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68	520	4	1830	4030	14500	66600	422000
74	525	4	1865	4200	14550	66650	425000
75	540	4	1892	4220	14600	67500	450000
80	550	4	1894	4280	15000	68000	458000
81.4	575	4	1895	4300	16000	70000	478000
88	580	4	1896	4314	16500	72000	500000
89.8	588	4	1897	4440	16800	73500	520000
95	600	4	1898	4444	17000	75000	521000
100	612	4	1899	4500	17500	80000	525000
101	625	4	1900	4720	17977	82000	543000
105	633	4	1901	4750	18000	85000	550000
105.7	640	4	1902	4850	18300	85000	570000
107	641	4	1903	4885	18380	85750	575000
120	645	4	1904	4900	18500	88000	600000
121.2	649	4	1905	5000	18800	90000	620000
125	650	4	1906	5100	19000	91000	650000
130	657	4	1907	5210	19500	93000	654000
135	665	4	1908	5235	20000	95000	660000
147.5	668	4	1909	5270	20441	100000	690000
150	670	4	1910	5300	20500	110000	700000
160	673	4	1911	5500	21000	115000	750000
165	675	4	1912	5600	21500	116667	761300
170	680	4	1913	5730	22000	120000	800000
175	681	4	1914	5770	22500	130000	813000
179	684	4	1915	5910	22990	135000	850000
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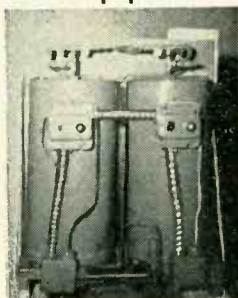
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Large advertisement for TAB TUBES with the slogan 'THAT'S A BUY' and contact information for the New York City store.

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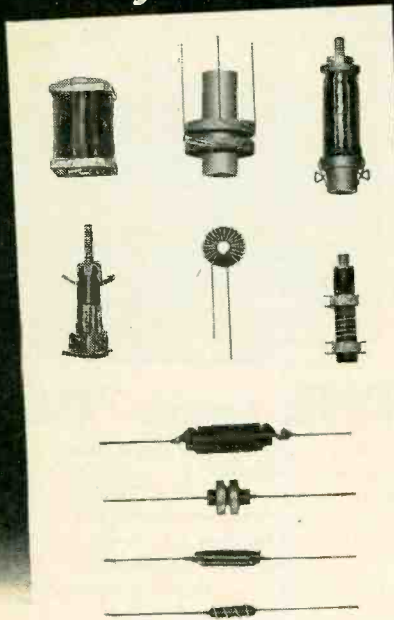
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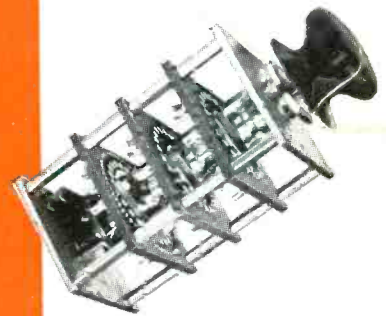
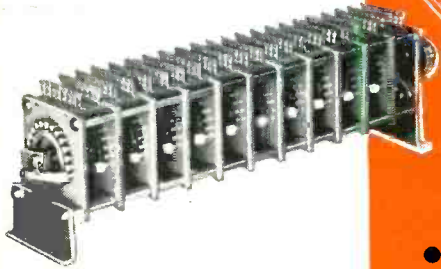
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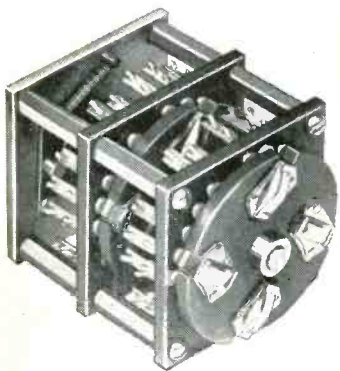
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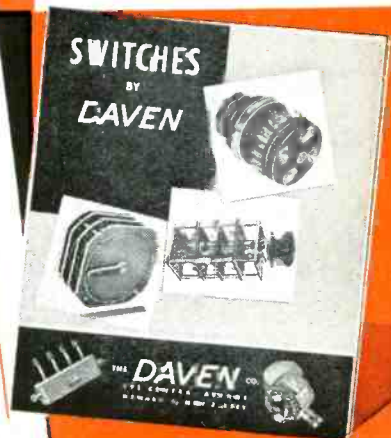
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C2B	Break before make	15	1	1 3/4"
D1A	Make before break	47	1	2 1/4"
D7A	Make before break	14	4	2 1/4"
D8B	Break before make	7	4	2 1/4"
D9A	Make before break	9	5	2 1/4"
E3A	Make before break	47	2	2 3/4"
E8B	Make before break	12	4	2 3/4"
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